## **LEVEL 2 ALTERNATIVES EVALUATION**

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SUBJECT: US 20 Albany Study – Level 2 Alternatives Evaluation Memo DKS P#23072-000

## INTRODUCTION

As part of the US 20 Albany study, a selection of project alternatives were selected and passed through fatal flaw evaluation (Tier 1 Screening) to determine which merited more detailed evaluation and consideration. The Project Management Team (PMT) consisting of ODOT and City of Albany met on October 10, 2023, to complete the Tier 1 Screening Process and agreed upon the alternative advancing to Level 2 Evaluation. The purpose of this memorandum is to present the outcomes of the detailed evaluation of these projects against the study evaluation criteria.

The Level 2 Evaluation builds on the Tier 1 screening by applying more rigorous transportation engineering analysis and evaluation criteria, ultimately providing a final recommended list of improvements for the corridor. The key findings and proposed recommendations from the Level 2 Evaluation target the corridor needs summarized in Figure 1.

This memorandum is organized into the following sections:

- Evaluation Criteria Overview of how the study evaluation criteria was implemented to evaluate proposed project alternatives
- Evaluation Tools, including:
  - Level of Traffic Stress Description
  - Summary of the corridor operations analysis tool (Vissim) was developed and calibrated
  - Description of project bundle assumptions used for simulation evaluation
- System Operations Summary Review of the simulation results, including:
  - Future No-Build System Conditions
  - Project Bundle System Conditions
- Level 2 Evaluation Results separated into the following locations
  - Springhill Street/US 20

- o 1<sup>st</sup> Avenue/Lyon Street and Lyon Street Bridge
- 2<sup>nd</sup> and 3<sup>rd</sup> Avenue at Lyon Street
- 1<sup>st</sup> and 2<sup>nd</sup> Avenue at Ellsworth Street
- Downtown Unsignalized Intersections
- o 9th Avenue/Lyon Street/OR 99E
- Ellsworth Street/Lyon Street Bike Facilities
- Recommendations Summary

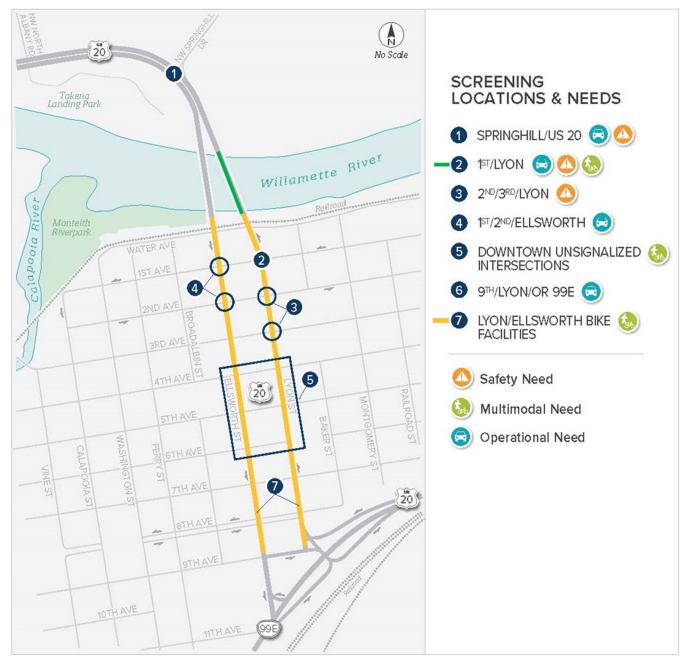


FIGURE 1: SCREENING LOCATIONS AND NEEDS

## **EVALUATION CRITERIA**

This section outlines the two-tiered screening and evaluation process used to develop and refine proposed projects for the US 20 corridor.

## TIER 1 SCREENING

The first screening applied a simplified, qualitative version of the project evaluation criteria that was developed by the PMT to align with the goals and objectives that guide this planning process. Each proposed project alternative was evaluated using the following performance measures:

- Motor Vehicle Operations
- On-Street Parking
- Pedestrian Benefit
- Bicycle Benefit
- Transit Benefit
- Turning Impacts/Driveway Access
- Safety
- Cost

A handful of alternatives that had a negative impact or were clearly outperformed by similar and lower cost alternatives were removed during the Tier 1 screening, including curb extensions throughout the corridor and a transit-only approach at Albany Transit Center.

### **LEVEL 2 EVALUATION**

Each advanced project alternative was evaluated against the Level 2 Evaluation criteria using the performance measures outlined in Table 1. Each criterion is a more comprehensive assessment of potential benefits and trade-offs associated with project alternatives using a combination of qualitative and quantitative analysis.

#### TABLE 1: LEVEL 2 EVALUATION CRITERIA

EVALUAT	ION CRITERIA	PERFORMANCE MEASURE	EVALUATION METHOD
MOTOR VEHICLE	Increases/reduces travel times	US 20 Corridor PM Peak Hour Travel Times (minutes)	Vissim
OPERATIONS	Increases/reduces queue lengths for major movements	PM Peak Hour Queue lengths for major movements	Vissim

EVALUATION CRITERIA		PERFORMANCE MEASURE	EVALUATION METHOD
	Increases/reduces delay and volume-to-capacity Int (v/c) relative to rat Operating Standards		Vissim – Delay Synchro – v/c
MOTOR VEHICLE OPERATIONS	Increases/reduces the risk of neighborhood cut through traffic	Unserved PM peak period demand by intersection approach	Vissim
	Increases/reduces congestion in Downtown or North Albany	PM Peak Period System Delay per vehicle	Vissim
	Increases/reduces number of on-street parking stalls	Change in street parking spaces	Quantitative Assessment based on Conceptual Layout
ON-STREET PARKING IMPACT	Increases/reduces number of on-street parking spaces in downtown business district	Change in street parking spaces in downtown business district	Quantitative Assessment based on Conceptual Layout
	Increases/reduces pedestrian crossing timing	Change in crosswalk length (ft)	Quantitative Assessment based on Conceptual Layout
PEDESTRIAN FACILITIES	Increases/reduces sidewalk width	Change in sidewalk width (ft)	Conceptual layout
	Increases/reduces estimated number of conflict points	Change in pedestrian/vehicle conflict points	Conceptual layout
BICYCLE FACILITIES	Increases/reduces bicycle safety/connectivity between specified locations	Change in Bicycle LTS caused by project	LTS Analysis
	Increases/reduces bicycle travel time between specified locations	Change in PM Peak Period Bicycle Travel time on US 20 Corridor	Vissim

EVALUATION CRITERIA		PERFORMANCE MEASURE	EVALUATION METHOD
TRANSIT FACILITIES	Increases/reduces transit travel times between specific destinations	Change in PM Peak Period Transit Travel time on US 20 Corridor	Vissim
TRANSIT FACILITIES	Enhances/degrades accessibility to transit facilities	Qualitative measure	Qualitative measure from Conceptual layout
PROPERTY IMPACTS/ACQUISITION	Estimated property/right of way acquisition	Estimate ROW needed (sq ft)	Conceptual layout
MAINTAIN/ENHANCE EMERGENCY VEHICLE ACCESS AND RESPONSE	Ability to accommodate emergency vehicle access and projected reduction in emergency vehicle response times	Qualitative measure	Qualitative measure from Conceptual layout
	Median restrictions	Length (ft) of medians with limitations	Quantitative Assessment based on Conceptual Layout
TURNING CONFLICTS/DRIVEWAY ACCESS	Driveways Impacts	Number of driveways impacted	Quantitative Assessment based on Conceptual Layout
	Increases/reduces out-of- direction travel (projected vehicle hours of delay)	Projected PM Peak Period vehicle hours of delay	Vissim
SAFETY	Increases/reduces estimated number of crashes per year	Expected change in crashes ODOT CRF due to project	
IMPACTS TO PARKS	Creates/reduces park areas	Estimated Park area impacted (sq ft)	Quantitative Assessment based on Conceptual Layout

 $<sup>^1</sup>$  ODOT CRF List (January 2023) full access online: https://www.oregon.gov/odot/Engineering/ARTS/CRF-List.xlsx

EVALUATION CRITERIA		PERFORMANCE MEASURE	EVALUATION METHOD
	Increases/reduces visual appearance	Qualitative measure	Qualitative measure from Conceptual layout
	Creates/reduces landscaping coverage	Qualitative measure	Qualitative measure from Conceptual layout
IMPACTS TO LANDSCAPING	Street tree impacts	Number of street trees removed	Quantitative Assessment based on Conceptual Layout
COMMUNITY LIVABILITY	Improves/degrades multi- modal access to downtown business district and/or North Albany	Change in Pedestrian and Bicycle LTS caused by project	LTS Analysis/Conceptual layout
ECONOMIC VITALITY	Projected vehicle hours of delay	PM Peak Period system vehicle hours of delay	Vissim microsimulation
CONSISTENCY WITH CITY/STATE STANDARDS	Does the proposed alternative require a design exception?	Qualitative measure	Qualitative Assessment
IMPACTS TO HISTORICAL RESOURCES	Avoid or minimize adverse permanent and temporary impacts to identified historical resources	Qualitative measure	Qualitative Assessment
IMPACTS TO CULTURAL RESOURCES	Likelihood of adverse impact to cultural resources	Qualitative measure	Qualitative Assessment
IMPACTS TO ENVIRONMENTAL RESOURCES	Increases impacts to environmental resources	Qualitative measure	Qualitative Assessment
SOCIETAL BENEFITS	Overall benefits (safety, economic, environmental, etc.)	Qualitative measure	Qualitative Assessment
PROJECT COST	Estimated Cost	Estimated Improvement Capital Cost in 2023 dollars	Quantitative Assessment

Note that the level of traffic stress (LTS) was analyzed for proposed pedestrian and bicycle facilities in the study area using methodology from the ODOT Analysis and Procedures Manual (APM). LTS rates the stress of roadway segments based on characteristics such as motor vehicle traffic volumes and speeds, presence of walking and bicycling facilities, and degree of separation between motorized and nonmotorized users. The possible scores range from 1 to 4, with 1 representing the lowest stress and 4 representing the highest stress.

Each improvement project considered in the Level 2 Evaluation was analyzed against all applicable criteria from Table 1. The results of the applicable performance measures evaluated for alternative were rolled up into the main categories (Motor Vehicle Operations, On-Street Parking Impacts, Bicycle Facilities, etc.) and identified as:

- Significant Benefit (++) At least one performance measure changed from not meeting (No-Build conditions) to meeting standards or improved by 25% or more.
- Some Benefit (+) Most performance measures showed improvement, but none met the "Significant Benefit" thresholds.
- Significant Impact (--) At least one performance measure changed from meeting (No-Build conditions) to not meeting standards or degraded by 25% or more.
- Some impact (-) Most performance measures showed impacts, but none met the "Significant Impact" thresholds.
- No Change no discernable change in any performance measures for the category

### **EVALUATION TOOLS**

The methods and application of the tools used to evaluate the majority of the quantitative performance measures outlined in the prior section were summarized in the Existing and Future Baseline Conditions Memorandum. This memorandum includes descriptions of the Highway Capacity Manual (HCM) analysis performed with Synchro, the development of future year traffic forecasts, and the safety analysis methods. This memorandum addresses the additional tools used to complete the Level 2 Evaluation.

### LEVEL OF TRAFFIC STRESS (LTS)

The level of traffic stress (LTS) was analyzed for proposed pedestrian and bicycle facilities in the study area using methodology from the ODOT Analysis and Procedures Manual (APM). LTS rates the stress of roadway segments based on characteristics such as motor vehicle traffic volumes and speeds, presence of walking and bicycling facilities, and degree of separation between motorized and nonmotorized users. The possible scores range from 1 to 4, with 1 representing the lowest stress and 4 representing the highest stress.

### **MICROSIMULATION (VISSIM)**

The project team developed a Vissim model for the study corridor, extending from the US/20 North Albany Road intersection southward to the US 20 intersection with OR 99E. The model was calibrated to the 30<sup>th</sup> Highest Hour PM Peak Hour conditions using the seasonally adjusted traffic

counts used for the Highway Capacity Manual (HCM) analysis presented in the Existing and Future Baseline Conditions Memorandum. The model calibration followed the ODOT Vissim Protocol guidelines, aligning corridor travel times, queuing, and traffic throughput at study intersections with Google Travel Time data, field observations, and intersection turn movement counts. The Vissim model included a 4-6 PM analysis period, with 15-minute traffic volume distributions to capture peak hour vehicle arrival profiles. The Vissim model also includes:

- Detailed intersection geometry, including crosswalks and Leading Pedestrian Interval (LPI) signal phasing
- Unsignalized crosswalks along Ellsworth Street and Lyon Street
- Heavy Vehicles (trucks)
- Transit stops and routes for Lines 2, 3, and the US 20 Commuter Line
- Bicycle facilities and bicycle riders, including the sharrows on Ellsworth Street (including the bridge) and Lyon Street
- Trip Origin-Destination (vehicle routing) based on Replica Data

A Future No-Build (year 2043) Vissim model was built from the calibrated Existing conditions model, using the traffic volume forecasts described in the Existing and Future Baseline Conditions Memorandum. This model was validated to ensure the network was performing reasonably and was then used as the basis for comparison against proposed corridor improvements.

The detailed descriptions and results for the Vissim model data, development, existing conditions calibration, and Future No-Build assumptions are included in the Albany US 20 Study Vissim Model Memorandum, which is included as Appendix A of this memorandum.

### **PROJECT BUNDLE DESCRIPTIONS**

Many alternatives passed through the Tier 1 Screening to the Level 2 Evaluation. To better understand the corridor-wide/system level impacts and benefits of these alternatives, three Project Bundles were created to allow the proposed improvements to be analyzed in the Vissim model. These project bundles all include every non-conflicting proposed improvement, i.e. projects that do not preclude any of the other proposed projects. Competing/conflicting projects were distributed across the three project Bundles. Note that project bundles were created for analysis purposes only and are not intended to be considered as "alternatives".

The composition of the project bundles is summarized in Table 2.

LOCATION	#	DESCRIPTION	ANALYSI	ANALYSIS PROJECT BUNDLE	
LOCATION	#	DESCRIPTION	#1	#2	#3
	1A	Re-stripe to allow Dual SBL turn	Х	Х	Х
SPRINGHILL/US 20	1C	SBL Truck Route to US 20 via Hickory	Х		
-	1D	US 20 Superelevation Correction		Х	Х
LYON STREET BRIDGE	2F	2-way multi-use path on Lyon St Bridge	Х	Х	Х
	2C	Dual WBR, Single WBT on 1 <sup>st</sup>	Х		
1 <sup>st</sup> /LYON	2D	WBR + WBTR on 1st		Х	
-	2E	WBR + WBTR, shift bike lane to south side of 1st			Х
1 <sup>ST</sup> & 2 <sup>ND</sup>	4B	Signal Timing Updates	Х	Х	Х
AVE/ELLSWORTH ST	4C	New SBL turn lane at 2 <sup>nd</sup> /Ellsworth	Х	Х	Х
2 <sup>ND</sup> & 3 <sup>RD</sup> AVE/LYON ST	3B	Signal Timing Updates	Х	Х	Х
DOWNTOWN UNSIGNALIZED INTERSECTIONS	6B	RRFBs at $4^{th} \& 5^{th}$ / Ellsworth, $4^{th} \& 5^{th} \& 6^{th}$ /Lyon	х	Х	х
9 <sup>TH</sup> /LYON/OR 99E	5A	Dual northbound 99E Off-Ramp	Х	Х	Х
	7A	2-way cycle track on Lyon (east side)	Х		
CORRIDOR BIKE	7B	1-way cycle track on Lyon & Ellsworth		Х	
FACILITIES	7C	Buffered bike lanes on Lyon & Ellsworth			Х

#### TABLE 2: ANALYSIS PROJECT BUNDLES COMPOSITION

As shown in Table 2, only three locations (Springhill/US 20, 1<sup>st</sup>/Lyon Street, and Ellsworth/Lyon Street Corridor Bike Facilities) have conflicting alternatives, with all other locations including the same proposed improvements across the three analysis project bundles. The proposed improvements at these three locations are the only contributors to differences in the Vissim model system results across the three analysis project bundles.

The three analysis project bundles were coded as three separate scenarios in the Vissim model. Each scenario used the same traffic volume forecasts and vehicle routing assumptions as the Future No-Build scenario. The Vissim coding assumptions for the analysis project bundle scenarios are summarized in the Albany US 20 Study Vissim Model Memorandum (Appendix A).

## SYSTEM OPERATIONS SUMMARY

As noted in the prior section, 2043 PM peak period No-Build and analysis project bundles scenarios were coded and analyzed using the Vissim model. The key system bottlenecks and the analysis project bundles effects on these bottlenecks are summarized in the following sections.

### **FUTURE NO-BUILD SYSTEM CONDITIONS**

Based on the 2043 PM Peak Period Vissim model, the following system bottlenecks were identified along the US 20 corridor with the project Study Area:

- The 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections with Ellsworth Street (US 20) continue to act as a system bottleneck under future (year 2043) traffic conditions. By 4:00 PM, southbound green time constraints at these intersections combines with heavy competing side street traffic demand and causes queues to spill back to the Springhill Drive intersection across the river. These queues compound the queues on the southbound approach of Springhill Drive, which is already attempting to serve traffic demand beyond the intersection capacity. Queues on eastbound US 20 extend back through North Albany Road by 4:45 PM, and beyond the study area extents by 5:15 PM. At 6 PM, despite the traffic demand decreasing from the Peak Hour period, 11% (nearly 200 vehicles) of the eastbound US 20 traffic demand remains queued up beyond the study area extents west of North Albany Road. In addition, 15% (185 vehicles) of the southbound Springhill Drive traffic remains queued beyond the study area. This system bottleneck also results in the Ellsworth Street bridge serving less than 83% of the forecasted future traffic demand from 4-6 PM.
- Eastbound 2<sup>nd</sup> Avenue queues beyond the project study area by 4:00 PM, due to increased conflicts and queuing on the city blocks between 1<sup>st</sup> and 2<sup>nd</sup> Avenue on Lyon Street (which blocks eastbound left turns from 2<sup>nd</sup> Avenue) and queues between Ellsworth and Lyon Street on 2<sup>nd</sup> Avenue. The combined impacts of these queues, which are caused in large part by signal timing prioritized to progress the US 20 through movements on Lyon Street and Ellsworth Street, result in sustained queues on 2<sup>nd</sup> Avenue eastbound that fail to dissipate by 6:00 PM, leading to 14% (approximately 170 vehicles) of unserved vehicle demand on this approach.
- The 1<sup>st</sup> Avenue and Lyon Street intersection continue to act as a critical system bottleneck under 2043 conditions, with the brunt of the capacity constraint impact experienced on the 1<sup>st</sup> Avenue westbound approach. Anticipated increases in bicycle and pedestrian activity at this intersection in the future further limits the westbound right turn capacity (by about 5%), and combined with increased traffic demand on 1<sup>st</sup> Avenue, results in queues that spill back well beyond the study area by 4:00 PM. These queues do not dissipate by 6:00 PM, with 33% (nearly 600 vehicles) remaining in queue and unserved. Indirectly, the constraint benefits northbound travel on Lyon Street in the model, but this highlights a larger corridor concern, as this level of queuing is not considered a realistic future condition, with drivers likely to search for other routes to access Lyon Street. This would cause more traffic on side streets such as 3<sup>rd</sup> and 4<sup>th</sup> Avenue, along with heavier usage of the OR 99E southbound off-ramp to Lyon Street, creating long queues Lyon Street, OR 99E southbound, 1<sup>st</sup> Avenue westbound, 3<sup>rd</sup> Avenue

westbound, and 4<sup>th</sup> Avenue westbound. This system bottleneck also results in the Lyon Street bridge only serving 90% of the forecasted future traffic demand from 4-6 PM.

- The OR 99E northbound off-ramp queues back to the mainline by 4:15 PM and does not begin to clear until 6:00 PM.
- System wide, the key bottlenecks described in this section increase the average delay per vehicle within the study area from 1.5 minutes to 9.7 minutes, a nearly 650% increase from present day to year 2043 conditions.

The 2043 No-Build Vissim simulation results tabulating and graphically presenting the summarized system bottleneck information are included in the appendices of the Albany US 20 Study Vissim Model Memorandum, which is included as Appendix A of this memorandum.

## **PROJECT BUNDLE SYSTEM CONDITIONS**

The project bundles outline in the prior section of this memorandum were analyzed for 2043 PM peak period conditions. The changes to the system bottlenecks described for the 2043 No-Build conditions are summarized as follows:

- All three bundles improve the operations at the 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections with Ellsworth Street (US 20) due to the added southbound left turn land at 2<sup>nd</sup> Avenue and Ellsworth and increased southbound green time at 1<sup>st</sup> Avenue and Ellsworth. The Ellsworth Street queues do not spill back to Springhill Drive until about 5:30 PM, minimally impact the southbound left turn at Springhill Drive, and are dissipating by 6:00 PM. The southbound US 20 demand crossing the Ellsworth Street bridge is fully served in all the project bundles, with approximately 500 more vehicles successfully crossing from 4-6 PM compared to No-Build conditions.
- The combined benefits of the re-striped second southbound left turn lane and the reduced downstream queuing on Ellsworth Street reduce the queuing on southbound Springhill Drive across all the project bundles, with the 4-6 PM traffic demand fully served, 185 more vehicles than under the No-Build condition.
- The increased southbound throughput on the Ellsworth Street Bridge (15% increase over No-Build conditions) with all the project bundles exposes additional bottlenecks further to the south, particularly at the 9<sup>th</sup> Avenue/Lyon Street/OR 99E intersection. The queues from this bottleneck extend north through 4<sup>th</sup> Avenue by 5:30-5:45 PM across the project bundles but begin to dissipate by 6:00 PM.
- The three proposed alternatives for the 1<sup>st</sup> Avenue and Lyon Street intersection all improve the westbound right turn queues on 1<sup>st</sup> Avenue over No-Build conditions, serving the entire 4-6 PM traffic demand for this movement, nearly 600 more vehicles than No-Build conditions. The exclusive dual right turn alternative evaluated in Project Bundle 1 provides the shortest queues and least delay on 1<sup>st</sup> Avenue. However, the improved 1<sup>st</sup> Avenue operations result in the worst queuing performance (of the project bundles) on 2<sup>nd</sup> Avenue, as both 1<sup>st</sup> and 2<sup>nd</sup> Avenue vehicles are competing for the same limited capacity on the Lyon Street bridge. The alternative with a westbound right turn and shared through-right configuration coupled with a shift of the existing bike lane to the south side of 1st Avenue results in the most balanced operations across the 1<sup>st</sup> Avenue, 2<sup>nd</sup> Avenue, and Lyon Street approaches to the Lyon Street Bridge.
- The improved capacity at the 1<sup>st</sup> Avenue and Lyon Street intersection across all the project bundles results in increased throughput on the Lyon Street Bridge, with 500 more vehicles

crossing the bridge from 4-6 PM compared against No-Build conditions. These additional vehicles expose the bottleneck at the westbound US 20 approach to the Springhill Drive intersection. The westbound right turn operates nearly at free flow capacity and draws heavy demand. The storage for this movement is limited and westbound through queues often spill back far enough to block the right turn bay opening during red phases. While the dual southbound left turn striping allows for shorter conflicting phases at this intersection, the limited right turn storage still creates a bottleneck issue, as westbound US 20 queues propagate very rapidly across the bridge under these queuing conditions. These queues spill back down Lyon Street and extend to 9<sup>th</sup> Street/OR 99E from 4:45-5:15 PM before beginning to dissipate.

- The improvement to the OR 99E northbound off-ramp provides independent benefit to the 9<sup>th</sup> Avenue/Lyon Street/OR 99E intersection, but the combination of queuing impacts from westbound US 20 at Springhill Drive and increased southbound throughput at 2<sup>nd</sup> Avenue and Ellsworth Street lead to additional queuing at this intersection compared to No-Build conditions within the Vissim model. However, the amount of side street queuing on 1<sup>st</sup> Avenue under No-Build conditions indicate that more vehicles would shift to OR 99E to access the Lyon Street Bridge, likely resulting in much worse operations at the 9<sup>th</sup> Avenue/Lyon Street/OR 99E intersection compared to the project bundles conditions.
- Based on the Vissim analysis of the project bundles, all three Lyon Street and Ellsworth Street bicycle facility alternatives have minimal impacts on the overall corridor operations, including operations at the system bottlenecks.
- System wide, the benefits of the improvements incorporated into the project bundles decreases average PM peak period vehicle delay across the corridor from 9.7 minutes to 3.2-4.4 minutes for the project bundles.

The 2043 Project Bundle Vissim simulation results tabulating and graphically presenting the summarized system bottleneck information are included in the appendices of the Albany US 20 Study Vissim Model Memorandum, which is included as Appendix A of this memorandum.

### **LEVEL 2 EVALUATION RESULTS**

The Level 2 Evaluation results are summarized by location in the following sections, as shown below:

- Springhill Drive/US 20
- Lyon Street Bridge
- 1<sup>st</sup> Avenue/Lyon Street
- 2<sup>nd</sup> and 3<sup>rd</sup> Avenue at Lyon Street
- 1<sup>st</sup> and 2<sup>nd</sup> Avenue at Ellsworth Street
- Downtown Unsignalized Intersections
- 9th Avenue/Lyon Street/OR 99E
- Ellsworth/Lyon Street Bike Facilities

Each section focuses on the performance of the improvements evaluated against the Level 2 Evaluation criteria. The layouts for each proposed alternative are included in Appendix C of this memorandum.

### **SPRINGHILL DRIVE/US 20**

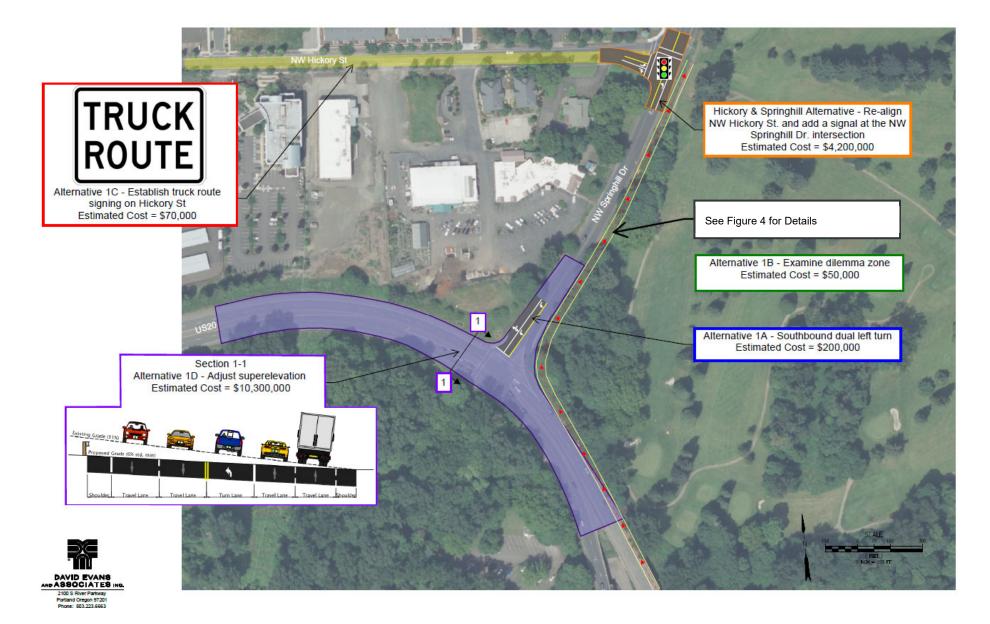
Springhill Drive serves as a key north-south route through North Albany on the west side of the Willamette River to Albany and Corvallis via US 20. In a previously conducted safety study of the corridor (2016), the local community reported experiencing long delays caused by the heavy truck traffic. It was also noted that the US 20 cross slopes (superelevation) of this intersection make it difficult to turn during snow/ice<sup>2</sup>. The existing superelevation is 11%, nearly twice as steep as the 6% needed for the existing curve and roadway design speed. This issue also occasionally leads to semi-trucks rolling over while completing the southbound left turn. Continued housing growth in North Albany has increased the southbound left turn traffic demand considerably, and future growth will continue to push this intersection over the capacity of the current configuration.

## ALTERNATIVES

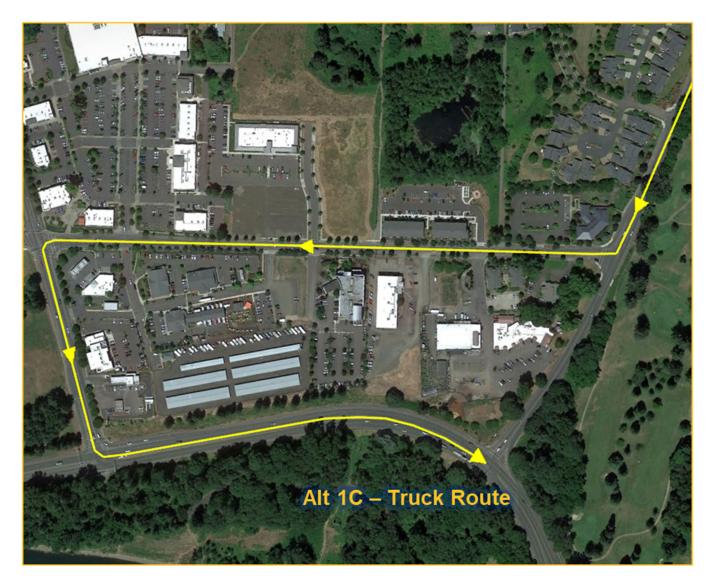
Figure 2 summarizes the improvement projects evaluated against the Level 2 Criteria. The estimated project costs are included as well, along with other recommended improvements that tie in to the proposed alternatives for US 20/Springhill Drive. The alternatives include:

- **1A** Restripe to allow southbound dual left turn lanes on Springhill Drive at US 20.
- **1B** Extend the US 20 dilemma zone for the signal at Springhill Drive.
- **1C** Establish a temporary truck route down Hickory Street to North Albany Road, accommodating the southbound left turn for trucks at US 20 and Springhill Drive (see Figure 3).
- **1D** Adjust the US 20 Superelevation at the Springhill Drive intersection from 11% to 6%.

<sup>&</sup>lt;sup>2</sup> US 20 Highway Safety Study – Corvallis City Limits to Springhill Road, Albany (2016) full access online: https://www.co.benton.or.us/sites/default/files/fileattachments/public\_works/page/4213/us20\_safety\_study\_final\_report \_as\_submitted.pdf



#### FIGURE 2: PROPOSED ALTERNATIVES AT US 20/SPRINGHILL DRIVE



#### FIGURE 3: ALTERNATIVE 1C - TEMPORARY TUCK ROUTE

In addition, a new project was identified for the Springhill Drive and Hickory Street intersection. This project would re-align the Hickory Street leg of the existing intersection to correct the existing skew angle, add a new signal, and enhance the east-west pedestrian crossing to connect the proposed MUP to the planned Hickory Street path. This project is outside the US 20 Project Study Area but is recommended for inclusion in the upcoming City of Albany Transportation System Plan to fill a key active transportation system gap and improve traffic safety at this location.

## LEVEL 2 EVALUATION

The Level 2 Evaluation of the US 20/Springhill Drive alternatives is summarized below. Only criteria applicable to the alternatives were evaluated.

## **Motor Vehicle Operations**

Extending the US 20 signal's dilemma zone (Alternative 1B) is a safety-oriented improvement and is not expected to have any quantified benefits or impacts to motor vehicle operations. Alternatives 1C (Hickory Truck Route) and 1D (US 20 Superelevation Correction) do not significantly impact traffic operations but are necessary to re-stripe southbound Springhill Drive to allow for dual southbound left turns (Alternative 1A).

The PM peak hour intersection delay was evaluated in the Vissim analysis, and the results for these locations are included in the appendices to the Albany US 20 Study Vissim Model Memorandum, which is included as Appendix A to this memorandum. Due to other proposed projects throughout the US 20 corridor, the isolated intersection delay performance measures for these intersections are not directly reflective of the alternatives evaluated at these locations. Implementing the dual left turns provides sufficient capacity to serve the entire southbound Springhill Drive traffic demand under 2043 4-6 PM peak period conditions, improving over No-Build where only 85% of this same demand can enter the intersection. Overall, the improvements to this intersection reduce queueing on Springhill Drive while also reducing red time for US 20 movements and are therefore assumed to contribute to the net decrease in delay for the US 20 corridor system and to improve travel times on the US 20 corridor.

Table 3 summarizes the HCM 2000 based v/c ratios for the two signalized intersections most directly benefiting/impacted by the proposed improvements to US 20/Springhill Drive.

ALTERNATIVE	DESCRIPTION	LOCATION		PM V/C
NO-BUILD	No changes from existing	rom existing North Albany Road/US 20		0.84
ALT 1A+1C	Springhill dual SBL + Truck Route	North Albany Road/US 20	0.85	0.87
ALT 1A+1D	Springhill dual SBL + Superelevation Correction	North Albany Road/US 20	0.83	0.84
NO-BUILD	No changes from existing	kisting Springhill Dr/US 20		1.03
ALT 1A+1C	Springhill dual SBL + Truck Route	Springhill Dr/US 20	0.85	0.85
ALT 1A+1D	Springhill dual SBL + Superelevation Correction	Springhill Dr/US 20	0.86	0.86

#### TABLE 3: US 20/SPRINGHILL DRIVE ALTERNATIVES V/C RATIOS

As shown in Table 3, the truck route (Alternative 1C) degrades the capacity of the North Albany Road intersection while the superelevation correction (Alternative 1D) does not. Overall, the added southbound left turn capacity brings the US 20/Springhill Drive intersection back below capacity under both AM and PM 2043 conditions.

## Safety

All four alternatives provide expected safety benefits at US 20/Springhill Drive. The re-striping of the Springhill Drive approach to allow dual left turns (Alternative 1A+1C or 1D) is expected to decrease crash frequency of all injury crashes reduces by 29%<sup>3</sup>. In addition, the substandard superelevation on US 20 through the intersection increases the risk of overturning crashes for vehicles taking the southbound left turn. Reducing superelevation to the standard minimum, as part of Alternative 1D, can reduce the frequency of overturning crashes.

Within the five-year study period (2017-2021), 29 of the 34 intersection crashes observed at US 20/Springhill Drive were rear-ends. The extended dilemma zone on US 20 is expected to reduce this specific crash type by granting drivers the appropriate amount of decision time to safely navigate through the intersection.

## **Economic Vitality**

As noted in the Motor vehicle discussion, re-striping to a dual southbound left turn (Alternative 1A) contributes to significant improvements to system delay. However, the truck route on Hickory (Alternative 1C) forces out of direction truck travel and independently impacts economic vitality, particularly when compared against the superelevation correction (Alternative 1D) alternative, which improves truck safety while also allowing the benefits of Alternative 1A.

## **Consistency with City/State Adopted Plans**

A couple of City plans, including the North Albany Refinement Plan and the City's Transportation System Plan (TSP), anticipated this intersection would exceed capacity into the future and had proposed re-striping for a dual southbound left turn.<sup>4</sup> The City's TSP had also proposed adjusting the superelevation to meet standards.<sup>5</sup>

## **Societal Benefits**

The dilemma zone adjustment provides safety benefits, and the combination of the dual southbound left turn with either temporary truck route or the superelevation adjustment enhances motor vehicle operations and reduces congestion at Springhill Drive and North Albany Road. Therefore, all the proposed alternatives provide significant societal benefits.

## **Summary of Level 2 Evaluation**

The Level 2 Evaluation results for the US 20/Springhill Drive intersection alternatives are summarized by anticipated level of benefit/impact in Table 4. Only applicable criteria are included in the table.

<sup>&</sup>lt;sup>3</sup> ODOT CRF List – Countermeasure #H63

<sup>&</sup>lt;sup>4</sup> North Albany Refinement Plan (2003) full access online: <u>https://www.oregon.gov/ODOT/Planning/TPOD/facility\_plan/refinement\_plans/city\_of\_albany\_refinement\_plan\_2003.pdf</u>

<sup>&</sup>lt;sup>5</sup> Abany Transportation System Plan (2010) full access online: <u>https://www.albanyoregon.gov/images/stories/publicworks/engineering/tsp/albanytsp\_022410.pdf</u>

APPLICABLE SCREENING CRITERIA	ALT 1A	ALT 1B	ALT 1C	ALT 1D
MOTOR VEHICLE OPERATIONS	(++)	No Change	(++)	(++)
SAFETY	(++)	(++)	(+)	(++)
ECONOMIC VITALITY	(++)	No Change	(-)	(++)
CONSISTENCY WITH CITY/STATE STANDARDS	(++)	No Change	No Change	(++)
SOCIETAL BENEFITS	(++)	(++)	(+)	(++)
PROJECT COST	\$200,000	\$50,000	\$70,000	\$10,300,000

TABLE 4: US 20/SPRINGHILL DRIVE LEVEL 2 EVALUATION RESULTS SUMMARY

As shown in Table 4, the only alternative with anticipated negative impacts is the temporary truck route on Hickory (Alternative 1C), which is expected to impact truck travel times and cause undesirable freight/passenger vehicle conflicts along the detour route. The benefits of dual southbound left turn (Alternative 1A) are significant at both the intersection and system level under future conditions, but this alternative cannot be implemented without either the Hickory truck route or the US 20 superelevation correction (Alternative 1D). Based on safety and freight benefits, the superelevation correction is preferred over the Hickory truck route and is recommended as a near term solution as soon as funding is available. The Hickory truck route is only recommended as a short-term, temporary solution if funding for the superelevation is not obtained before the US 20/Springhill Drive intersection reaches capacity, at which time the dual left turn lane alternative would be implemented. Given existing safety and motor vehicle conditions at this location, the dual left turn re-striping (Alternative 1A) and adjustments to the US 20 dilemma zone (Alternative 1B) are both considered short-term improvement needs.

## LYON STREET BRIDGE

The Lyon Street Bridge currently provides limited facilities and protection for bicycles and pedestrians. Based on input from City staff and ODOT, the following alternative was evaluated to improve these issues.

### ALTERNATIVES

The only alternative evaluated for this location was a reconfiguration of the Lyon Street bridge deck to include a MUP that continues up Springhill Drive to Hickory Street (Alternative 2F), as shown in **Error! Reference source not found.**. The bridge cross section would include 10-foot MUP with a

vertical concrete barrier beside a 4-foot shoulder, two 12-foot travel lanes, and a 2-foot shy distance from bridge barrier.



## FIGURE 4: LYON STREET BRIDGE ALTERNATIVE

Alternative 2F would fit within the existing bridge deck and would not require any significant changes to the existing structure. Since US 20 is a Reduction Review Route, this improvement would require Mobility Advisory Committee (MAC) approval.

### LEVEL 2 EVALUATION

The Level 2 Evaluation of the Lyon Street Bridge improvement is summarized below. Only criteria applicable to the proposed improvement were evaluated.

## **Pedestrian Facilities**

Pedestrian facilities are significantly benefited by the proposed Lyon Street Bridge MUP (Alternative 2F). An MUP with a buffer reduces the level of stress for people walking to the lowest level.<sup>6</sup>

## **Bicycle Facilities**

<sup>&</sup>lt;sup>6</sup> On a two-lane roadway, 10-15' total buffering width (landscaping, shoulder, and bike lane) needed to achieve PLTS 1, otherwise PLTS 2. For 25 mph roadway, landscaping and/or vertical separation needed for PLTS 1, no buffer or a solid surface buffer result in PLTS 2.

The proposed MUP would significantly enhance safety and comfort for people biking across the river.<sup>7</sup> Bicycle Level of traffic stress on the Lyon Street Bridge would drop from Level 4 to Level 1.

## Safety

The installation of a MUP (Alternative 2F) on the Lyon Street bridge and up to Hickory Street reduces the risk of bicycle/pedestrian crashes by 59%, significantly enhancing safety for bicyclists and pedestrians crossing the river<sup>8</sup>. In addition, the bi-directional MUP allows cyclists to shift from the limited active transportation facilities on the Ellsworth Street bridge over to the improved Lyon Street bridge facilities, further improving safety in the corridor.

## **Community Livability Improvements**

The MUP promotes multi-modal travel, providing a low stress walking and biking connection between North Albany and Downtown Albany.

## **Societal Benefits**

The proposed MUP project improves bicycle and pedestrian safety and comfort for the Willamette River crossing, encouraging shifts away from auto focused modes of travel.

## **Summary of Level 2 Evaluation**

The Level 2 Evaluation results for the Lyon Street Bridge alternative is summarized by anticipated level of benefit/impact in Table 4. Only applicable criteria are included in the table.

### TABLE 5: LYON STREET BRIDGE LEVEL 2 EVALUATION RESULTS SUMMARY

APPLICABLE SCREENING CRITERIA	ALT 2F
PEDESTRIAN FACILITIES	(++)
BICYCLE FACILITIES	(++)
SAFETY	(++)
COMMUNITY LIVABILITY IMPROVEMENTS	(++)
SOCIETAL BENEFITS	(++)
PROJECT COST	\$3,200,000

<sup>&</sup>lt;sup>7</sup> Physically separated bicycle lanes (separated from motor vehicles by landscaped buffers, curbs, bollards, bioswales, onstreet parking or other vertical delineators) are generally classified as BLTS 1. At 25 mph, on-street bike lanes with no separation would need to be  $\geq$  7' to reach BLTS 1, otherwise BLTS 3. If adjacent to a parking lane, the bike lane width in addition to parking with would have to be  $\geq$  15' to reach BLTS 2, otherwise BLTS 3.

<sup>&</sup>lt;sup>8</sup> ODOT CRF List – Countermeasure #BP273

Based on the project benefits identified in the Level 2 Evaluation, the Lyon Street Bridge MUP (Alternative 2F) is recommended for implementation as a near-term project.

#### **1<sup>ST</sup> AVENUE/LYON STREET**

The intersection at 1st Avenue/Lyon Street, which is expected to fail in the next five years, is a critical bottleneck on the corridor. The westbound right turn traffic demand is expected to increase in the future, pushing the intersection well over capacity and creating extensive queuing and delays on both Lyon Street and 1<sup>st</sup> Avenue. In addition, this congestion will lead to more traffic shifting to the Oregon 99E (OR 99E) eastbound off-ramp, and to local streets such as 3<sup>rd</sup> and 4<sup>th</sup> Street. The existing bike facility on 1<sup>st</sup> Avenue essentially terminates in favor of the existing westbound right turn lane at Lyon Street, creating an unsafe condition for cyclists attempting to either access Ellsworth Street to the west or routing north across the river.

#### ALTERNATIVES

The following list of alternatives were considered for this intersection (shown in Figures 5 through 7):

- 2A Close the north crosswalk at Lyon Street and 1<sup>st</sup> Avenue and replace it with a new multi-use path connection under the Lyon Street Bridge and across to Ellsworth Street. ODOT does not support the closure of the north crosswalk at Lyon Street and 1<sup>st</sup> Avenue, so this alternative was only included as an option in case the operational alternatives at Lyon Street and 1<sup>st</sup> Avenue could not function with that crossing in place. As shown in the subsequent evaluation results, these alternatives could function with the crosswalk in place, so Alternative 2A was not evaluated further.
- **2C** Change westbound lane geometry to TH, RT, RT and add a curb extension on the west leg. Add a pedestrian phase to the crossing on the north leg.
- **2D** Remove one westbound approach lane and change lane geometry to TH-RT, RT. Add a curb extension on the west leg. Add a pedestrian/bicycle phase to the crossing on the north leg.
- **2E** Remove one westbound approach lane and change lane geometry to TH-RT, RT. Add a curb extension on the west leg. Shift the bike lane to the south side of 1<sup>st</sup> Avenue and install a bike box on the westbound approach for bikes to cross up to the bridge. Add a pedestrian phase to the crossing on the north leg.

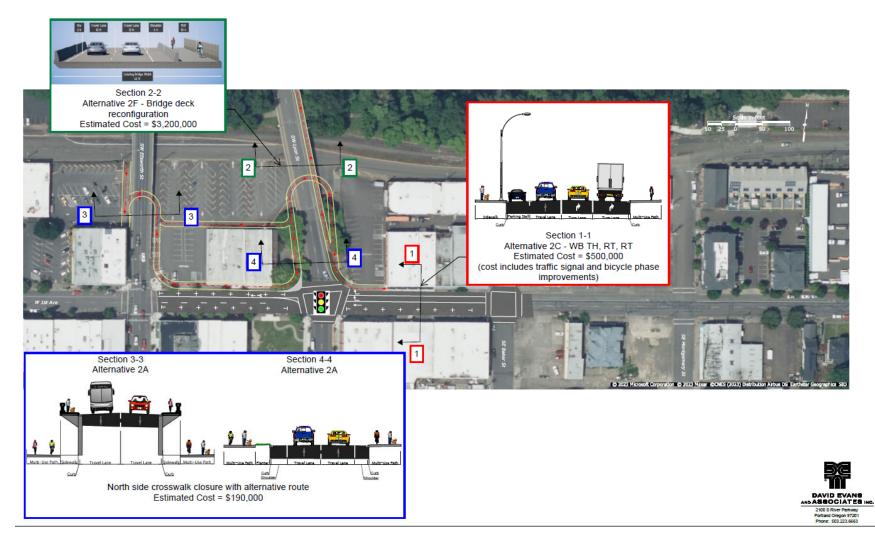


FIGURE 5: LYON ST AND 1ST AVE - ALTERNATIVE 2C

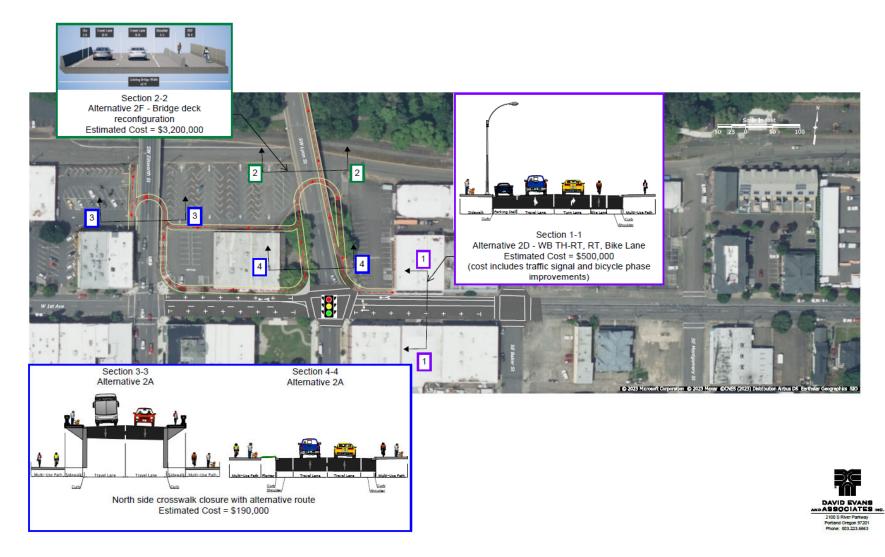


FIGURE 6: LYON ST AND 1ST AVE - ALTERNATIVE 2D

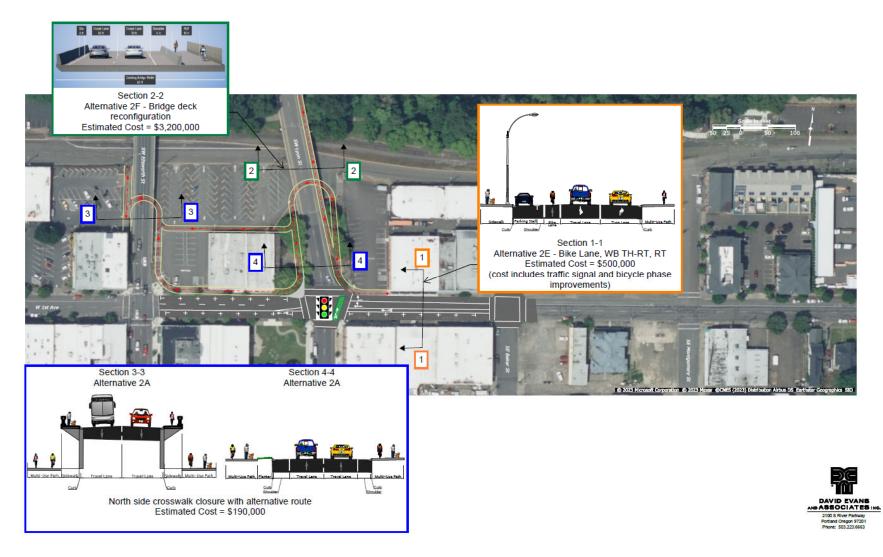


FIGURE 7: LYON ST AND 1ST AVE - ALTERNATIVE 2E

#### **LEVEL 2 EVALUATION**

The Level 2 Evaluation of the Lyon Street/1<sup>st</sup> Avenue intersection alternatives is summarized below. Only criteria applicable to the alternatives were evaluated.

#### **Motor Vehicle Operations**

Under 2043 No-Build conditions, from 4-6 PM only 67% of the forecasted traffic demand for the westbound right turn at Lyon Street/1<sup>st</sup> Avenue was served. All proposed alternatives reduce the 1<sup>st</sup> Avenue westbound through lanes from two to one, re-purposing the existing roadway cross section to better serve the high demand for the westbound right turn.

The PM peak hour intersection delay was evaluated in the Vissim analysis, and the results for the 1<sup>st</sup> Avenue/Lyon Street intersection are summarized in Table 6.

#### TABLE 6: LYON STREET/1ST AVENUE ALTERNATIVES - YEAR 2043 PM PEAK HOUR DELAY

LYON STREET/1 <sup>ST</sup> AVENUE MOVEMENT	NO-BUILD	ALT 2C	ALT 2D	ALT 2E
WESTBOUND RIGHT TURN	670 s/veh	93 s/veh	352 s/veh	370 s/veh
INTERSECTION TOTAL	169 s/veh	33 s/veh	121 s/veh	124 s/veh

As detailed in the prior System Operations Summary section, the exclusive dual right turn lane alternative (Alternative 2C), while providing the best operations for the Lyon Street/1<sup>st</sup> Avenue intersection in isolation, performs worse than the other alternatives along Lyon Street northbound and 2<sup>nd</sup> Avenue eastbound. Alternative 2E provides the best balance in delay between Lyon Street and 1<sup>st</sup> Avenue and has more flexibility in signal timing compared to Alternative 2D due to the bike lane being shifted out of conflict with the westbound right turn movement.

As discussed previously in the System Operations Summary section, all three proposed alternatives provide sufficient capacity to serve the forecasted 2043 PM peak period demand, which significantly improves queueing system wide over No-Build conditions, where only 67% of the westbound right turn demand is served. This lessens the risk of neighborhood cut-through traffic on 3<sup>rd</sup> and 4<sup>th</sup> Avenue. System wide, all three alternatives contribute to decreasing the average delay per vehicle and increasing throughput on the Lyon Street Bridge.

Table 7 summarizes the HCM 2000 based v/c ratios for the alternatives at Lyon Street/1<sup>st</sup> Avenue signal.

ALTERNATIVE	DESCRIPTION	AM V/C	PM V/C
NO-BUILD	No changes from existing	1.03	1.31
ALT 2C	Exclusive dual right turn lanes with protected ped/bike phasing	0.83	1.09
ALT 2D	Right+Through/Right configuration with protected ped/bike phasing	0.88	1.23
ALT 2E	Right+Through/Right configuration with protected ped phasing (bike lane on the south side of $1^{st}$ Avenue	0.87	1.17

#### TABLE 7: LYON STREET/1<sup>ST</sup> AVENUE ALTERNATIVES V/C RATIOS

As shown in Table 7, all three alternatives improve the capacity of the Lyon Street/1<sup>st</sup> Avenue intersection. While none of the alternatives fully meet the intersection mobility standards, all provide a significant upgrade over the forecasted No-Build conditions, with the exclusive dual westbound right turn (Alternative 2C) providing the largest improvement. Shifting the 1<sup>st</sup> Avenue bike lane to the south side of the road reduces conflicts for the westbound right turn, resulting in a more capacity for Alternative 2E compared to Alternative 2D.

## **On-street Parking Impacts**

All proposed alternatives include the removal of five on-street parking stalls along the north side of 1<sup>st</sup> Avenue to maintain sufficient storage for the westbound right turn lanes. The parking spaces are already used as queued vehicle storage during AM and PM peak hour conditions.

## **Pedestrian Facilities**

Alternative 2C would include an exclusive pedestrian phase for the north crosswalk at Lyon Steet/1<sup>st</sup> Avenue, holding the westbound right turn to allow the pedestrians to cross safely. Alternatives 2D and 2E would include an exclusive pedestrian phase for this crosswalk, holding all westbound movements. Alternatives 2E and 2D both provide opportunity for a shorter crosswalk on the east leg of the intersection, and all three alternatives include a pedestrian refuge island on the northwest corner of the intersection, shortening the west leg crosswalk. The existing Leading Pedestrian Interval (LPI) for northbound Lyon Street would be maintained, protecting the west leg crosswalk with time for pedestrians to enter the driver's line-of-sight before vehicles are given a green indication.<sup>9</sup>

## **Bicycle Facilities**

Shifting the bicycle lane to the south side of 1<sup>st</sup> Avenue, as part of Alternative 2E, eliminates the conflict with westbound right-turning vehicles. Additionally, a green bike lane across the east led of the intersection to cross up to the bridge will increase visibility of people on bicycles and reduce

<sup>&</sup>lt;sup>9</sup> FHWA Proven Safety Countermeasures – Leading Pedestrian Interval: https://highways.dot.gov/safety/proven-safetycountermeasures/leading-pedestrian-

interval#:~:text=A%20leading%20pedestrian%20interval%20(LPI,to%20turn%20right%20or%20left.

vehicle encroachment in the dedicated bicycle facility. This alternative is considered significantly beneficial to bicycles.

Alternative 2D maintains a protected bike lane, but still does not completely mitigate the westbound vehicle right turn hook conflict with 1<sup>st</sup> Avenue bicycles traveling through the intersection. Therefore, this alternative is considered somewhat beneficial to bicyclists.

Alternative 2C cannot feasibly contain a bike lane on 1<sup>st</sup> Avenue approaching the intersection, forcing bikes to use the existing sidewalk, which is already constrained by street trees and other obstacles. This is considered a significant impact to bicycles at this location.

## Safety

Improving safety for people biking or walking through this section was a top priority considering seven of the nine bicycle and pedestrian crashes (2017-2021) took place on the Ellsworth Street-Lyon Street couplet between  $1^{st}$  Avenue and  $2^{nd}$  Avenue.

Bicycle/pedestrian crash frequency reduces 55% with a leading pedestrian interval/pedestrian phase, as part of all three alternatives.

Curb extensions, proposed as part of all the alternatives, reduce all crash types by 30%<sup>10</sup>. Shifting the bicycle lane to the south side of 1<sup>st</sup> Avenue, as part of Alternative 2E, eliminates the conflict point with westbound right turns. Plus, urban green bicycle lanes at conflict points reduces bicycle crashes by 39%. Therefore, Alternative 2E is considered a significant safety benefit, while Alternatives 2D and 2C are considered a somewhat significant improvement.

## **Community Livability Improvements**

The improvements to overall bicycle and pedestrian connectivity from Alternative 2D and 2E through this congestion challenged intersection enhances community livability, while the impacts of routing bikes onto the 1<sup>st</sup> Avenue sidewalk negate the other benefits provided by Alternative 2C.

## **Economic Vitality**

As noted in the Motor vehicle discussion, the three alternatives improve delay and queuing for the US 20 corridor, including improvements to freight travel throughout the corridor.

## **Consistency with City/State Adopted Plans**

The City's TSP recommended a similar project at this location, re-striping the westbound approach to allow for a dual right turn movement.<sup>11</sup>

<sup>&</sup>lt;sup>10</sup> ODOT CRF List – Countermeasure #I33

<sup>&</sup>lt;sup>11</sup> Abany Transportation System Plan (2010) full access online: https://www.albanyoregon.gov/images/stories/publicworks/engineering/tsp/albanytsp\_022410.pdf

## **Societal Benefits**

All the proposed alternatives enhance freight, motor vehicle, and transit by reducing congestion, queuing, and delay on the US 20 corridor. In addition, Alternatives 2D and 2E provide improvement for active transportation modes at Lyon Street/1<sup>st</sup> Avenue.

### **Summary of Level 2 Evaluation**

The Level 2 Evaluation results for the Lyon Street/1<sup>st</sup> Avenue intersection alternatives are summarized by anticipated level of benefit/impact in Table 8. Only applicable criteria are included in the table.

APPLICABLE SCREENING CRITERIA	ALT 2C	ALT 2D	ALT 2E
MOTOR VEHICLE OPERATIONS	(++)	(++)	(++)
ON-STREET PARKING IMPACTS	(-)	(-)	(-)
PEDESTRIAN FACILITIES	(+)	(+)	(+)
BICYCLE FACILITIES	(-)	(+)	(++)
SAFETY	(+)	(+)	(++)
COMMUNITY LIVABILITY IMPROVEMENTS	(+)	(+)	(++)
ECONOMIC VITALITY	(++)	(++)	(++)
CONSISTENCY WITH CITY/STATE STANDARDS	(++)	(++)	(++)
SOCIETAL BENEFITS	(+)	(++)	(++)
PROJECT COST	\$500,000	\$500,000	\$500,000

#### TABLE 8: LYON STREET/1<sup>ST</sup> AVENUE LEVEL 2 EVALUATION RESULTS SUMMARY

As shown in Table 8, across the applicable Level 2 Evaluation Criteria, Alternative 2E performs the best, providing the best safety, livability, and bicycle facility benefits. Shifting the bike lane to the south side of 1<sup>st</sup> Avenue is a larger scale project, and Alternative 2D provides many similar benefits without precluding Alternative 2E. Therefore, Alternative 2D is recommended for immediate implementation, while Alternative 2E is recommended as the ultimate solution to address increasing traffic and bicycle demand on 1<sup>st</sup> Avenue. Alternative 2C is not recommended for implementation due to impacts to bicycles on 1<sup>st</sup> Avenue.

## 2ND AND 3RD AVENUE AT LYON STREET

Based on the latest report (2021), this section was identified within the top 15 percent Safety Priority Index System (SPIS) locations in the state. The most recent five years of crash data (2017-

2021) indicates that one of the leading contributors to the many rear ends, angle/turning crashes, and one pedestrian crash resulting in serious injury was disregarding the traffic signal.

## ALTERNATIVES

Alternative **3B**, updating signal timing to better balance green time based on forecasted traffic volume changes, was the alternative evaluated at these intersections. The intersection green times were adjusted to better balance Lyon Street versus side street traffic.

## **LEVEL 2 EVALUATION**

Various signal timing adjustments were tested in Vissim, but these adjustments indicated little to no independent operational benefit to the corridor. The alternatives implemented at Ellsworth Street/2<sup>nd</sup> Avenue and Lyon Street/1<sup>st</sup> Avenue impact operations at these intersections. Therefore, rather than evaluate the individual benefits of signal timing adjustments to these intersections, the recommendation is to re-optimize the signal timing at the Lyon Street signals at 2<sup>nd</sup> and 3<sup>rd</sup> Avenue when recommended improvements at Ellsworth Street/2<sup>nd</sup> Avenue and Lyon Street/1<sup>st</sup> Avenue are implemented.

## **1<sup>ST</sup> AND 2<sup>ND</sup> AVENUE/ELLSWORTH STREET**

The 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections with Ellsworth Street create the critical southbound US 20 bottleneck detailed in the System Operation Summary section of this memorandum. The limited green time for Ellsworth Street at 1<sup>st</sup> Avenue combines with the high southbound left turning volume at 2<sup>nd</sup> Avenue to create Ellsworth Street/US 20 vehicle queues back through N Albany Road. These queues result in 11% of 4-6 PM future eastbound US 20 demand remaining unserved at 6PM. These queuing issues are compounded at 2<sup>nd</sup> Avenue due to the limited queue storage between Ellsworth and Lyon Street, and on Lyon Street between 1<sup>st</sup> and 2<sup>nd</sup> Avenue. Eastbound 2<sup>nd</sup> Avenue quickly becomes congested as traffic on this street competes with northbound Lyon Street traffic, which in turn competes with westbound right turning traffic from 1<sup>st</sup> Avenue. Approximately 14% of the 2<sup>nd</sup> Avenue traffic demand is unserved from 4-6 PM. The 1<sup>st</sup> and 2<sup>nd</sup> Avenue/Ellsworth Street bottleneck limits the capacity of the Ellsworth Street bridge, and growth in future traffic demand (primarily coming from North Albany) is queued back out of the system during the PM peak period. The combined delay times through this section could also cause more eastbound to northbound traffic to shift to local streets such as 3<sup>rd</sup> and 4<sup>th</sup> Avenue.

### ALTERNATIVES

The alternatives considered for this section are shown in Figure 8 and include the following:

- **4B** Upgrade signal timing to adjust the side street split at Ellsworth Street/1<sup>st</sup> Avenue from 25 seconds to 21 seconds by reducing the pedestrian walk time.
- **4C** Add southbound left turn lane at Ellsworth Street and 2<sup>nd</sup> Avenue by removing a half block of parking on both sides of Ellsworth Street between 1<sup>st</sup> and 2<sup>nd</sup> Avenue. Add an exclusive left turn phase and protected pedestrian phase for the east crosswalk. This alternative would likely require public outreach to accustom users to pedestrian activated crossings.



FIGURE 8: ELLSWORTH STREET/2<sup>ND</sup> AVENUE - ALTERNATIVES

## LEVEL 2 EVALUATION

The Level 2 Evaluation of the Ellsworth Street and 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections alternatives are summarized below. Only criteria applicable to the alternatives were evaluated.

## **Motor Vehicle Operations**

The side street signal timing adjustments (Alternative 4B) provides additional southbound green time to Ellsworth Street, increasing the capacity of the Ellsworth Street bridge.

The exclusive southbound left turn lane (Alternative 4C) adds capacity to the Ellsworth Street/2<sup>nd</sup> Avenue intersection. This improvement replaces the LPI with a protected pedestrian phase on the east crosswalk, which adds additional green time to the southbound through movement. The left turn lane increases the intersection capacity, further improving southbound throughput over the Ellsworth Bridge, and decreases queuing and delay on southbound US delay. 2<sup>nd</sup> Avenue eastbound is now able to receive additional green time, improving the queuing on this approach to Ellsworth Street, with only 2-4% of the 4-6 PM future traffic demand unserved, compared to 14% under No-Build conditions. This lessens the risk of neighborhood cut-through traffic on 3<sup>rd</sup> and 4<sup>th</sup> Avenue.

The PM peak hour intersection delay was evaluated in the Vissim analysis, and the results for the Ellsworth Street and 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections are summarized in Table 9.

#### TABLE 9: ELLSWORTH STREET/1<sup>st</sup> and 2<sup>ND</sup> avenue - year 2043 PM PEAK HOUR DELAY

INTERSECTION	NO-BUILD	ALT 4B+4C
ELLSWORTH STREET/1 <sup>ST</sup> AVENUE	670 s/veh	93 s/veh
ELLSWORTH STREET/2 <sup>ND</sup> AVENUE	169 s/veh	33 s/veh

As detailed in the prior System Operations Summary section, the benefits of both the signal timing adjustment (Alternative 4B) and the southbound left turn lane at Ellsworth Street/2<sup>nd</sup> Avenue both contribute to decreased queuing and vehicle delay across the US 20 corridor, particularly for southbound movements. Therefore, the benefits to these performance measures are more extensive than those summarized in Table 9.

Table 10 summarizes the HCM 2000 based v/c ratios for the proposed improvement at the Ellsworth Street/ $2^{nd}$  Avenue signal.

TABLE 10: ELLSWORTH STREET/2 <sup>N</sup>	<sup>o</sup> AVENUE ALTERNATIVE V/C RATIOS
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ALTERNATIVE	DESCRIPTION	AM V/C	PM V/C
NO-BUILD	No change from existing	0.97	0.93
ALT 4C	Added southbound left turn lane with protected ped phase	0.74	0.74

As shown in Table 10, Alternative 4C significantly improves the capacity of the Ellsworth Street/2<sup>nd</sup> Avenue intersection under future forecasted conditions.

### **On-street parking**

A total of three on-street parking stalls will be removed from each side of Ellsworth Street between 1<sup>st</sup> and 2<sup>nd</sup> Avenue to make room for the additional southbound left turn lane as part of Alternative 4C.

### **Pedestrian Facilities**

The proposed southbound left turn lane at the Ellsworth Street/2<sup>nd</sup> Avenue intersection (Alternative 4C) improves pedestrian facilities by providing a protected pedestrian phase for the east crosswalk at this intersection.

### Safety

Upgrading signal timings to include more volume balanced appropriate splits could reduce all crash types by reducing congestion and maximizing vehicle throughout. Similarly, an exclusive left turn lane can improve safety by enhancing motor vehicle operations.

#### **Economic Vitality Benefits**

Both proposed alternatives maximize vehicle throughput and reduce overall congestion and delay.

## **Consistency with City/State Adopted Plans**

The City TSP recommended similar projects, including both signal timing updates and the new southbound left turn lane.

### **Summary of Level 2 Evaluation**

The Level 2 Evaluation results for the Ellsworth Street and 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections alternatives are summarized by anticipated level of benefit/impact in Table 11. Only applicable criteria are included in the table.

#### TABLE 11: ELLSWORTH STREET/1<sup>ST</sup> AND 2<sup>ND</sup> AVENUE LEVEL 2 EVALUATION RESULTS SUMMARY

APPLICABLE SCREENING CRITERIA	ALT 4B	ALT 4C
MOTOR VEHICLE OPERATIONS	(++)	(++)
ON-STREET PARKING IMPACTS	No Change	(-)
PEDESTRIAN FACILITIES	No Change	(++)
SAFETY	(+)	(++)
ECONOMIC VITALITY	(++)	(++)
CONSISTENCY WITH CITY/STATE STANDARDS	(++)	(++)
PROJECT COST	\$20,000	\$250,000

Based on the impacts summarized above for each proposed alternative and their relative cost, both Alternative 4B and 4C should be considered for short-term implementation.

# DOWNTOWN UNSIGNALIZED INTERSECTIONS ( $4^{TH}$ AVENUE, $5^{TH}$ AVENUE, AND $6^{TH}$ AVENUE)

The downtown unsignalized intersections in this section are currently marked with standard crosswalks. However, it is a challenge for bicyclists and pedestrians to cross US 20 due to limited visibility, vehicle congestion, and a long crossing distance.

### ALTERNATIVES

The alternative considered for these intersections is to add Rapid Rectangular Flashing Beacons (RRFBs) on upstream crossings (Alternative 5B). The proposed locations and total estimated cost for the five crossings are shown in Figure 9.





### FIGURE 9: UNSIGNALIZED INTERSECTIONS - ALTERNATIVE 5B

## **LEVEL 2 EVALUATION**

The Level 2 Evaluation of the Downtown Unsignalized Intersections alternatives are summarized below. Only criteria applicable to the alternatives were evaluated.

### **Motor Vehicle Operations**

As crosswalks currently exist at the proposed RRFB crossing locations, little to no impact is foreseen on motor vehicle operations.

### **Pedestrian FACILITIES**

Multiple RRFBs can improve pedestrian travel time within the downtown business district and encourage more linked trips.

## **Bicycle FACILITIES**

Installation of RRFBs drastically improves safety for bicycles crossing the major roadways of Lyon Street and Ellsworth Street.

## **Transit Facilities**

Accessibility to transit facilities is improved by providing low-stress crossings within the downtown business district.

## Safety

Although no bicycle/pedestrian involved crashes were recorded within this segment during the study period, the installation of multiple RRFBs along a corridor can help maintain vehicle speeds low, increase consciousness of multimodal activity presence, and contribute to a low-stress multimodal network.

## **Community livability**

Multimodal activity can be enhanced within the downtown business district by providing low-stress crossings and connectivity.

## **Consistency with City/state Adopted Plans**

This alternative is consistent with the City's adopted plans. The City TSP identified the need for increased frequency of pedestrian crossings on high-volume roadways. A low-stress network within the downtown business district also meets the City's TSP goals to reduce reliance on motor vehicles and provide greater opportunities for linked trips.

## **Social Benefits**

Strategically placed signalized crossings encourage more multi-modal travel and linked trips through the downtown business district by granting multiple safe low-stress crossings.

### **Summary of Level 2 Evaluation**

The Level 2 Evaluation results for the Downtown Unsignalized Intersections alternative is summarized by anticipated level of benefit/impact in Table 12. Only applicable criteria are included in the table.

TABLE 12: UNSIGNALIZED DOWNTOWN INTERSECTIONS LEVEL 2 EVALUATION RESULTS SUMMARY

APPLICABLE SCREENING CRITERIA	ALT 2F
MOTOR VEHICLE OPERATIONS	No Change
PEDESTRIAN FACILITIES	(++)
BICYCLE FACILITIES	(+)
TRANSIT FACILITIES	(+)
SAFETY	(++)
COMMUNITY LIVABILITY	(++)
CONSISTENCY WITH CITY/STATE STANDARDS	(++)
SOCIETAL BENEFITS	(++)
PROJECT COST	\$500,000

In consideration of the benefits described above and relative cost, Alternative 5B should be considered for implementation.

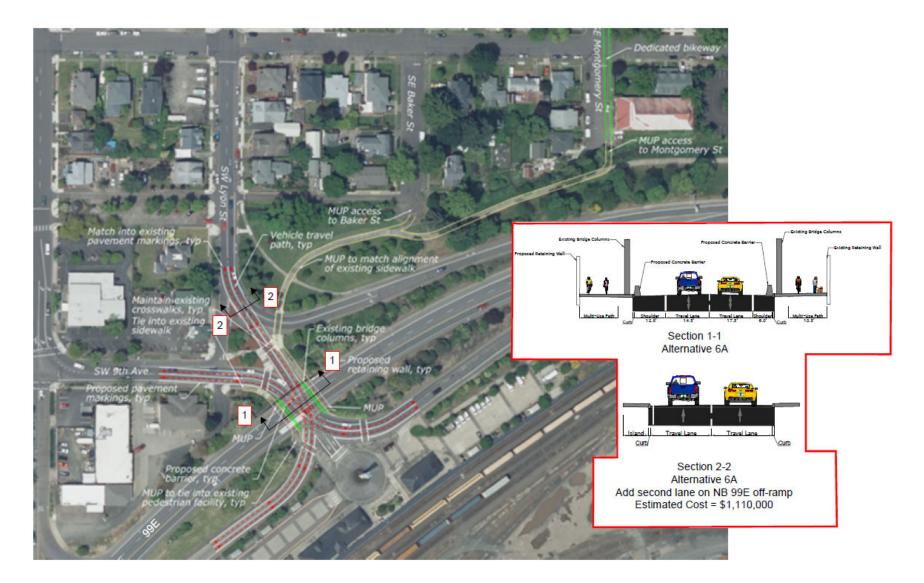
### 9<sup>TH</sup> AVENUE/LYON STREET/OR 99E

This location is one of the projected key bottlenecks in the future no-build scenario. As discussed in the Systems Operations Summary section, traffic operations upstream on Ellsworth Street significantly impact the amount of traffic able to reach this intersection during the PM peak period. The primary identified issue at this location is queue spillback on both OR 99E off-ramps, which receive limited green time during the peak periods.

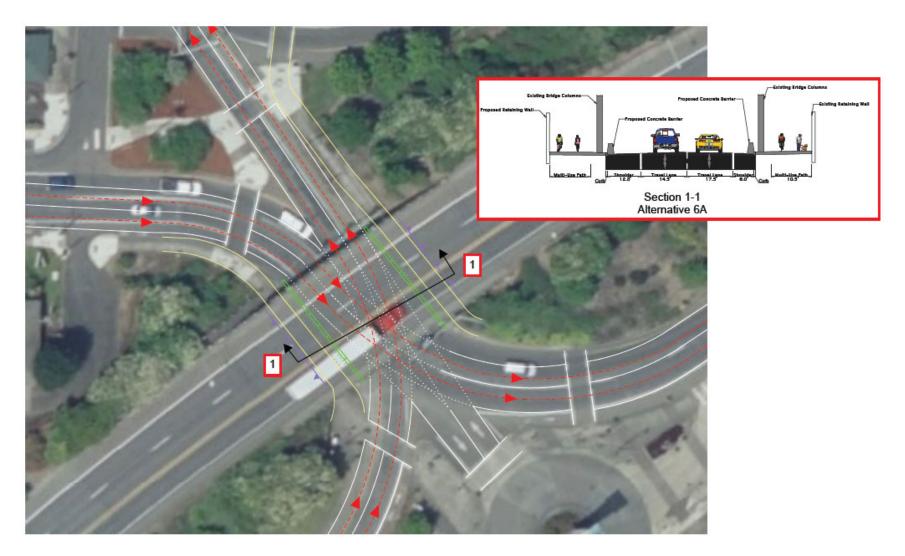
### ALTERNATIVES

The proposed alternative for this location is to add a second lane to the 99E off-ramp that continues through the intersection to northbound Lyon Street. The concept would incorporate MUP on OR 99E overpass providing access to local roadways, including Baker Street and Montogomery Street.

Figure 10 displays an aerial of this segment, including the proposed cross sections for the OR 99E underpass and northbound off ramp, and shows a zoomed in view of the layout through the OR 99E underpass.



#### FIGURE 10: 9TH AVE/LYON ST/OR 99E RAMPS - ALTERNATIVE 6A



#### FIGURE 11: 9TH AVE/LYON ST/OR 99E RAMPS - ALTERNATIVE 6A ZOOMED IN VIEW

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US 20 ALBANY STUDY • LEVEL 2 ALTERNATIVES EVALUATION MEMO • APRIL 2024

#### **LEVEL 2 EVALUATION**

The Level 2 Evaluation of the at 9<sup>th</sup> Avenue/Lyon Street/OR 99E Ramps alternative is summarized below. Only criteria applicable to the alternative were evaluated.

#### **Motor Vehicle Operations**

The additional off-ramp lane helps reduce congestion at this intersection. Adding the 2<sup>nd</sup> lane on the northbound OR 99E Off-Ramp allows for reduced green time for this off-ramp, which is then rebalanced to the other movements at the interchange. The benefits of these changes are summarized in Table 13, which summarizes the HCM 2000 based v/c ratios for the proposed improvement at 9<sup>th</sup> Avenue/Lyon Street/OR 99E Ramps signal.

#### TABLE 13: 9TH AVENUE/LYON STREET/OR 99E RAMPS ALTERNATIVE V/C RATIOS

ALTERNATIVE	DESCRIPTION	AM V/C	PM V/C
NO-BUILD	No change from existing	0.69	1.10
ALT 6A	Dual northbound OR 99E off-ramp	0.55	0.86

The added lane improves the flexibility of the signal timing at the intersection to better manage queue spillback on both OR 99E off-ramps and reduces the risk of neighborhood cut-through travel on 3<sup>rd</sup> and 4<sup>th</sup> Avenue by improving the OR 99E to US 20 regional connection.

## **Pedestrian Facilities**

The concept plan includes a barrier protected mixed use path on both sides of the roadway through the OR 99E underpass. The proposed concrete barrier in addition to the existing bridge columns will provide vertical separation between motor vehicles and users of the MUP on either side of the OR 99E underpass, reducing the Pedestrian LTS to the lowest level.

## **Bicycle Facilities**

The MUP expands connectivity of the bicycle low-stress network between the downtown business district and the Albany Transit Center.

## **Transit Facilities**

Multimodal access to/from the Albany Transit Center is considerably improved with the integration of the MUP on both sides of the overpass.

## Safety

Installation of a MUP significantly reduces conflict points, while bicycle and pedestrian crash risk is expected to decrease by  $63\%^{12}$ .

<sup>&</sup>lt;sup>12</sup> ODOT CRF List – Countermeasure #BP27

#### **Community Livability**

Multimodal connectivity between the downtown business district and/or North Albany is enhanced with MUP tied into the Albany Transit Center. The additional off-ramp lane helps reduce northbound queueing and congestion from OR 99E onto Lyon Street.

#### **Economic Vitality**

The proposed alternative improves capacity at a key regional intersection, benefiting the regional connection between OR 99E and US 20. This will improve truck travel to/from the US 20 corridor, promoting economic vitality for the region.

#### **Consistency with City/state Adopted Plans**

Implementing an MUP leading to the downtown business district and near major destinations meets the City's TSP goals to reduce reliance on motor vehicles and provide greater opportunities for linked trips.

#### **Social Benefits**

The additional off-ramp lane reduces congestion at this intersection, and the MUP enhances bicycle/pedestrian safety while promoting multimodal travel for people with various experience levels.

#### **Summary of Level 2 Evaluation**

The Level 2 Evaluation results for the 9<sup>th</sup> Avenue/Lyon Street/OR 99E Ramps alternative is summarized by anticipated level of benefit/impact in Table 14. Only applicable criteria are included in the table.

APPLICABLE SCREENING CRITERIA	ALT 6A
MOTOR VEHICLE OPERATIONS	(++)
PEDESTRIAN FACILITIES	(++)
BICYCLE FACILITIES	(++)
TRANSIT FACILITIES	(++)
SAFETY	(++)
COMMUNITY LIVABILITY	(++)
ECONOMIC VITALITY	(+)
CONSISTENCY WITH CITY/STATE STANDARDS	(++)
SOCIETAL BENEFITS	(++)
PROJECT COST	\$1,110,000

#### TABLE 14: 9TH AVENUE/LYON STREET/OR 99E RAMPS LEVEL 2 EVALUATION RESULTS SUMMARY

The vehicle capacity issues at this location have not yet occurred but will with expected traffic growth in the future. Therefore, Alternative 6A is recommended for long-term implementation.

#### LYON/ELLSWORTH BICYCLE FACILITIES

Bicycle facilities are proposed along the Lyon-Ellsworth couplet in order to integrate a low-stress network for bicyclists from North Albany to/from the downtown business district. The current bicycle LTS on this corridor is 4 through the couplet because the roadway is shared with a highvolume of motorized vehicles.

#### ALTERNATIVES

The following list of alternatives were considered:

- 7A Install a two-way cycle track on east side of Lyon Street. This option would involve removing landscaping and one parking lane on the east side of Lyon Street. This track would connect OR 99E to the Lyon Street bridge through Albany's downtown area.
- **7B** Install two one-way cycle tracks on one side of Lyon Street and Ellsworth Street. This option requires removal of the parking lanes on the east side of Lyon Street and the west side of Ellsworth Street.
- **7C** Install buffered bike lanes on one side of Lyon Street and Ellsworth Street. This option requires removal of the parking lanes on the east side of Lyon Street and the west side of Ellsworth Street.

**7D** Implement a neighborhood bikeway on Montgomery Street connecting to the Lyon Street bridge via 1<sup>st</sup> Avenue.

Figure 12 summarizes the proposed alternatives considered in the Level 2 evaluation, and Figure 13 through Figure 15 show detail the impacts and costs of the couplet alternatives.



FIGURE 12: LYON/ELLSWORTH STREET BICYCLE FACILITIES - ALTERNATIVES

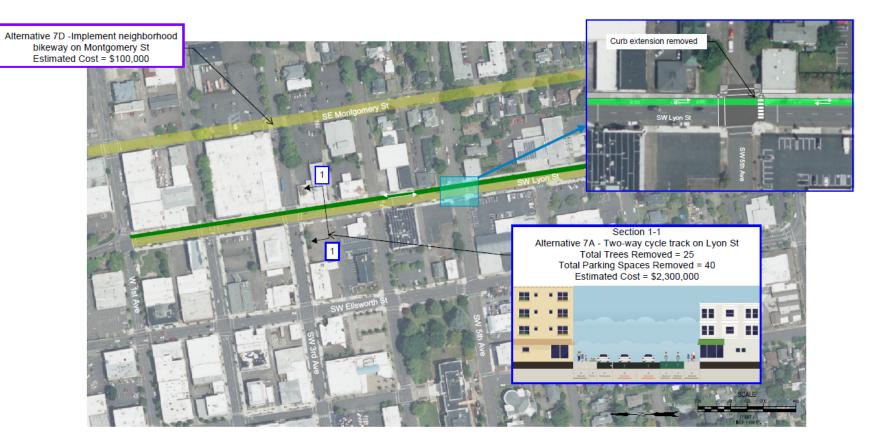


FIGURE 13: ELLSWORTH/LYON STREET BICYCLE FACILITIES - ALTERNATIVE 7A





FIGURE 14: ELLSWORTH/LYON STREET BICYCLE FACILITIES - ALTERNATIVE 7B

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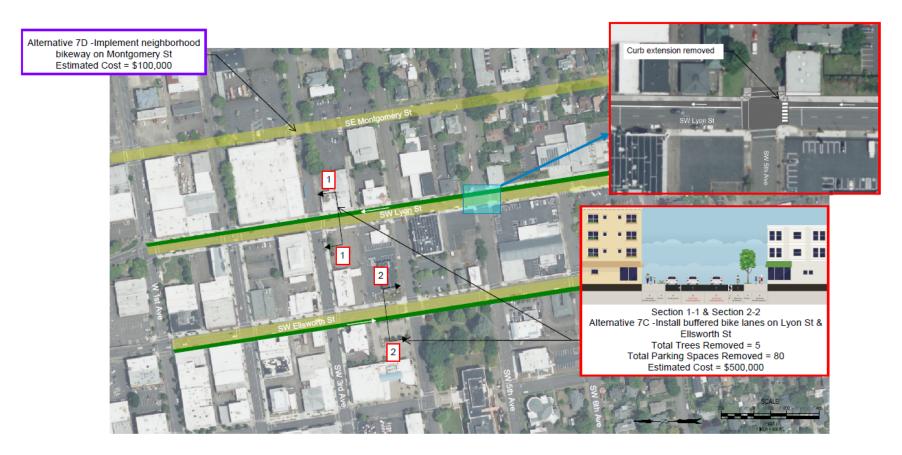


FIGURE 15: ELLSWORTH/LYON STREET BICYCLE FACILITIES - ALTERNATIVE 7C



#### **LEVEL 2 EVALUATION**

The Level 2 Evaluation of the Lyon/Ellsworth Street active transportation facility alternatives is summarized below. Only criteria applicable to the alternatives were evaluated.

#### **Motor Vehicle Operations**

All proposed alternatives on Lyon and Ellsworth Street shift bicycles off the existing shared vehicle lanes, reducing conflicts and improving vehicle travel times. The proposed facilities do not have any anticipated negative operational impacts at the intersections along the couplet.

#### **On-Street Parking**

All proposed alternatives on Lyon and Ellsworth Street would require on-street parking stalls to be removed to grant spacing for bicycle facilities. The two-way cycle track (Alternative 7A) would remove 40 parking spaces along one side of Lyon Street, while the one-way cycle tracks and buffered bicycle lanes (Alternatives 7B and 7C) remove a total of 80 on-street parking spaces.

#### **Bicycle Facilities**

The exclusive bicycle facilities (Alternatives 7A, 7B, and 7C) eliminate conflict points with motor vehicles and overall help increase visibility of multimodal travel through the corridor.

A neighborhood bikeway, as part Alternative 7D, designates the low volume Montgomery Street corridor as a street for bicycle travel priority. This neighborhood bikeway would use signs, pavement markings, and speed and volume management measures to discourage through trips by motor vehicles.<sup>13</sup>

#### Safety

Cycle tracks reduce bicycle crashes of all severities by 59%<sup>14</sup>. Buffered bicycle lanes reduce bicycle crashes of all severities by 47%<sup>15</sup>. Neighborhood greenway applications decrease bicycle and pedestrian crash risk by 63%<sup>16</sup>.

#### **Impacts to Landscaping**

All proposed alternatives on Lyon and Ellsworth Street would require removal of landscaping to grant spacing for continuous facilities. The two-way cycle track (Alternative 7A) would have 25 trees removed, while the one-way cycle tracks and buffered bicycle lanes (Alternatives 7B and 7C, respectively) would remove five trees.

<sup>&</sup>lt;sup>13</sup> NACTO Urban Bikeway Design Guide – Bicycle Boulevards: https://nacto.org/publication/urban-bikeway-designguide/bicycle-boulevards/

<sup>&</sup>lt;sup>14</sup> ODOT CRF List – Countermeasure #BP23

<sup>&</sup>lt;sup>15</sup> ODOT CRF List – Countermeasure #BP24

<sup>&</sup>lt;sup>16</sup> ODOT CRF List – Countermeasure #BP27

#### **Community Livability**

All proposed alternatives lead to the proposed MUP at 9<sup>th</sup> Avenue/Lyon Street leading to the Albany Transit Center. Alternative 7A provides the most direct connection to this MUP, limiting the amount of turns bicycles are required to make to complete the US 20 corridor route.

#### **Consistency with City/state Adopted Plans**

These proposed alternatives meet the City's TSP goals to reduce reliance on motor vehicles and provide greater opportunities for linked trips between North Albany and the downtown business district.

#### **Social Benefits**

All of the proposed alternatives enhance bicycle/pedestrian safety while promoting multimodal travel for people with various experience levels.

#### **Summary of Level 2 Evaluation**

The Level 2 Evaluation results for the US 20/Springhill Drive intersection alternatives are summarized by anticipated level of benefit/impact in Table 15. Only applicable criteria are included in the table.

# TABLE 15: LYON/ELLSWORTH STREET ACTIVE TRANSPORTATION FACILITIES LEVEL 2EVALUATION RESULTS SUMMARY

APPLICABLE SCREENING CRITERIA	ALT 7A	ALT 7B	ALT 7C	ALT 7D
MOTOR VEHICLE OPERATIONS	(+)	(+)	(+)	No Change
ON-STREET PARKING	(-)	()	()	No Change
BICYCLE FACILITIES	(++)	(++)	(++)	(++)
SAFETY	(++)	(++)	(+)	(++)
IMPACTS TO LANDSCAPING	()	(-)	(-)	No Change
COMMUNITY LIVABILITY	(++)	(+)	(+)	(++)
CONSISTENCY WITH CITY/STATE STANDARDS	(++)	(++)	(++)	(++)
SOCIETAL BENEFITS	(++)	(++)	(+)	(++)
PROJECT COST	\$2,300,000	\$2,700,000	\$500,000	\$100,000

As shown in Table 15, all four alternatives provide significant benefits to the community. Alternative 7D does not conflict with the other alternatives and is recommended for near-term implementation. Alternatives 7A, 7B, and 7C will all be considered in the upcoming City of Albany Transportation System Plan Update. Note that if Alternative 7B is selected as the ultimate solution, Alternative 7C could be implemented in the near term as Phase 1 of the project with minimal throw-away cost.

# **RECOMMENDATIONS SUMMARY**

Table 16 provides the complete list of project recommendations, broken down by section. These recommendations include priority, defined as follows:

- Short-Term 0-5 years
- Long-Term 5-20 years
- Temporary only implement for <2 years
- Select in TSP Update preferred alternative and implementation timeline to by finalized in the upcoming TSP Update

#### TABLE 16: RECOMMENDED PROJECT FOR IMPLEMENTATION

LOCATION	ALT	DESCRIPTION	PRIORITY	
	1A	Restripe to allow SB dual left turn	Short-Term	
—	1B	Examine dilemma zone	Short-Term	
SPRINGHILL DRIVE/US 20		Establish truck route down Hickory Road to		
STRINGHTEL DRIVE/00 20	1C	North Albany Road to redirect southbound	Temporary	
_		trucks		
	1D	Fix superelevation	Short-Term	
	2D	Change WB lane geometry to TH-Rt, RT,	Short-Term	
_	20	add curb extension on Northeast corner	Shore renn	
1 <sup>ST</sup> AVENUE/LYON STREET AND LYON	2E	Shift bike lane to south side of $1^{st}$ Avenue	Long-Term	
STREET BRIDGE		Reconfigure the bridge deck to include a		
	2F	multi-use path that continues up Springhill	Short-Term	
		Dr to Hickory St		
2ND & 3RD AVE/LYON ST	3B	Adjust signal timing	Short-Term	
	4B	Adjust signal timing	Short-Term	
1ST & 2ND AVE/ ELLSWORTH ST	4C	Remove half block of parking and add left	Short-Term	
	4C	turn lane at 2nd/Ellsworth SB approach	Short-Term	
DOWNTOWN UNSIGNALIZED INTERSECTIONS	5B	Add RRFBs on upstream crossing	Short-Term	
		Widen to dual lanes on OR 99E northbound		
9TH AVE/LYON STREET/OR 99E RAMPS	6A	off-ramp, add in MUPs on both side of the	Long-Term	
KAPIF 5		OR 99E underpass		
	7A	Two-way cycle track on Lyon Street		
LYON-ELLSWORTH COUPLET BIKE	7B	1-way cycle tracks on Lyon and Ellsworth	Select in the	
FACILITIES	7C	Buffered bike lanes on Lyon and Ellsworth	TSP Update	
	7D	Montgomery Neighborhood Bikeway	Short-Term	

# APPENDICES

- **APPENDIX A ALBANY US 20 VISSIM REPORT**
- **APPENDIX B PROPOSED ALTERNATIVES SYNCHRO RESULTS**
- **APPENDIX C ALTERNATIVES SCHEMATICS**
- **APPENDIX D ADDITIONAL ALTERNATIVES ADDENDUM**

# **APPENDIX A - ALBANY US 20 VISSIM REPORT**

DKS ALBANY US 20 CORRIDOR STUDY • LEVEL 2 EVALUATION MEMORANDUM APPENDICES • APRIL 2024



# **TECHNICAL MEMORANDUM**

DATE:	February 14, 2024	
TO:	Rob Emmons   City of Albany Ron Irish   City of Albany	
FROM:	Anders Hart   DKS Associates Aaron Berger, PE   DKS Associates Scott Mansur, PE   DKS Associates	
SUBJECT:	Albany US 20 Corridor Study - Vissim Calibration, Future No- Build, and Project Bundles Analysis Report	Project #23072-000

This memorandum documents the development and calibration of the Existing Conditions PM Peak period Vissim model for the Albany US 20 Study. In addition, this document includes the 2043 No-Build and Build Project Bundles development, validation, and results.

#### **PROJECT DESCRIPTION**

The purpose of the Albany US 20 Corridor Study is to analyze operational and safety improvements for a segment of US 20 within the city of Albany and to develop recommendations for operational, safety, and active transportation solutions along the corridor.

The primary purpose of the project Vissim analysis is to understand and test system impacts and interactions between localized solutions along the US 20 corridor. This model is intended to refine the preferred alternative projects and support the Level 2 Alternatives Evaluation process.

#### EXISTING CONDITIONS MODEL DEVELOPMENT AND CALIBRATION

#### STUDY AREA AND MODEL AREA

The Vissim study intersections are shown in Figure 1. These intersections are the primary locations for volume calibration within the model. The model extents are outlined in Figure 2. The model includes 11 signalized intersections and three unsignalized study intersections. The model also includes driveways that influence the arrival patterns, lane utilization, and queueing at the study

intersections, per the ODOT Vissim Protocol guidelines<sup>1</sup>. Performance measures are reported only for the study intersections.

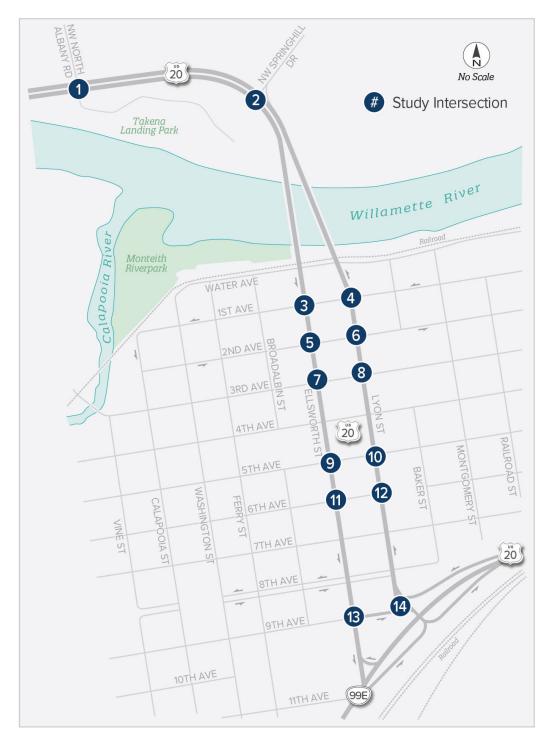


FIGURE 1: STUDY INTERSECTIONS

<sup>&</sup>lt;sup>1</sup> Protocol for Vissim Simulation, June 2011, Oregon Department of Transportation





FIGURE 2: VISSIM MODEL EXTENTS

# DATA COLLECTION SUMMARY

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The following data was collected to develop and calibrate the base year Vissim model:

• **Roadway Geometry Data**: This included roadway segment lengths, number of lanes, lengths of storage bays and tapers, intersection geometry, pedestrian crossing locations and

widths, and transit stop locations. This data was primarily obtained from aerial imagery and Google Street View and was verified with field observations.

- **Traffic Control Data**: This included posted speeds, stop bar and stop sign locations, traffic signal locations, traffic signal timing data, and detector plans. The signal timing data was obtained from ODOT, who maintains all the signals within the model. The remaining data was obtained from aerial imagery and Google Street View and was verified with field observations.
- Traffic Volume Data: PM Peak period (4-6 PM) traffic Count data was compiled for all the Vissim model study intersections to serve as inputs for the existing year PM peak hour Vissim model. Traffic counts were collected on May 3, 2023, and included 5-minute volume profiles. Study intersection traffic count locations, collection dates, and intersection-specific peak hours are shown in Table 1. Bicycle, pedestrian, and heavy vehicle percentage data was also compiled from these counts, which are provided in Appendix A. These counts were balanced and seasonally adjusted to the 30 highest annual hours (30 HV) using a factor of 1.03. The count data indicated a system-wide peak hour of 4:45-5:45 PM. The seasonally adjusted and balanced PM Peak hour volumes at the study intersections are shown in Figure 3. Count data for the Lyon St & 6<sup>th</sup> Ave and SW Ellsworth & 6<sup>th</sup> Avenue intersections were estimated using a combination of estimated volumes and turn percentages from Replica data and May 2023 counts at other locations. Count data for the 2<sup>nd</sup> and 3<sup>rd</sup> Avenue intersections with SW Lyon Street and SW Ellsworth Street were taken from the 2014 Albany Transportation System Plan and factored based on May 2023 counts at other locations.

#	INTERSECTION	DATE COLLECTED	INTERSECTION SPECIFIC PEAK HOUR
1	US 20 & North Albany Rd	Wednesday, May 3, 2022	4:45-5:45 p.m.
2	US 20 & Springhill Dr	Wednesday, May 3, 2022	4:45-5:45 p.m.
3	1 <sup>st</sup> Ave/Ellsworth S (US 20)	Wednesday, May 3, 2022	4:55 p.m5:55 p.m.
4	1 <sup>st</sup> Ave/Lyon St (US 20)	Wednesday, May 3, 2022	4:10-5:10 p.m.
5	2 <sup>nd</sup> Ave/Ellsworth St (US 20)	Factored 2014 counts	N/A
6	2 <sup>nd</sup> Ave/Lyon St (US 20)	Factored 2014 counts	N/A
7	3 <sup>rd</sup> Ave/Ellsworth St (US 20)	Factored 2014 counts	N/A
8	3 <sup>rd</sup> Ave/Lyon St (US 20)	Factored 2014 counts	N/A

TABLE 1: STUDY INTERSECTION COUNT LOCATION, DATE, AND INTERSECTION PEAK HOUR



#	INTERSECTION	DATE COLLECTED	INTERSECTION SPECIFIC PEAK HOUR
9	5 <sup>th</sup> Ave/Ellsworth St (US 20)	Wednesday, May 3, 2022	4:30-5:30 p.m.
10	5 <sup>th</sup> Avenue/Lyon St (US 20)	Wednesday, May 3, 2022	4:25-5:25 p.m.
11	6 <sup>th</sup> Ave/Ellsworth St (US 20)	Estimated (Replica)	N/A
12	6 <sup>th</sup> Ave/Lyon St (US 20)	Estimated (Replica)	N/A
13	9 <sup>th</sup> Ave/Ellsworth St (US 20)	Wednesday, May 3, 2022	4:25-5:25 p.m.
14	9 <sup>th</sup> Ave/Lyon St/OR 99E Ramps	Wednesday, May 3, 2022	4:35-5:35 p.m.







FIGURE 3: EXISTING A.M. AND P.M. PEAK HOUR BALANCED COUNTS

- **Transit Data:** This included bus schedules, headways, and stop locations. Local transit routes within the Vissim model study area include Line 2 (Regular Service East), Line 3 (Regular Service West), and the US 20 Commuter. This data was obtained from the City of Albany website.
- **Field Observations**: The project team performed field observations in the study area during the weekday p.m. peak period<sup>2</sup>. Field observations were used to help verify roadway geometry and traffic control data, as well as to identify queuing issues and areas of congestion.
- Origin Destination (O-D) data development: In addition to the turn movement count data at the study intersections, the Vissim model requires origin-destination (O-D) data to route the traffic through the network (i.e., the origin location and the destination location of each vehicle). This routing information was developed with O-D data from Replica.
- **Queueing Data**: Queue lengths throughout the study area were noted during field observations. In addition, PM peak hour Google Traffic map data was reviewed for the project study area to assess system queueing. This data is saved in Appendix B.

# MODEL DEVELOPMENT SUMMARY

The Vissim model development process used two documents as guidance, including The Federal Highway Administration's (FHWA's) Traffic Analysis Toolbox Volume iii: Guidelines for Applying Traffic Microsimulation Modeling Software<sup>3</sup> and the ODOT Protocol for Vissim Simulation. This section describes the steps completed in the existing (or base) year 2023 PM peak period model development process.

# NETWORK CODING

This step involved coding the geometry of the entire network. Network objects and attributes added in this step include the following:

- 1. Physical roadway (links and connectors)
- 2. Intersection geometry (links and connectors)
- 3. Pedestrian links
- 4. Bicycle links

<sup>&</sup>lt;sup>2</sup> Field observations conducted on Wednesday, August 3, 2023.

<sup>&</sup>lt;sup>3</sup> Traffic Analysis Toolbox Volume III: Guidelines for Applying Traffic Microsimulation Modeling Software, Federal Highway Administration, August 2003.

5. Traffic control (speed distributions and decisions, reduced speed areas, conflict areas, priority rules, stop signs, signal heads, detectors, and signal timing)

Desired speed distributions were developed using the ODOT Vissim protocol methods for links without measured speed data based on posted speed.

# TRAFFIC DEMAND AND ROUTING

The first step in demand development was to develop a Visum model encompassing the extents of the Vissim model, with Traffic Analysis Zones (TAZ) representing all of the network entry and exit points. O-D Matrix Estimation (ODME) was used in this Visum subarea model to develop an O-D matrix based on the PM peak hour balanced turning movement volumes. O-D data from Replica from Fall 2022 (the most recent data available) provided the initial seed trip distribution. The result of this process was a PM peak hour O-D matrix representing the desired routes through the model area and calibrated to the balanced volumes and Replica data.

The O-D data was assigned to the Visum network, which was aligned geometrically with the Vissim model. The vehicle routing information from the Visum model was then exported to the Vissim model as hourly volume inputs and static vehicle routing.

Pedestrian counts were used as pedestrian inputs for all intersections and crossing locations within the Vissim model. Pedestrian counts were rounded up to the nearest 10 to provide a more conservative estimate of pedestrian activity within the model network.

Bicycle routes were used to guide bikes north on Lyon Street and south on Ellsworth Street using the sharrow lanes. Bikes approaching the Ellsworth Street Bridge were given a 50/50 split partial route, with half using the sidewalk and half using the sharrow on the bridge. Bicycle volumes were rounded up to the nearest 10.

# TRAFFIC VOLUME PEAKING PROFILE

The initial PM peak hour volume inputs in Vissim (from the demand development process described above) were modified to include a "peaking profile" of 15-minute volume flow rate increments and extended out to cover the 4-6 PM peak period, as well as a 15-minute seeding period. The peaking profiles were generated based on traffic counts. All input locations with volumes greater than 50 vehicles per hour (vph) were assigned a profile unique to a corresponding traffic count. The traffic counts for all other approaches representing side streets with volumes less than 50 vph were added together and used to develop a typical low volume approach profile for the model. Field observations and traffic counts show that none of the side streets had radically different peaking profiles that would have an impact on corridor operations. The volume profiles used for the model are included in Appendix C.

# **VEHICLE COMPOSITIONS**

The volume inputs included heavy vehicle percentages based on the count data. The heavy vehicle percentages were rounded to the nearest one percent from the existing counts, and the



percentages were applied to the corresponding volume inputs within the model network. The heavy vehicle fleet was modified from the Vissim defaults to be consistent with the ODOT Vissim protocol.

#### SIMULATION PERIOD AND SEEDING PERIOD

The FHWA's Traffic Analysis Toolbox recommends a seeding period equal to or greater than twice the estimated travel time at free-flow conditions to traverse the entire network. The free flow travel time is approximately 3 minutes. To be conservative and allow for the congestion levels and queues to develop to peak conditions, a seeding period of 15 minutes was chosen. The Vissim simulation period included the 15-minute seeding period (initialization period) followed by the entire two-hour analysis period (4-6 PM). The volume rate for the 4:00-4:15 PM period was used for the seeding period flow rate. Measures of effectiveness were collected for the one-hour system peak period.

#### **ERROR CHECKING**

The error checking portion of the model development focused on fixing coding errors before the calibration process began. Error checking is a process that includes a review of the coded data and a review of the animation. All coded data (geometry, speeds, signal timing data, stop and yield controls, transit data, and traffic volumes) was reviewed by the model developer and quality control reviewer.

A review of the animation was conducted to determine locations where conflict areas or priority rules might be missing, where signal timing may not be operating correctly, or any other locations where generally coded parameters may have been overlooked. No significant error messages, such as vehicle input not generating all vehicles or vehicles getting diffused from the network were generated.

#### **CALIBRATION AND VALIDATION**

Upon the completion of the error checking, the Vissim model was calibrated following the traffic volume and travel time calibration criteria in the ODOT Simulation Protocol. Additionally, the model was visually validated against queue observations. The model calibration and validation was based on 10 simulation runs.

The following calibration targets were used for the existing year Vissim model:

- A quantitative comparison between volume data and model outputs aligning with the ODOT Vissim Protocol calibration criteria for traffic volume GEH and travel time target criteria.
- A qualitative comparison (visual inspection and validation) of queuing and general operations along the entire study area based on field observations and Google Traffic Maps of conditions collected during traffic counts.

To best replicate field conditions, the Vissim model calibration process implemented a variety of standard techniques where appropriate, including:

- Lane change distance on turning movement connectors to capture upstream lane positioning, including the following locations:
  - 。 Southbound left turn at Ellsworth Street/2<sup>nd</sup> Avenue Set to 1200 feet
  - Eastbound left turn at Lyon Street/2<sup>nd</sup> Avenue Set to 1500 feet
  - Westbound right turn at Lyon Street/1<sup>st</sup> Avenue Set to 2000 feet
  - Westbound right turn at US 20/Springhill Drive Set to 1500 feet
  - Westbound right turn at US 20/North Albany Road Set to 1500 feet
  - OR 99E northbound on-ramp lane drop Set to 720 feet
- Intersection "keep clear" zones through congested intersections, particularly the 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections with Lyon and Ellsworth Street, and at the 9<sup>th</sup> Avenue/Lyon Street/OR 99E Ramps intersection.
- Increased turning speeds for turning movements with larger than typical radii. The westbound
  right turn movement at Lyon Street and 1<sup>st</sup> Avenue was set to an average speed of 12 mph (for
  non-heavy vehicles rather than the more typical right turn speed of 9 mph, to reflect the wider
  radius of this movement.

The model used the following vehicle driving behaviors:

- "Urban" this driving behavior used the Wiedermann 74 model with default parameters and was applied to all motor vehicle facilities within the model, except for the OR 99E northbound onramp.
- "Merge" this driving behavior used the Wiedermann 99 model with default parameters, with the following adjustments. The safety reduction factor was adjusted to 0.30, and the gap time distribution (CC1) was set to an average of 0.90 seconds. This driving behavior was used for the two to one lane merge section of the northbound on-ramp to OR 99E.
- "Footpath (no interaction)" This driving behavior was applied to pedestrians on crosswalks throughout the model and involves no interaction between pedestrians.
- "Cycle Track (free overtaking)" This driving behavior was used for all bicycle facilities, including for bicycles using the sharrows on the Ellsworth Bridge, Ellsworth Street, and Lyon Street. The overtaking setting allows bicycles to pass other cyclists based on their desired speed.

## VOLUME/DENSITY

The initial calibration target set was for traffic volumes. Per the ODOT Vissim Protocol guidelines, individual turn movements greater than 100 vehicles per hour must be calibrated within an acceptable GEH Statistic<sup>4</sup>. The GEH statistic was calculated for all study intersections. The traffic volume calibration results are documented in Appendix D. The total throughput at all study intersections passed the GEH statistic check. All movements with a volume greater than 100 vehicle per hour also passed the GEH statistic check.

<sup>&</sup>lt;sup>4</sup> The GEH Statistic is a universal measure to compare model inputs and outputs. It is a continuous volume tolerance formula was developed to avoid the pitfalls associated with using a simple percentage comparison of a wide range of volumes.



#### QUEUING

The simulation model was also used to measure delay relative to desired speed as an indicator of queue length. The figures in Appendix D show the relative delay (queues) for each 15-minute interval during the 4:00-6:00 PM analysis period, as averaged over 10 simulations. The colors shown in these figures indicate the following approximate queue states:

- Dark Green = Free flow, no delay
- Light Green = Slight slowing
- Yellow = Increased slowing, but not yet stop and go
- Orange = Furthest extent of stop and go queues
- Red = Fluctuates between low-speed flow and stopped queue
- Dark Red = Stop and go queue during the entire 15-minute peak interval

As part of the calibration process, these maps were compared to the Google Typical Traffic maps and were found to approximate the existing summer traffic trends.

#### **VEHICLE TRAVEL TIMES**

The simulation model was used to measure vehicle travel times between the northern and southern extents. For travel time measurements, the northern extent was located near the US 20 / NW N Albany Road and the southern extent was the OR 99E ramps. Google travel times for weekdays during the 4:45-5:45 PM period<sup>5</sup> were used to validate the model results. As shown in Table 2, the model travel times are within 15% of the observed travel times.

#### TABLE 2: OBSERVED AND MODEL PEAK-HOUR (4:45-5:45 P.M.) TRAVEL TIMES

DIRECTION	AVERAGE PM PEAK HOUR GOOGLE API TRAVEL TIME (SEC)	VISSIM TRAVEL TIME (SEC)	PERCENT DIFFERENCE
NORTHBOUND (OR 99E TO N ALBANY RD)	193	174	-9.9%
SOUTHBOUND (N ALBANY RD TO OR 99E)	298	264	-11.6%

#### **BASE YEAR MODEL MEASURES OF EFFECTIVENESS**

The following measures of effectiveness were collected from the base year model and summarized in Appendix D:

- Average and 95<sup>th</sup> percentile motor vehicle queue lengths
- Vehicle delay

<sup>&</sup>lt;sup>5</sup> Southbound Google travel times were collected on Wednesday, July 26 and Wednesday, August 2 2023 and northbound Google travel times were collected on Wednesday, July 26 and Thursday, July 27 2023.



- Congestion plots
- Latent demand

To calculate 95<sup>th</sup> percentile queues, queue length data was collected from Vissim using queue counters on critical approaches and a 120-second interval to reflect queues that form while traffic flow is impeded. The 95th percentile queue was then calculated using a percentile function. The delay measurements were calculated over the system peak hour interval (4:45-5:45 p.m.) for each simulation run at each signalized study intersection. Delay reported for a study intersection is measured upstream to the next intersection and not through the intersection. Congestion plots were created based on relative speed.

## **EXISTING CONDITIONS CALIBRATION SUMMARY**

As presented in this memo, the existing conditions model meets the calibration targets for volume throughput that GEH for all turn volumes > 100 vph and all model entry/exit locations. Model validation is further confirmed via queuing observations as documented by the Vissim Queue Delay plots (included in Section 4 of the Appendix) compared to the Google Traffic map (included in Section 2 of the Appendix), showing consistent patterns over each 15-minute interval. Based on the information presented in this memorandum, the existing conditions model is calibrated according to the ODOT Vissim Protocol and is ready for use to support the Albany US 20 Corridor Study.

# 2043 NO BUILD

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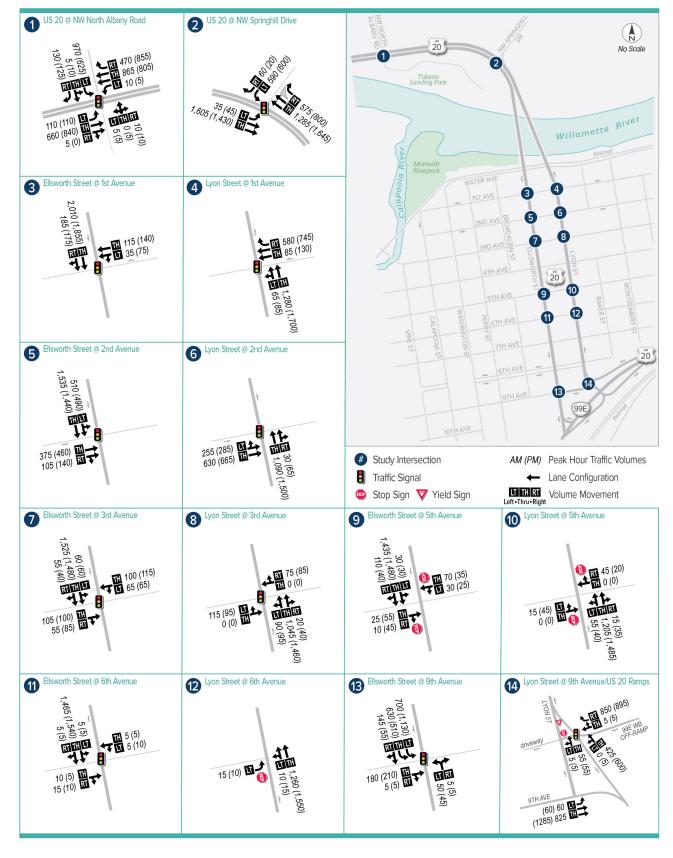
## **NO-BUILD NETWORK ASSUMPTIONS**

The No Build network is identical to the Existing Conditions network, as it is intended to represent future conditions with no projects.

## **NO-BUILD VOLUME DEVELOPMENT**

Future traffic volumes were forecasted for the year 2043 at the project study intersections using 2019 base year and 2043 future year scenarios of the Corvallis Albany Lebanon Model (CALM). The model's 2043 future transportation network included financially constrained projects listed in the Statewide Transportation Improvement Program, the Albany Area Metropolitan Planning Organization (AAMPO) and Corvalis Area Metropolitan Planning Organization (CAMPO) Regional Transportation Plans (RTPs), and the most recent land use assumptions. There were no notable improvements projects in the AAMPO Financially Constrained List project list in the vicinity of the study area that are expected to influence traffic volumes.

Raw link level volumes from the model were post-processed using methodology outlined in NCHRP Report 765: Analytical Travel Forecasting Approaches for Project-Level Planning and Design. The No Build volumes are shown in Figure 4.



#### FIGURE 4: 2043 NO BUILD TRAFFIC VOLUMES

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These forecasted volumes were coupled with the O-D data calibrated for Existing Conditions to run an updated ODME in Visum, developing updated vehicle routing information. This data was again exported back into Vissim as hourly routes and inputs. The same 15-minute peaking profiles as the Existing Conditions model (described in the Model Development Summary section above) were applied to the 2043 volume forecasts.

Pedestrian volumes were increased by 50% and bicycle volumes were increased by 100% from the Existing Conditions to conservatively capture future growth.

#### **NO-BUILD KEY FINDINGS**

The 2043 No-Build PM Vissim model scenario was run for 10 random seeds, and the results were averaged to produce both system level and local intersection performance metrics. These metrics include:

- Unserved demand by input location
- System Measures
- GEH statistics for study intersections
- Intersection Delay
- Queuing Results
- Travel Time Results
- Congestion Plots

Based on these performance measures (included in Appendices E and F) and visual observations of the No-Build simulations, the following system bottlenecks were identified along the US 20 corridor with the project Study Area:

- The 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections with Ellsworth Street (US 20) continue to act as a system bottleneck under future (year 2043) forecast traffic conditions. By 4:00 PM, the constraints to southbound green time at these intersections coupled with heavy competing side street traffic command causes queues to spill back to the Springhill Drive intersection across the river. These queues impact the southbound approach of Springhill Drive, which is independently attempting to serve side street demand beyond the intersection capacity. Queues on eastbound US 20 extend back through North Albany Road by 4:45 PM, and beyond the study Area extents by 5:15 PM. At 6 PM, even with the traffic demand decreasing from the Peak Hour period, 11% (nearly 200 vehicles) of the eastbound US 20 traffic demand remains queued up beyond the study area extends west of North Albany Road, in addition to 15% (185 vehicles) of the southbound Springhill Drive traffic. This system bottleneck also results in the Ellsworth Street bridge serving less than 83% of the forecasted future traffic demand from 4-6 PM.
- Eastbound 2<sup>nd</sup> Avenue queues beyond the project study area by 4:00 PM, due to increased conflicting and queuing on the city blocks between 1<sup>st</sup> and 2<sup>nd</sup> Avenue on Lyon Street, which blocks eastbound left turns from 2<sup>nd</sup> Avenue, and between Ellsworth and Lyon Street on 2<sup>nd</sup> Avenue. The combined queueing impacts of these queues, which are caused in large part by signal timing prioritized to progress the US 20 through movements on Lyon Street and Ellsworth Street, result in sustained queues on 2<sup>nd</sup> Avenue eastbound that fail to dissipate by 6:00 PM, leading to 14% (approximately 170 vehicles) of unserved vehicle demand.

- The 1<sup>st</sup> Avenue and Lyon Street intersections continues to act as a critical system bottleneck under 2043 conditions, with the brunt of the capacity constraint impact felt on the 1<sup>st</sup> Avenue westbound approach. Anticipated increases in bicycle and pedestrian activity at this intersection in the future further limit the westbound right turn capacity (by about 5%), and coupled with increased traffic demand on 1<sup>st</sup> Avenue, result in queues that spill back well beyond the study area by 4:00 PM. These queues do not dissipate by 6:00 PM, with 33% (nearly 600 vehicles) of demand remaining in queue and unserved. Indirectly, the constraint benefits northbound travel on Lyon Street in the model, but this highlights a larger corridor concern, as this level of queuing is not considered a realistic future condition, with drivers likely to search for other routes to access Lyon Street. This would cause more traffic on side streets such as 3<sup>rd</sup> and 4<sup>th</sup> Avenue, along with heavier usage of the OR 99E southbound off-ramp to Lyon Street, creating long queues Lyon Street, OR 99E southbound, 1<sup>st</sup> Avenue westbound, and 4<sup>th</sup> Avenue westbound. This system bottleneck also results in the Lyon Street bridge only serving 90% of the forecasted future traffic demand from 4-6 PM.
- The OR 99E northbound off-ramp queues back to the mainline by 4:15 PM and does not begin to clear until 6:00 PM.
- System wide, the key bottlenecks described in this section increased the average delay per vehicle with the study area from 1.5 minutes to 9.7 minutes, a nearly 650% increase from present day to year 2043 conditions.

#### **NO-BUILD SYSTEM PERFORMANCE MEASURES**

Table 3 compares the Existing Conditions and 2043 No Build system performance measures. It shows that unserved demand, vehicle delay, and average delay per vehicle all are expected to increase dramatically under No Build conditions due to the bottlenecks described previously.

MEASURE	EXISTING (2023)	NO BUILD (2043)	% CHANGE
UNSERVED DEMAND (VEHICLES)	0	1,152	-
IN-SYSTEM DELAY (VEHICLE- HOURS)	274	977	+257%
OUT-OF-SYSTEM DELAY (VEHICLE-HOURS)	0	1,152	-
TOTAL DELAY (VEHICLE-HOURS)	274	2,129	+677%
AVERAGE DELAY/VEHICLE (MINUTES/VEHICLE)	1.5	9.8	+553%

#### TABLE 3: SYSTEM PERFORMANCE MEASURES FOR EXISTING CONDITITIONS AND 2043 NO BUILD

#### **NO-BUILD QUEUING AND DELAY**



Figures showing 2043 No Build average/95<sup>th</sup>-percentile peak-hour and peak-hour average delay are included in Appendix E. The key findings related to queuing and delay are described in the Key Findings Section.

#### **NO-BUILD VEHICLE TRAVEL TIMES**

Table 4 shows the peak-hour corridor travel times for Existing Conditions and 2043 No Build conditions. However, vehicle travel time results are not fully accurate performance measures when large proportions of the vehicle demand go unserved.

DIRECTION	EXISTING (2023)	NO BUILD (2043)	% CHANGE
NORTHBOUND US 20 (SEC)	174	244	+40%
SOUTHBOUND US 20 (SEC)	264	571	+116%

The No-Build vehicle travel time results do not fully capture the corridor congestion, as many vehicles are prevented from even entering the US 20 corridor by the bottlenecks outlined in the Key Findings Section.

#### **NO-BUILD VALIDATION MEASURES**

Full GEH results are found in Appendix E. They show that several movements have high GEH statistics, which aligns with the bottleneck locations discussed above. Key movements unable to serve the full No-Build demand include the westbound right at 1<sup>st</sup> Avenue/Lyon Street, the southbound through at 2<sup>nd</sup> Avenue/Ellsworth Street, and the eastbound through at 2<sup>nd</sup> Avenue/Ellsworth Street.

## PROJECT BUNDLE ANALYSIS

## **PROJECT BUNDLES NETWORK ASSUMPTIONS**

Alternatives 1-3 are "project bundles" with various improvements meant to improve operations and facilitate multimodal safety on the corridor. The following sections describe common and differing projects in each Alternative.

#### **COMMON ELEMENTS ACROSS ALL PROJECT BUNDLES**

All three project bundles included the following changes over the No-Build Vissim model:

- Dual southbound left turn lanes at Springhill Drive
- A two-way multi-use path on the Lyon Street Bridge



- Signal-timing updates at the 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections with Lyon Street and Ellsworth Street (reduce walking time)
- A southbound left turn lane at 2nd Avenue/Ellsworth Street and protected pedestrian phase holding the southbound left turn
- RRFBs at 4<sup>th</sup> and 5<sup>h</sup> Avenues and Ellsworth Street and 4<sup>th</sup>, 5<sup>th</sup>, and 6<sup>th</sup> Avenue and Lyon Street
- Dual northbound lanes on the OR 99E off-ramp

#### **PROJECT BUNDLE 1 ASSUMPTIONS**

The following network changes were made exclusive to Project Bundle 1:

- A truck route along NW Hickory Street to divert southbound trucks away from Springhill Drive to N Albany Road, coded with a added link from Springhill Drive to N Albany Road and a partial route for trucks to re-direct the southbound left turn movement onto N Albany Road
- Dual westbound right turn lanes at 1<sup>st</sup> Avenue/Lyon Street, one westbound through lane, protected bike/pedestrian phase that holds the westbound right turn
- A two-way cycle track on the east side of Lyon Street

#### **PROJECT BUNDLE 2 ASSUMPTIONS**

The following network changes were made exclusive to Project Bundle 2:

- One westbound right lane, one westbound right/through lane, and a bike lane on the north side of 1<sup>st</sup> Avenue at Lyon Street, along with a protected bike/pedestrian phase that holds the westbound approach
- One-way cycle tracks on Lyon Street and Ellsworth Streets (the east and west sides, respectively)

## **PROJECT BUNDLE 3 ASSUMPTIONS**

The following network changes were made exclusive to Project Bundle 3:

- One westbound right turn lane, one westbound right/though lane, and a bike lane on the south side 1<sup>st</sup> Avenue at Lyon Street, along with a protected pedestrian phase that holds the westbound approach
- Buffered bike lanes on Lyon and Ellsworth Streets (the east and west sides, respectively)

## **PROJECT BUNDLES VOLUME DEVELOPMENT**

All alternatives used the same volumes as the 2043 No Build scenario described previously.

#### **PROJECT BUNDLES KEY FINDINGS**

The 2043 Project Bundles 1, 2, and 3 Vissim model scenarios were each run for 10 random seeds, and the results were averaged to produce both system level and local intersection performance metrics. These metrics include:



- Unserved demand by input location
- System Measures
- GEH statistics for study intersections
- Intersection Delay
- Queuing Results
- Travel Time Results
- Congestion Plots

Based on these performance measures (included in Appendices F through J) and visual observations of the Project Bundle simulations, the following changes to the system bottlenecks caused by the projects modeled in the bundles were identified along the US 20 corridor with the project Study Area:

- All three bundles improve the operations at the 1<sup>st</sup> and 2<sup>nd</sup> Avenue intersections with Ellsworth Street (US 20) due to the added southbound left turn land at 2<sup>nd</sup> Avenue and Ellsworth and increased southbound green time at 1<sup>st</sup> Avenue and Ellsworth. The Ellsworth Street queues do not spill back to Springhill Drive until about 5:30 PM, minimally impact the southbound left turn at Springhill Drive, and are dissipating by 6:00 PM. The southbound US 20 demand crossing the Ellsworth Street bridge is fully served in all the project bundles, with approximately 500 more vehicles successfully crossing from 4-6 PM compared to No-Build conditions.
- The combined benefits of the re-striped second southbound left turn lane and the reduced downstream queuing on Ellsworth Street reduce the queuing on southbound Springhill Drive across all the project bundles, with the 4-6 PM traffic demand fully served, 185 more vehicles than under the No-Build condition.
- The increased southbound throughput on the Ellsworth Street Bridge with all the project bundles exposes additional bottlenecks further to the south, particularly at the 9<sup>th</sup> Avenue/Lyon Street/OR 99E intersection. The queues from this bottleneck extend north through 4<sup>th</sup> Avenue by 5:30-5:45 across the project bundles but begin to dissipate by 6:00 PM.
- The three proposed alternatives for the 1<sup>st</sup> Avenue and Lyon Street intersection all improve the westbound right turn queues on 1<sup>st</sup> Avenue over No-Build conditions, serving the entire 4-6 PM traffic demand for this movement, nearly 600 more vehicles than No-Build conditions. The exclusive dual right turn alternative evaluated in Project Bundle 1 provides the shortest queues and least delay on 1<sup>st</sup> Avenue. However, the improved 1<sup>st</sup> Avenue operations result in the worst queuing performance (of the project bundles) on 2<sup>nd</sup> Avenue, as both 1<sup>st</sup> and 2<sup>nd</sup> Avenue vehicles are competing for the same limited capacity on the Lyon Street bridge. The alternative with a westbound right turn and shared through-right configuration coupled with a shift of the existing bike lane to the south side of 1st Avenue results in the most balanced operations across the 1<sup>st</sup> Avenue, 2<sup>nd</sup> Avenue, and Lyon Street approaches to the Lyon Street Bridge.
- The improved capacity at the 1<sup>st</sup> Avenue and Lyon Street intersection across all the project bundles results in increased throughput on the Lyon Street Bridge, with 500 more vehicles crossing the bridge from 4-6 PM compared against No-Build conditions. These additional vehicles expose the bottleneck at the westbound US 20 approach to the Springhill Drive intersection. The westbound right turn operates nearly at free flow capacity and draws heavy demand. The storage for this movement is limited and westbound through queues often spill back far enough to block the right turn bay opening during red phases. While the dual southbound left turn striping allows for shorter conflicting phases at this intersection, the

limited right turn storage still creates a bottleneck issue, as westbound US 20 queues propagate very rapidly across the bridge under these queuing conditions. These queues spill back down Lyon Street and extend to 9<sup>th</sup> Street/OR 99E from 4:45-5:15 PM before beginning to dissipate.

- The improvement to the OR 99E northbound off-ramp provides independent benefit to the 9<sup>th</sup> Avenue/Lyon Street/OR 99E intersection, but the combination of queuing impacts from westbound US 20 at Springhill Drive and increased southbound throughput at 2<sup>nd</sup> Avenue and Ellsworth Street lead to additional queuing at this intersection compared to No-Build conditions within the Vissim model. However, the amount of side street queuing on 1<sup>st</sup> Avenue under No-Build conditions indicate that more vehicles would shift to OR 99E to access the Lyon Street Bridge, likely resulting in much worse operations at the 9<sup>th</sup> Avenue/Lyon Street/OR 99E intersection compared to the project bundles conditions.
- Based on the Vissim analysis of the project bundles, all three Lyon Street and Ellsworth Street bicycle facility alternatives have minimal impacts on the overall corridor operations, including operations at the system bottlenecks.
- System wide, the benefits of the improvements incorporated into the project bundles decreases average PM peak period vehicle delay across the corridor from 9.7 minutes to 3.2-4.4 minutes for the project bundles.

## **PROJECT BUNDLES SYSTEM PERFORMANCE MEASURES**

Table 5 shows the system performance measures for the 2043 and Project Bundles 1-3. All three Project Bundles have significantly lower delay and unserved (latent) demand compared to the 2043 No Build scenario due to the improvement outlined in the Project Bundles Key Findings Section.

MEASURE	NO BUILD	ALT. 1	ALT. 2	ALT. 3
UNSERVED DEMAND (VEHICLES)	1,152	53	89	32
IN-SYSTEM DELAY (VEHICLE-HOURS)	977	628	860	699
OUT-OF-SYSTEM DELAY (VEHICLE-HOURS)	1,152	66	121	45
TOTAL DELAY (VEHICLE-HOURS)	2,129	694	981	744
AVERAGE DELAY/VEHICLE (MINUTES/VEHICLE)	9.8	3.2	4.5	3.4

#### TABLE 5: SYSTEM PERFORMANCE MEASURES FOR NO BUILD AND ALTERNATIVES

#### **PROJECT BUNDLES VEHICLE TRAVEL TIME**

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Table 6 shows that Project Bundles 1-3 have lower southbound travel times compared to the 2043 No Build scenario, but higher northbound travel times. This is due to increased northbound throughput onto Lyon Street bridge in the in the Project Bundles, which, as described in the Project

Bundles Key Findings Section, causes queue spillback along Lyon Street, resulting in increasing travel times relative to the 2043 No Build condition. Full travel time results are found in Appendix J.

DIRECTION	NO BUILD	ALT. 1	ALT. 2	ALT 3
NORTHBOUND US 20 (SEC)	244	305	335	279
SOUTHBOUND US 20 (SEC)	571	356	411	331

TABLE 6. NO BUILD AND ALTERNATIVES 1-3 CORRIDOR TRAVEL TIMES

#### **PROJECT BUNDLES VALIDATION MEASURES**

Peak-hour GEH results for Project Bundles 1-3 are found in Appendices G through I. The GEH measures at the corridor study intersection align with the key bottleneck described in the Project Bundles Key Findings Section.



# **APPENDIX**

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# **APPENDIX A: TRAFFIC COUNTS AND REPLICA ESTIMATES**

**PM PEAK HOUR COUNTS AND REPLICA ESTIMATES** 



LOCATION: NW North Albany Rd -- Albany-Corvallis Hwy (US20) OC JOB #: 16184214 DATE: Wed, May 3 2023 CITY/STATE: Albany, OR Peak-Hour: 4:45 PM -- 5:45 PM 1.3 Peak 15-Min: 5:30 PM -- 5:45 PM ÷ ŧ 6 533 3.1 16.7 1.3 . . € 603 ← 1137 629 🔶 103 🌶 22 - 1 + ▲ 1.3 ← 1.7 769 🜩 0.97 **+** 530 **+** 2.1 2.8 + 0 -872 → 0 🥆 ŧ ŧ ŧ ÷ ŧ Quality Counts Λ DATA THAT DRIVES COMMUNITIES ... . ι. \$ ł þ • • **t** 0 A ÷ 0 7 **f** 0 • ŧ C N/A N/A ÷ و t t ----← N/A N/A N/A N/A a ç ŧ ŧ N/A N/A ŧ NW North Albany Rd NW North Albany Rd Albany-Corvallis Hwy (US20) Albany-Corvallis Hwy (US20) 15-Min Count Period Hourly Totals (Southbound) (Northbound) (Eastbound) (Westbound) Total Beginning At Left Thru Right υ Left Thru Right υ Left Thru Right υ Left Thru Right υ 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM Northbound Southbound Eastbound Westbound Peak 15-Min Flowrates Total Left U Left Right υ Left Right υ Left Thru υ Thru Right Thru Thru Right All Vehicles Heavy Trucks Buses Pedestrians Bicycles Scooters Comments:

Report generated on 5/24/2023 1:17 PM

LOCATION: NW Springhill Dr -- Albany-Corvallis Hwy (US20)/N Lyon St QC JOB #: 16184216 CITY/STATE: Albany, OR DATE: Wed, May 3 2023 Peak-Hour: 4:45 PM -- 5:45 PM 482 2.7 580 1.2 Peak 15-Min: 5:00 PM -- 5:15 PM **↑** 2.6 ŧ ŧ ŧ 0 469 0 13 7.7 . 1131 🗢 39 🌶 € 541 ← 1659 1.9 🗢 5.1 🌶 € 0.9 ← 1.6 0.97 2.4 🜩 **+** 1.9 1271 🜩 **+** 1118 2.5 🔹 0 🥆 1310 → 0 🥆 ŧ ٦ ŧ ſ 0 0 0 0 0 0 ŧ ŧ ÷ ŧ Quality Counts n DATA THAT DRIVES COMMUNITIES 0 0 1 \$ • • **t** 5 AD 0 0 0 **4** 2 0 7 **F** 0 **۴** 0 ŧ 0 0 N/A ÷ t 1 ← N/A N/A 🛥 N/A N/A ⇒ G 1 ₩ 7 ç ŧ ٩ ŧ N/A N/A

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4:05 PM	0	0	0	0	35	0	0	0	3	95	0	0	0	101	43	0	277	
4:10 PM	0	0	0	0	37	0	2	0	6	103	0	0	0	120	46	0	314	
4:15 PM	0	0	0	0	36	0	3	0	0	73	0	0	0	85	45	0	242	
4:20 PM	0	0	0	0	37	0	1	0	4	114	0	0	0	103	42	0	301	
4:25 PM	0	0	0	0	41	0	2	0	4	98	0	0	0	88	38	0	271	
4:30 PM	0	0	0	0	44	0	1	0	5	103	0	0	0	73	41	0	267	
4:35 PM	0	0	0	0	33	0	0	0	3	95	0	0	0	121	51	0	303	
4:40 PM	0	0	0	0	51	0	2	0	2	86	0	0	0	81	30	0	252	
4:45 PM	0	0	0	0	36	0	1	0	3	106	0	0	0	85	36	0	267	
4:50 PM	0	0	0	0	36	0	0	0	3	127	0	0	0	108	45	0	319	
4:55 PM	0	0	0	0	34	0	0	0	2	95	0	0	0	88	36	0	255	3303
5:00 PM	0	0	0	0	49	0	1	0	3	95	0	0	0	85	59	0	292	3360
5:05 PM	0	0	0	0	46	0	2	0	3	100	0	0	0	110	48	0	309	3392
5:10 PM	0	0	0	0	36	0	4	0	2	95	0	0	0	99	49	0	285	3363
5:15 PM	0	0	0	0	43	0	0	0	3	96	0	0	0	93	50	0	285	3406
5:20 PM	0	0	0	0	37	0	1	0	5	112	0	0	0	90	46	0	291	3396
5:25 PM	0	0	0	0	32	0	0	0	5	130	0	0	0	86	49	0	302	3427
5:30 PM	0	0	0	0	44	0	2	0	2	99	0	0	0	90	50	0	287	3447
5:35 PM	0	0	0	0	42	0	0	0	3	105	0	0	0	93	33	0	276	3420
5:40 PM	0	0	0	0	34	0	2	0	5	111	0	0	0	91	40	0	283	3451
5:45 PM	0	0	0	0	29	0	1	0	0	103	0	0	0	94	36	0	263	3447
5:50 PM	0	0	0	0	38	0	2	0	3	109	0	0	0	74	41	0	267	3395
5:55 PM	0	0	0	0	32	0	0	0	2	86	0	0	0	92	33	0	245	3385
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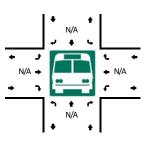
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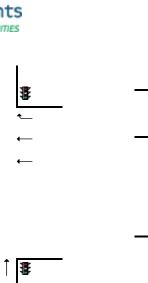
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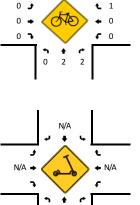
LOCATION: SW Lyon St -- W 1st Ave QC JOB #: 16184212 CITY/STATE: Albany, OR DATE: Wed, May 3 2023 Peak-Hour: 4:10 PM -- 5:10 PM 1670 0 0 Peak 15-Min: 4:55 PM -- 5:10 PM ŧ ÷ **↑** 0 0 0 0 0 . L. . 198 🗢 0 🌶 € 503 ← 622 1.5 🗢 0 🌶 0 🍝 0.95 0 🌩 **+** 119 0 **+** 0 **-€** 0 **→** 0 0 🔸 0 🤉 ► 2.5 ► 0 ŧ 2.4 ŧ Counts 1246 COMMUNITIES 0 0 \$ 0 🖌 4 2 0 •



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N/A

5-Min Count Period		(North				(South	yon St bound)			(Eastb	t Ave ound)			(West	t Ave bound)		Total	Hourly Totals
Beginning At	Left	Thru	Right	U	Left	Thru	Right	U	Left	Thru	Right	U	Left	Thru	Right	U		
4:00 PM	5	101	0	0	0	0	0	0	0	0	0	0	0	11	42	0	159	
4:05 PM	13	91	0	0	0	0	0	0	0	0	0	0	0	12	47	0	163	
4:10 PM	6	103	0	0	0	0	0	0	0	0	0	0	0	8	55	0	172	
4:15 PM	8	95	0	0	0	0	0	0	0	0	0	0	0	16	45	0	164	
4:20 PM	8	96	0	0	0	0	0	0	0	0	0	0	0	12	37	0	153	
4:25 PM	7	85	0	0	0	0	0	0	0	0	0	0	0	13	49	0	154	
4:30 PM	5	75	0	0	0	0	0	0	0	0	0	0	0	5	46	0	131	
4:35 PM	6	116	0	0	0	0	0	0	0	0	0	0	0	12	40	0	174	
4:40 PM	8	94	0	0	0	0	0	0	0	0	0	0	0	8	32	0	142	
4:45 PM	7	90	0	0	0	0	0	0	0	0	0	0	0	12	25	0	134	
4:50 PM	7	98	0	0	0	0	0	0	0	0	0	0	0	3	46	0	154	
4:55 PM	6	83	0	0	0	0	0	0	0	0	0	0	0	8	42	0	139	1839
5:00 PM	4	113	0	0	0	0	0	0	0	0	0	0	0	12	35	0	164	1844
5:05 PM	7	119	0	0	0	0	0	0	0	0	0	0	0	10	51	0	187	1868
5:10 PM	6	101	0	0	0	0	0	0	0	0	0	0	0	11	41	0	159	1855
5:15 PM	8	107	0	0	0	0	0	0	0	0	0	0	0	5	37	0	157	1848
5:20 PM	3	104	0	0	0	0	0	0	0	0	0	0	0	8	33	0	148	1843
5:25 PM	5	91	0	0	0	0	0	0	0	0	0	0	0	12	45	0	153	1842
5:30 PM	5	93	0	0	0	0	0	0	0	0	0	0	0	12	42	0	152	1863
5:35 PM	3	94	0	0	0	0	0	0	0	0	0	0	0	9	44	0	150	1839
5:40 PM	5	89	0	0	0	0	0	0	0	0	0	0	0	7	41	0	142	1839
5:45 PM	11	92	0	0	0	0	0	0	0	0	0	0	0	11	39	0	153	1858
5:50 PM	6	81	0	0	0	0	0	0	0	0	0	0	0	6	39	0	132	1836
5:55 PM	12	71	0	0	0	0	0	0	0	0	0	0	0	3	42	0	128	1825
Peak 15-Min		North	bound			South	bound			Eastb	ound			West	oound		_	
Flowrates	Left	Thru	Right	U	Left	Thru	Right	U	Left	Thru	Right	U	Left	Thru	Right	U	То	tal
All Vehicles	68	1260	0	0	0	0	0	0	0	0	0	0	0	120	512	0	19	60
Heavy Trucks	0	28	Ő	U	Ő	ŏ	Ő	U	0	õ	0	U	0	4	4	U		6
Buses	Ŭ	20	Ŭ		Ŭ	Ŭ	Ŭ		Ŭ	Ŭ	Ŭ		Ŭ					•
Pedestrians		0				0				0				0			(	C
Bicycles	0	4	4		0	0	0		0	Ő	0		0	0	4			2
Scooters	Ū	7	-		Ũ	U	U		Ũ	U	U		Ũ	U	7		1	-
Comments:																		

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Report generated on 5/19/2023 12:05 PM

Scooters Comments:

Pedestrians

**Bicycles** 

Report generated on 5/19/2023 12:05 PM

SOURCE: Quality Counts, LLC (http://www.qualitycounts.net) 1-877-580-2212

	Location:	Lyon Str 5/3/2023	eet/Pacific	c Highway	Exit Ran	npSW 9	th Avenu	ue/Pacific H	lighway B	Exit Ramp	þ					Peak Hour																				
																	: 5:00 PM -																			
5	ite Code:	1618420															: 0.911017	1																		
			Lya	on St				P	acific Blvd	WB Off Ran	mp				Pacific Bh	vd EB Ramps					Ly	on St					SW 9t	h Ave		( I	i		Comme			
_			South	ibound					West	tbound						vestbound					North	nbound					Eastb	ound			()		Southea			
													Right to WB Off					1	Right to EB	Right to WB Off						Right to				( I	1			Left to		
	Right to			Left to EB				<ul> <li>Right to</li> </ul>					WB Off	Right to		Left to 9th	Left to	1				Left to				ĒB	To WB		Left to	( I	Right to	Right to	To EB		Left to	
Start Time	Dwy	Right	Thru	Ramps	Left	U-Turn	Lyon St		Ave	Lyon St	Ramps	U-Turn	Ramp		To Dwy	Ave	Lyon St	U-Turn	Ramps	Ramp	Thru	Dwy	Left	U-Turn	Right		Off Ramp	Left	Dwy	U-Turn	9th Ave	Lyon St	Ramps	Ramp	Lyon St	U-Turn
04:00 PM	0	0	0	0	0	0	) 6		(	) (	0 0	0	0	27		) (	) (	, (	0 0	0	(	0 0	0 0	0 0	0	102		5	0	0	0	0	0	0	0	0
04:05 PM 04:10 PM	0	0	0	0	0	0		59 0	(	) (	0 0	0	0	39		1 (	) (	<u>) (</u>	0 0	0	(	0 0	0 0	0 0	0	83		5	0	0	0	0	0	0	0	0
04:10 PM	0	0	0	0	0	0		68 0	(	) (	0 0	0	0	28		) (	) (	, (	0 0	0	(	0 0	0 0	0 0	0	109		3	0	0	0	0	0	0	0	0
04:15 PM 04:20 PM	0	0	0	0	0	0	6	03 1	(	) (	0 0	0	0	35	) (	) (	) (	<u>) (</u>	0 0	0	(	0 0	0 0	0 0	0	84		5	0	0	0	0	0	0	0	0
04:20 PM	0	0	0	0	0	0		67 0	(	) (	0 0	0	0	36	,	) (	) (	, (	0 0	0	(	0 0	0 0	0 0	0	76		2	0	0	0	0	0	0	0	0
04:25 PM 04:30 PM	0	0	0	0	0	0	5	59 0	(	) (	0 0	0	0	40	, L	) (	) (	<u>) (</u>	0 0	0	(	0 0	0 0	0 0	0	78		7	0	0	0	0	0	0	0	0
04:30 PM	0	0	0	0	0	0		57 0	(	) (	0 0	0	0	38	0 U	) (	) (	, (	0 0	0	(	0 0	0 0	0 0	0	80		3	0	0	0	0	0	0	0	0
04:35 PM 04:40 PM	0	0	0	0	0	0		71 0	(		0 0	0	0	36	6 0	) (	) (	1 0	0 0	0	(	0 0	0 0	0 0	0	109	9 0	3	0	0	0	0	0	0	0	0
04:40 PM	0	0	0	0	0	0		52 1	(	) (	0 0	0	0	41	I C	) (	) (	) (	0 0	0	(	0 0	0 0	0 0	0	79	9 0	1	0	0	0	0	0	0	0	0
04:45 PM	0	0	0	0	0	0	6	62 1	(		0 0	0	0	38	3 C	) (	) (	1 0	0 0	0	(	0 0	0 0	0 0	0	74		5	0	0	0	0	0	0	0	0
04:50 PM	0	0	0	0	0	0	) 6	60 0	(	) (	0 0	0	0	31	I C	) (	) (	) (	0 0	0	(	0 0	0 0	0 0	0	94	1 0	7	0	0	0	0	0	0	0	0
04:55 PM 05:00 PM	0	0	0	0	0	0		58 1	(	) (	0 0	0	0	32		) (	) (	1 0	0 0	0	(	0 0	0 0	0 0	0	87		5	1	0	0	0	0	0	0	0
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05:05 PM	0	0	0	0	0	0	6	69 0	(	) (	0 0	0	0	35	5 C	) (	) (	1 0	0 0	0	(	0 0	0 0	0 0	0	106	6 0	4	0	0	0	0	0	0	0	0
05:10 PM	0	0	0	0	0	0	6	67 0	(		0 0	0	0	40	0 0	) (	) (	1 0	0 0	0	(	0 0	0 0	0 0	0	113	3 0	7	1	0	0	0	0	0	0	0
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05:25 PM	0	0	0	0	0	0		66 0	0	) (	0 0	0	0	34	1 C	) (	0 0	/ C	0 0	0	0	0 0	0 0	0 0	0	80		3	1	0	0	0	0	0	0	0
05:30 PM	0	0	0	0	0	0		64 0	(	) (	0 0	0	0	28		) (	) (	1 0	0 0	0	(	0 0	) 0	0 0	0	96		5	0	0	0	0	0	0	0	0
05:35 PM	0	0	0	0	0	0	5	58 0	0	0 0	0 0	0	0	19	e C	0 0	0 0	J C	0 0	0	0	0 0	0 0	0 0	0	67		4	0	0	0	0	0	0	0	0
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05:45 PM	0	0	0	0	0	0	) 5	56 0	(	) (	0 0	0	0	40	0 0	) (	) (	1 0	0 0	0	(	0 0	0 0	0 0	0	77		0	1	0	0	0	0	0	0	0
05:50 PM 05:55 PM	0	0	0	0	0	0		56 1	(	) (	0 0	0	0	21	L L	) (	) (	) (	0 0	0	(	0 0	) 0	0 (	0	100		6	1	0	0	0	0	0	0	0
05:55 PM	0	0	0	0	0	0	6	65 0	(	) (	0 0	0	0	22	2 0	) (	) (	1 0	0 0	0	(	0 0	0 0	0 0	0	79		3	1	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	149	93 7	(	) (	0 0	0	0	794	1 2	2 (	) (	1 0	0 0	0		0 0	0 0	0 0	0	2147	7 0	96	6	0	0	0	0	0	0	0

4th Avenue							Replica NB Thru Vol	7050	Entering NB Synchro volume	1275	
Factor	0.180851			0.183515			Replica SB Thru Vol	8250	Entering SB Synchro volume	1514	
4th/Lyon	PM Bal	ancing Final	4th/Ellsworth	PM Ba	alancing Fir	nal					
NBL	11		SBL	1	32	33					
NBT	1253		SBT	1512	-77	1435					
NBR	11		SBR	1	40	46					
EBL	1	17	18 EBT	5	17	22				NB 5th Ave	1275
EBT	5	32	37 EBR	9	-8	1				NB 4th	1261
WBR	7	53	60 WBT	5	6	11				NB 3rd Ave	1331
WBT	14	10	24 WBL	23	-22	1					
										4th-3rd	-70
Replica volu	imes										

4th/Lyon	PM	4th/Ellsworth	PM	
NBL	61	SBL		6
NBT	NA	SBT	NA	
NBR	59	SBR		4
EBL	3	EBT		26
EBT	30	EBR		48
WBR	41	WBT		27
WBT	75	WBL		125

#### 6th Avenue

Factor	0.181947	0.163364		0.214667	0.158876
6th/Lyon	AM	PM	6th/Ellsworth	AM	PM
NBT	1158	1250	SBL	2	2
NBL	7	6	SBT	1124	1410
EBL	1	3	SBR	1	2
			EBT	2	3
			EBR	7	7
			WBT	2	2
			WBL	2	6

7th Aven	ue						Replica NB Thru Vol	7590	Entering NB Synchro volume	1296
Factor	0.17	0751			0.16865	7	Replica SB Thru Vol	8710	Entering SB Synchro volume	1469
7th/Lyon	PM	Balancing	Final	7th/Ellsworth	PM	Balancing Final				
NBL		72		SBL		9				
NBT		1204 +15	1219	SBT	141	2				
NBR		20 -8	12	SBR	4	8				
EBL		47		EBT	4	1 2	43			
EBT		5		EBR	12	1				
WBR		3 35	38	WBT	7	1 -10	61			
WBT		18		WBL	2	0 10	30			
Replica v	olumes									
7th/Lyon	PM			7th/Ellsworth	РМ					
NBL		421		SBL	5	2				
NBT	NA			SBT	NA					
NBR		116		SBR	28	7				
EBL		273		EBT	24	1				
EBT		28		EBR	71	9				
WBR		17		WBT	42	0				

WBT

106

WBL

8th Avenu <b>Factor</b>		0302				0.16862	L			Replica NB Thru Vol Replica SB Thru Vol	7610 9210	Entering NB Synchro volume Entering SB Synchro volume (calc	1296 1553
8th/Lyon			Balancing	Final	8th/Ellsworth		Balancing	Final		·			
NBL		3			SBL	(	)						
NBT		1293			SBT	155	3 10	)					
NBR		0			SBR	(	כ						
EBL		1	5	5	6 EBT		2 4	1	6				
EBT		0			EBR	(	) 22	2	22				
WBR		4			WBT		2						
WBT		0	10	)	10 WBL		1 10	)	11				
Replica vo	lumes												
8th/Lyon					8th/Ellsworth	РМ							
NBL		19			SBL		כ						
NBT	NA				SBT	NA							
NBR		0			SBR		)						
EBL		8			EBT		Ð						
EBT		0			EBR		)						
WBR		23			WBT	1	1						
WBT		0			WBL		4						

The 8th Ave link west of Lyon St doesn't connect to Lyon St, so zeroes are shown for those turns

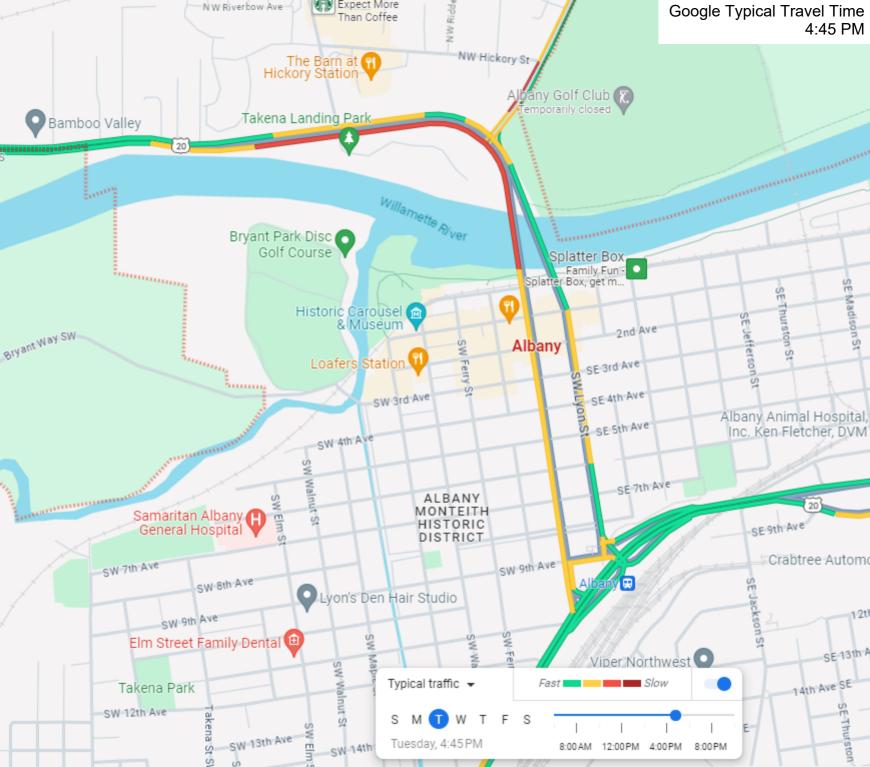
## **APPENDIX B: GOOGLE TYPICAL TRAFFIC MAP**

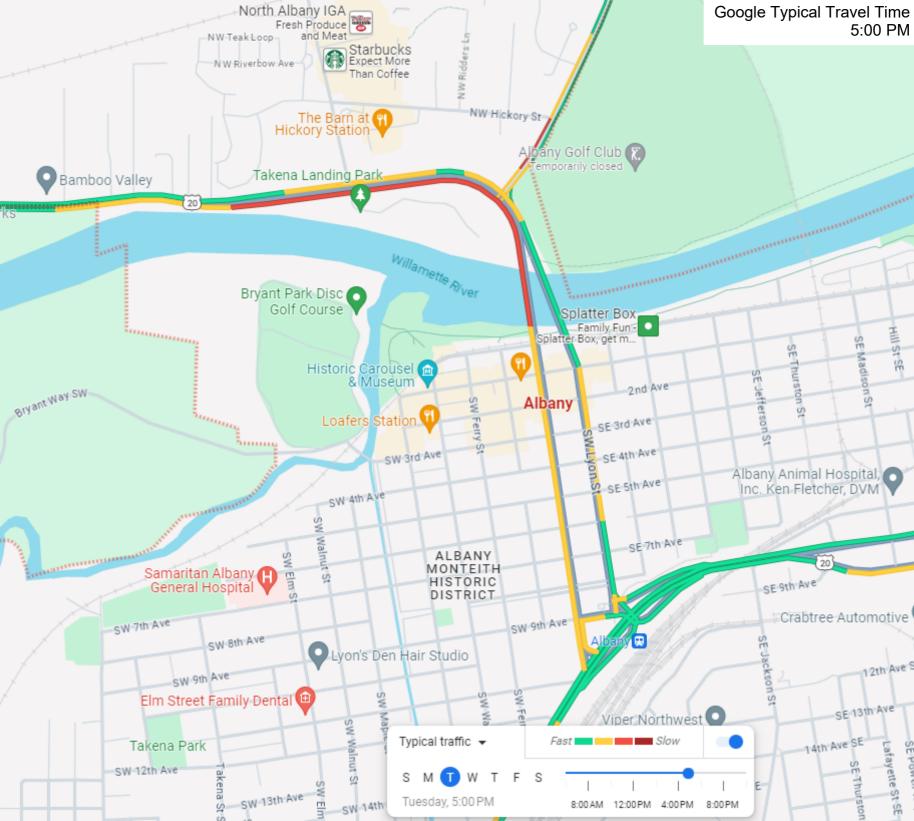




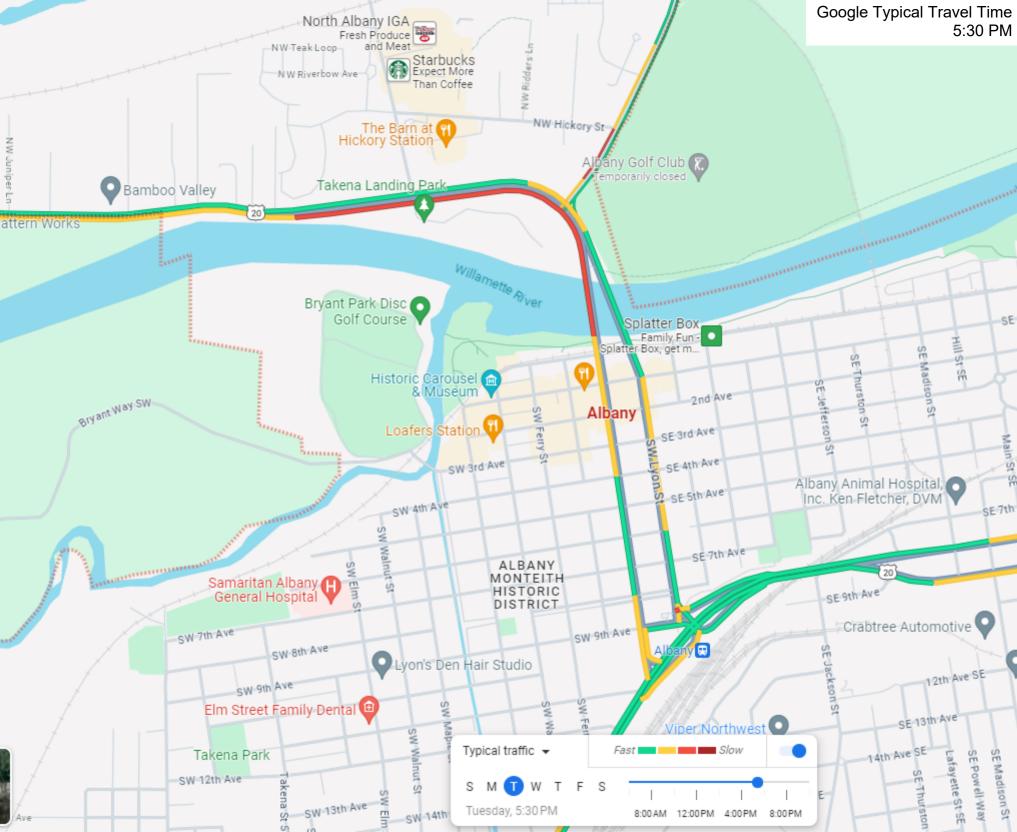


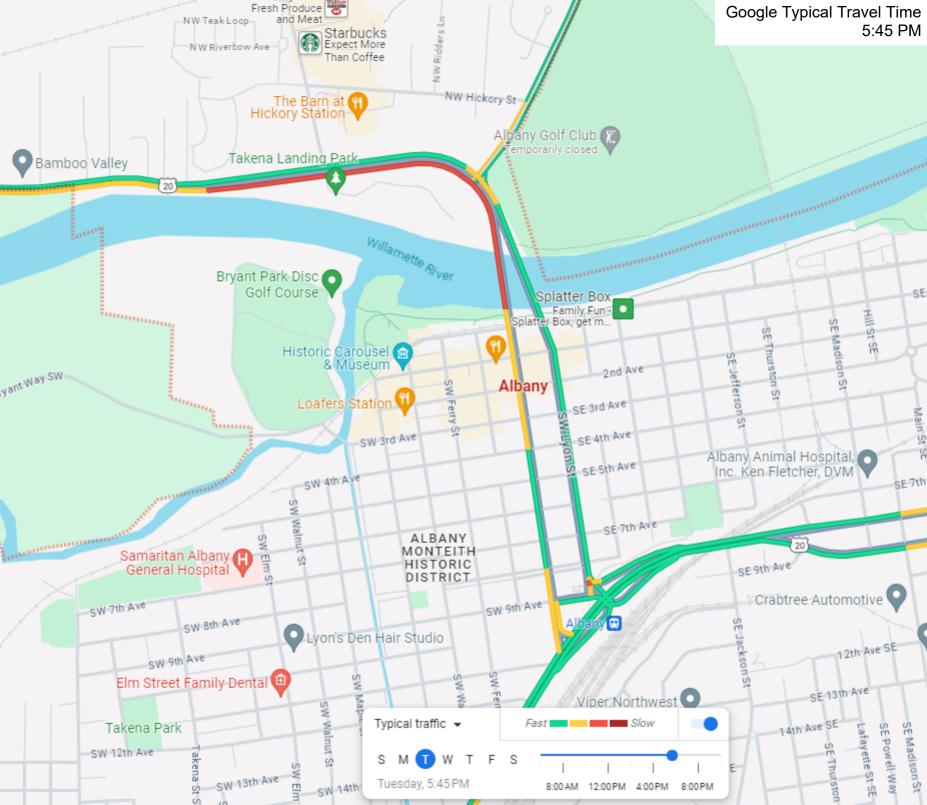


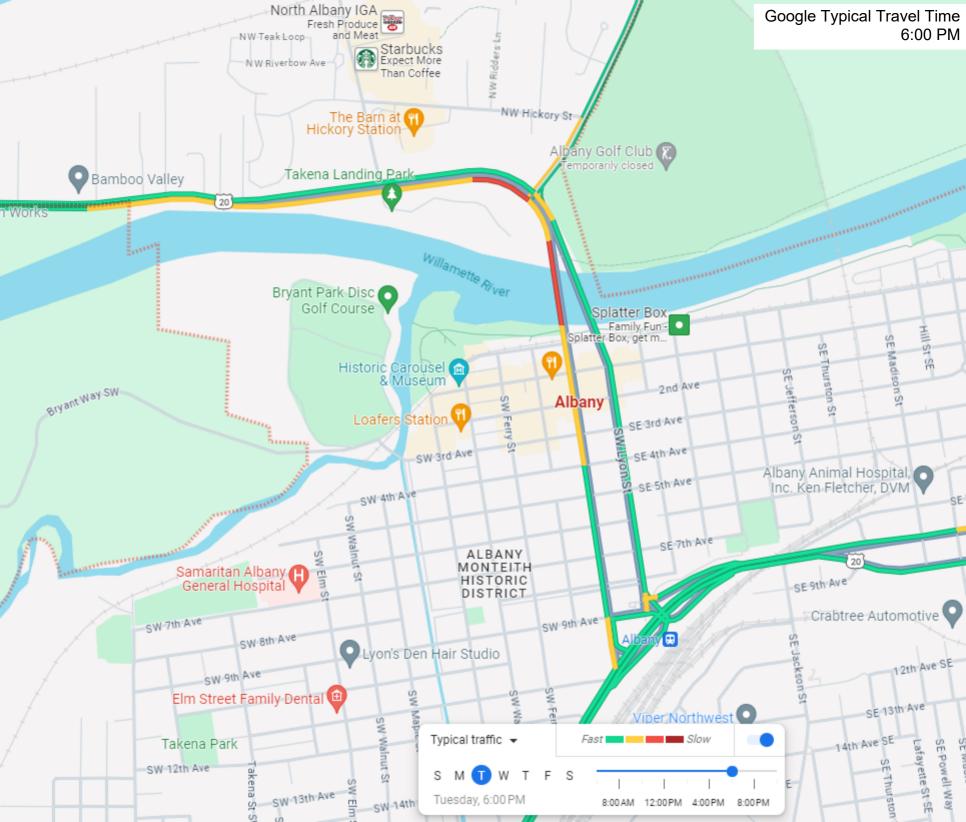












# **APPENDIX C: EXISTING CONDITIONS VOLUME PROFILES**

**DKS** ALBANY US 20 CORRIDOR STUDY • VISSIM PROTOCOL CALIBRATION AND PROJECT BUNDLE RESULTS REPORT • FEBRUARY 2024



1st Ave - WB1891891861541471731511671533rd Ave - WB $34$ $34$ $33$ $28$ $26$ $31$ $27$ $30$ $22$ 4th Ave - WB $21$ $21$ $33$ $26$ $21$ $18$ $11$ $25$ $22$ 5th Ave - WB $7$ $7$ $10$ $8$ $7$ $6$ $4$ $8$ $77$ 7th Ave - WB $7$ $7$ $10$ $8$ $7$ $6$ $4$ $8$ $77$ 7th Ave - WB $17$ $17$ $27$ $22$ $17$ $14$ $9$ $21$ $11$ 8th Ave - WB $4$ $4$ $6$ $5$ $4$ $3$ $2$ $5$ $4$ Pacific Hwy WB off-ramp - WB $210$ $210$ $203$ $193$ $194$ $213$ $209$ $189$ $19$ Albary Station - NB $1$ $1$ $2$ $2$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ Pacific Hwy EB off-ramp - EB $109$ $109$ $127$ $132$ $116$ $120$ $119$ $94$ $99$ Ellsworth Ave - NB $10$ $10$ $16$ $12$ $10$ $8$ $5$ $12$ $116$ 9th Ave - EB $8$ $8$ $12$ $10$ $8$ $7$ $4$ $10$ $88$ 7th Ave - EB $50$ $50$ $49$ $41$ $39$ $45$ $40$ $44$ 4th Ave - EB $7$ $7$ $11$ $9$ $7$									
Input	Seeding Period	4:00-4:15	4:15-4:30	4:30-4:45	4:45-5:00	5:00-5:15	5:15-5:30	5:30-5:45	5:45-6:00
1st Ave - WB	189	189	186	154	147	173	151	167	151
3rd Ave - WB	34	34	33	28	26	31	27	30	27
4th Ave - WB	21	21	33	26	21	18	11	25	22
5th Ave - WB	7	7	10	8	7	6	4	8	7
7th Ave - WB	17	17	27	22	17	14	9	21	18
8th Ave - WB	4	4	6	5	4	3	2	5	4
Pacific Hwy WB off-ramp - WB	210	210	203	193	194	213	209	189	190
Albany Station - NB	1	1	2	2	1	1	1	1	1
Pacific Hwy EB off-ramp - EB	109	109	127	132	116	120	119	94	95
Ellsworth Ave - NB	10	10	16	12	10	8	5	12	10
9th Ave - EB	53	53	45	38	47	61	35	40	59
8th Ave - EB	8	8	12	10	8	7	4	10	8
7th Ave - EB	50	50	49	41	39	45	40	44	40
5th Ave - EB	19	19	18	17	18	35	12	18	8
4th Ave - EB	7	7	11	9	7	6	4	8	7
3rd Ave - EB	52	52	51	43	41	48	42	46	42
2nd Ave - EB	154	154	151	125	119	140	123	136	123
6th Ave - EB	3	3	5	4	3	3	2	4	3
North Albany Rd - NB	3	3	4	3	3	2	1	3	3
US20 w/o North Albany Rd - EB	194	194	201	198	204	252	244	188	194
North Albany Rd - SB	120	120	142	161	185	162	142	167	159
Springhill Dr - SB	124	124	123	135	110	142	116	127	105

# **APPENDIX D: EXISTING CONDITIONS RESULTS**

GEH, DELAY, QUEUING, TRAVEL TIMES, AND LATENT DEMAND



	GI	EH - 4:45	to 5:45 PM		
Intersection					
Number	Intersection Name	Movement	Input Volume	VISSIM Output Volume	GEH
		NBL	1	0	1.4
		NBT	0	0	0.8
		NBR	7	7	0.0
		SBL	549	546	0.1
		SBT	6	6	0.0
		SBR	101	103	0.2
1	US 20 & N Albany Rd	EBL	106	98	0.8
		EBT	792	785	0.2
		EBR	0	1	0.8
		WBL	4	4	0.0
		WBT	596	601	0.2
		WBR	682	674	0.3
		Total	2845	2823	0.4
		SBL	482	479	0.1
		SBR	13	13	0.0
		EBL	40	37	0.5
2	US 20 & Springhill Dr	EBT	1308	1301	0.2
		WBT	1269	1267	0.0
		WBR	612	620	0.3
		Total	3724	3715	0.1
		NBL	91	91	0.0
		NBT	1365	1364	0.0
3	Lyon & 1st	WBT	122	124	0.2
		WBR	516	515	0.1
		Total	2094	2095	0.0
		NBT	1228	1230	0.1
		NBR	58	59	0.1
4	Lyon & 2nd	EBL	228	226	0.1
		EBT	550	539	0.5
		Total	2064	2052	0.3
		NBL	93	92	0.1
		NBT	1204	1203	0.0
		NBR	36	36	0.0
-		EBL	50	52	0.2
5	Lyon & 3rd	EBT	92	91	0.1
		WBT	82	82	0.0
		WBR	32	32	0.0
		Total	1590	1584	0.1
		NBL	34	34	0.0
		NBT	1248	1244	0.1
		NBR	20	20	0.0
-		EBL	25	24	0.2
6	Lyon & 5th	EBT	23	22	0.1
		WBT	17	16	0.3
		WBR	6	6	0.0
		Total	1373	1363	0.3
		NBL	433	447	0.7
		NBU	1	0	1.4
		SBT	3	3	0.0
		SBR	802	800	0.1
		EBL	1191	1193	0.1
7	Lyon & 9th	EBT	5	7	0.8

	GI	EH - 4:45	to 5:45 PM		
Intersection					
Number	Intersection Name	Movement	Input Volume	VISSIM Output Volume	GEH
		EBR	3	6	1.4
		EBU	52	47	0.7
		WBL	0	0	
		WBT	4	3	0.5
		Total	2494	2506	0.2
		NBL	33	31	0.4
		NBR	3	2	0.5
		SBL	1070	1071	0.0
8	Ellsworth & 9th	SBT	474	480	0.3
0		SBR	47	44	0.4
		EBT	179	181	0.1
		EBR	3	0	2.4
		Total	1809	1808	0.0
		SBL	8	7	0.4
		SBT	1400	1401	0.0
		SBR	33	34	0.2
9	Ellsworth & 5th	EBT	39	37	0.4
5		EBR	43	42	0.2
		WBL	17	16	0.3
		WBT	34	33	0.2
		Total	1575	1569	0.1
		SBL	49	49	0.0
		SBT	1372	1369	0.1
		SBR	40	39	0.1
10	Ellsworth & 3rd	EBT	93	94	0.1
		EBR	82	80	0.2
		WBL	62	64	0.2
		WBT	113	109	0.4
		Total	1812	1799	0.3
		SBL	394	387	0.3
		SBT	1327	1321	0.2
11	Ellsworth & 2nd	EBT	384	377	0.4
		EBR	134	133	0.1
		Total	2239	2217	0.5
		SBT	1646	1629	0.4
10		SBR	144	145	0.1
12	Ellsworth & 1st	WBL	74	77	0.3
		WBT	139	139	0.0
		Total	2003	1988	0.3
		SBL	0	0	. ·
		SBT	1459	1455	0.1
		SBR	2	3	0.6
13	Ellsworth & 6th	EBT	4	4	0.1
		EBR	7	7	0.0
		WBL	0	0	0.1
		WBT	4	4	0.1
	l	Total	1476	1470	0.1

ENTRY GEH (4:45-5:45 PM)							
Vissim							
Entry Location	Count	Throughput	Diff	%Diff	GEH		
US 20 & N Albany Rd - N	656	655	-1	-0.1%	0.0		
US 20 & N Albany Rd - S	8	7	-1	-15.9%	0.5		
US 20 & N Albany Rd - W	899	884	-15	-1.6%	0.5		
US 20 & Springhill Dr - N	495	492	-3	-0.6%	0.1		
Lyon & 1st - E	638	639	1	0.1%	0.0		
Lyon & 3rd - E	114	114	0	0.0%	0.0		
Lyon & 5th - E	23	22	-1	-5.2%	0.3		
Lyon & 9th - N	805	803	-2	-0.2%	0.1		
Lyon & 9th - S	434	447	13	3.0%	0.6		
Lyon & 9th - E	4	3	-1	-25.0%	0.5		
Ellsworth & 9th - S	36	33	-3	-7.6%	0.5		
Ellsworth & 9th - W	182	181	-1	-0.7%	0.1		
Ellsworth & 5th - W	83	79	-4	-4.4%	0.4		
Ellsworth & 3rd - W	176	174	-2	-0.9%	0.1		
Ellsworth & 2nd - W	519	510	-9	-1.7%	0.4		
Ellsworth & 6th - W	11	11	0	0.6%	0.0		
Total	5082	5054	-28	-0.6%	0.4		

EXIT GEH (4:45-5:45 PM)						
Vissim						
Exit Location	Count	Throughput	Diff	%Diff	GEH	
US 20 & N Albany Rd - N	788	772	-16	-2.1%	0.6	
US 20 & N Albany Rd - S	10	11	1	6.7%	0.2	
US 20 & N Albany Rd - W	698	704	6	0.9%	0.2	
US 20 & Springhill Dr - N	652	657	5	0.7%	0.2	
Lyon & 2nd - E	609	598	-11	-1.7%	0.4	
Lyon & 3rd - E	128	127	-1	-1.1%	0.1	
Lyon & 5th - E	43	42	-1	-1.8%	0.1	
Lyon & 9th - N	1191	1193	2	0.2%	0.1	
Lyon & 9th - S	7	9	2	28.6%	0.7	
Lyon & 9th - E	5	7	2	40.0%	0.8	
Ellsworth & 9th - S	477	480	3	0.6%	0.1	
Ellsworth & 9th - W	80	75	-5	-5.8%	0.5	
Ellsworth & 5th - W	67	67	0	0.3%	0.0	
Ellsworth & 3rd - W	153	148	-5	-3.2%	0.4	
Ellsworth & 1st - W	283	284	1	0.4%	0.1	
Ellsworth & 6th - W	6	7	1	14.9%	0.4	
Total	5197	5181	-16	-0.3%	0.2	

РМ РЕАК НО	UR <u>(4:4</u>	5-5:4 <u>5 P</u>	M) DEL	.AY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
	NB	Right	7	7
		Total	7	7
	SB	Left	546	28
		Through	6	26
		Right	103	5
		Total	655	25
		Left	98	47
US 20 & N Albany Rd	EB	Through	785	11
	LD	Right	1	18
		Total	884	15
		Left	4	57
	WB	Through	601	14
	VV D	Right	674	14
		Total	1279	14
		Total	2825	17
		Left	479	51
	SB	Right	13	28
		Total	492	51
	EB	Left	37	55
US 20 & Springhill Dr		Through	1301	19
		Total	1338	20
	WB	Through	1267	19
		Right	620	10
		Total	1887	16
		Total	3717	22
	NB	Left	91	5
		Through	1364	6
		Total	1455	6
Lyon & 1st	WB	Through	124	23
		Right	515	42
		Total	639	38
	NB	Total	2094	16
Lyon & 2nd		Through	1230	3
		Right	59	4
	EB	Total	1289	3
		Left	226	27
		Through	539	33
		Total	765	31
		Total	2054	13
		Left	92	10
	NR	Through	1203	9

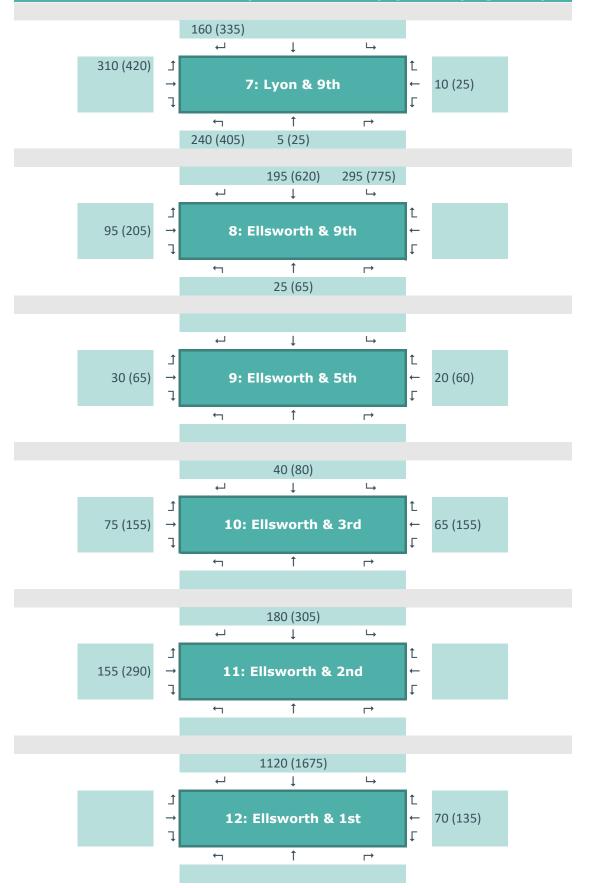
РМ РЕАК НО	UR (4:4	5-5:45 P	M) DEI	_AY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
	ND	Right	36	8
		Total	1331	9
		Left	52	15
Lyon & 3rd	EB	Through	91	17
		Total	143	16
		Through	82	23
	WB	Right	32	11
		Total	114	20
		Tota	1588	10
		Left	34	0
	NB	Through	1244	0
	ПD	Right	20	1
		Total	1298	0
		Left	24	13
Lyon & 5th	EB	Through	22	12
		Total	46	12
		Through	16	14
	WB	Right	6	9
		Total	22	13
		Tota	1366	1
	NB	Left	447	36
	ND	Total	447	36
		Through	3	19
	SB	Right	800	15
		Total	803	15
	EB	Left	1193	27
Lyon & 9th		Through	7	17
		Right	6	1
		U-Turn	47	6
		Total	1253	26
	WB	Through	3	46
		Total	3	46
		Total		24
		Left	31	38
	NB	Right	2	12
		Total	33	37
	SB	Left	1071	13
Ellsworth & 9th		Through	480	6
		Right	44	5
		Total	1595	11
	FR	Through	181	32

	UR (4:4	5-5:45 P	M) DEL	.AY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
	LD	Total	181	32
		Total	1809	13
	SB	Left	7	1
		Through	1401	1
		Right	34	2
		Total	1442	1
		Through	37	23
Ellsworth & 5th	EB	Right	42	11
		Total	79	17
		Left	16	9
	WB	Through	33	15
		Total	49	13
		Total	1570	2
		Left	49	1
	SB	Through	1369	2
	36	Right	39	2
		Total	1457	2
		Through	94	28
Ellsworth & 3rd	EB	Right	80	18
		Total	174	23
		Left	64	7
	WB	Through	109	28
		Total	173	20
		Total	1804	5
		Left	387	5
	SB	Through	1321	5
		Total	1708	5
Ellsworth & 2nd	EB	Through	377	38
		Right	133	24
		Total	510	34
		Total	2218	12
Ellsworth & 1st	SB WB	Through	1629	72
		Right	145	75
		Total	1774	72
		Left	77	34
		Through	139	23
		Total	216	27
		Total	1990	67
		Through	1455	2
	SB	Right	3	7
		Total	1458	2

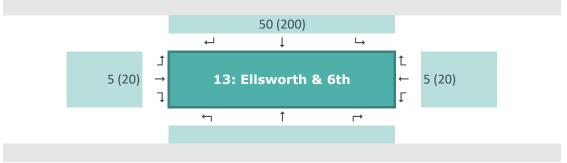
PM PEAK HOUR (4:45-5:45 PM) DELAY					
Intersection	Approach	Movement	Volume	Average Delay (s)	
	EB	Through	4	26	
Ellsworth & 6th		Right	7	5	
		Total	11	13	
	WB	Through	4	167	
		Total	4	167	
		Total	1473	2	

#### EXISTING PM PEAK HOUR (4:45 to 5:45 PM) QUEUES (Avg/95th) 140 (240) 15 (45) ⊣ Ţ $\mapsto$ 70 (155) 1 Ĺ 195 (470) 115 (230) 1: US 20 & N Albany Rd ← 145 (300) $\rightarrow$ L 5 (20) J ← 1 0 (20) 0 (0) 355 (685) ┛ Ļ $\square$ 35 (180) 30 (80) 1 Ĺ 260 (690) 2: US 20 & Springhill Dr ← 380 (830) $\rightarrow$ J L 1 $\rightarrow$ ← $\rightarrow$ Ţ $\rightarrow$ 305 (680) 1 Ĺ 3: Lyon & 1st 50 (100) ← **→** ļ L ← 1 $\rightarrow$ 200 (305) $\rightarrow$ Ţ 1 Ĺ 235 (330) 4: Lyon & 2nd $\rightarrow$ ← J L 1 ← $\rightarrow$ 65 (180) ┙ Ţ $\rightarrow$ 1 Ĺ 45 (110) $\rightarrow$ 5: Lyon & 3rd ← 50 (115) Г ļ 1 ← $\rightarrow$ 195 (385) ┛ $\rightarrow$ Ţ 1 Ĺ 6: Lyon & 5th 20 (45) $\rightarrow$ ← 10 (20) J L 1 $\rightarrow$

#### EXISTING PM PEAK HOUR (4:45 to 5:45 PM) QUEUES (Avg/95th)



### EXISTING PM PEAK HOUR (4:45 to 5:45 PM) QUEUES (Avg/95th)



	Existing Vissim Travel Time Calibration Results										
				Travel Time (Seconds)							
Direction	From/To	Sources	4:00-4:15	4:15-4:30	4:30-4:45	4:45-5:00	5:00-5:15	5:15-5:30	5:30-5:45	5:45-6:00	Peak Hour (4:45-5:45 PM)
Northbound	Lyon Street north of OR 99E SB Off-	Vissim	169	170	169	175	181	173	166	158	174
Northbound	Ramp/US 20 at N Albany Rd	Google Data	194	198	201	189	195	192	195	185	193
										Difference	-9.9%
Southbound	US 20 at N Albany Rd/OR 99E NB On	Vissim	240	265	264	279	263	251	261	216	264
Southbound	Ramp	Google Data	228	246	267	249	281	349	313	255	298
										Difference	-11.6%

	Average	Vehicle Hours	Latent		Vehicle Miles	
	Delay / veh	of Delay	Demand	Latent Delay	Travelled	Travel Time
	(sec)	(hrs)	(veh)	(veh-hrs)	(mi)	(hrs)
Avg	583.5	274.1	0.1	0.5	9747.2	635.5
StdDev	54.4	26.7	0.3	0.1	128.8	28.4
Min	509.9	237.2	0.0	0.4	9547.6	595.8
Мах	671.2	317.6	1.0	0.6	9945.6	682.3
Aver delay (web (min (web)	4 54					

Latent Demand

Avg delay/veh (min/veh)

1.51





## 415-430 PM

























## **APPENDIX E: NO BUILD RESULTS**

GEH, DELAY, QUEUING, TRAVEL TIMES, AND LATENT DEMAND



	NO-BUI	LD GEH -	4:45 to 5:4	5 PM	
Intersection					
Number	Intersection Name	Movement	Input Volume	VISSIM Output Volume	GEH
		NBL	5	4	0.5
		NBT	5	5	0.0
		NBR	10	9	0.3
		SBL	625	601	1.0
		SBT	10	11	0.3
		SBR	125	121	0.4
1	US 20 & N Albany Rd	EBL	110	81	3.0
		EBT	840	639	7.4
		EBR	0	0	
		WBL	5	4	0.5
		WBT	805	729	2.7
		WBR	855	776	2.8
		Total	3395	2981	7.3
		SBL	600	452	6.5
		SBR	20	14	1.5
		EBL	45	33	1.9
2	US 20 & Springhill Dr	EBT	1430	1209	6.1
		WBT	1645	1493	3.8
		WBR	800	727	2.6
		Total	4540	3929	9.4
		NBL	85	86	0.1
		NBT	1700	1708	0.2
3	Lyon & 1st	WBT	130	91	3.7
		WBR	745	508	9.5
		Total	2660	2392	5.3
		NBT	1500	1544	1.1
		NBR	65	69	0.5
4	Lyon & 2nd	EBL	285	250	2.1
		EBT	665	544	4.9
		Total	2515	2407	2.2
		NBL	95	98	0.3
		NBT	1460	1502	1.1
		NBR	40	39	0.2
5	Lyon & 2rd	EBL	65	67	0.2
5	Lyon & 3rd	EBT	95	89	0.6
		WBT	85	80	0.6
		WBR	40	42	0.3
		Total	1880	1915	0.8
		NBL	40	39	0.2
		NBT	1485	1526	1.1
		NBR	35	36	0.2
6	Lyon & 5th	EBL	40	40	0.0
0		EBT	45	44	0.1
		WBT	20	22	0.4
		WBR	10	9	0.3
		Total	1675	1715	1.0
		NBL	605	628	0.9
		NBU	5	6	0.4
		SBT	5	5	0.0
		SBR	895	886	0.3
		EBL	1285	1162	3.5
7	Lyon & 9th	EBT	5	6	0.4

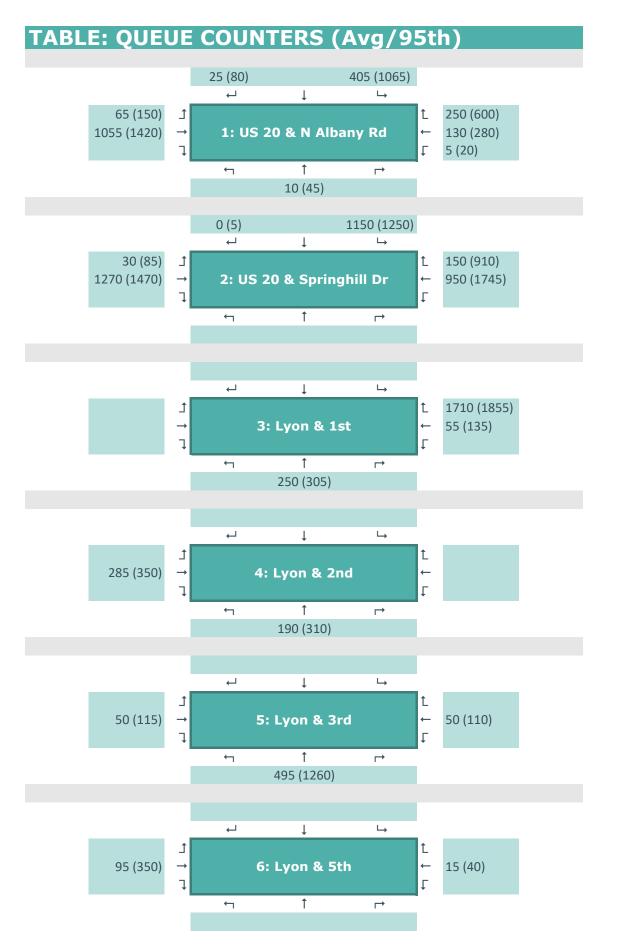
	NO-BUI	LD GEH -	4:45 to 5:4	5 PM	
Intersection					
Number	Intersection Name	Movement	Input Volume	VISSIM Output Volume	GEH
		EBR	5	2	1.6
		EBU	55	50	0.7
		WBL	0	0	•••
		WBT	5	3	1.0
		Total	2865	2748	2.2
		NBL	45	44	0.1
		NBR	10	10	0.0
		SBL	1130	996	4.1
2		SBT	510	451	2.7
8	Ellsworth & 9th	SBR	55	44	1.6
		EBT	210	210	0.0
		EBR	5	6	0.4
		Total	1965	1761	4.7
		SBL	30	27	0.6
		SBT	1500	1268	6.2
		SBR	40	32	1.3
0		EBT	55	57	0.3
9	Ellsworth & 5th	EBR	55	54	0.1
		WBL	25	22	0.6
		WBT	35	39	0.7
		Total	1740	1497	6.0
		SBL	60	52	1.1
		SBT	1480	1236	6.6
		SBR	40	32	1.3
10		EBT	100	103	0.3
10	Ellsworth & 3rd	EBR	85	83	0.2
		WBL	65	59	0.8
		WBT	115	117	0.2
		Total	1945	1683	6.2
		SBL	490	391	4.7
		SBT	1440	1192	6.8
11	Ellsworth & 2nd	EBT	460	319	7.1
		EBR	140	105	3.2
		Total	2530	2007	11.0
		SBT	1855	1529	7.9
		SBR	175	149	2.0
12	Ellsworth & 1st	WBL	75	53	2.8
		WBT	140	122	1.6
		Total	2245	1853	8.7
		SBL	5	0	3.2
		SBT	1560	1332	6.0
		SBR	15	12	0.8
13	Ellsworth & 6th	EBT	5	6	0.4
15		EBR	25	23	0.4
		WBL	10	4	2.3
		WBT	10	14	1.2
		Total	1630	1392	6.1

NO-BUILD PI	<b>М РЕАК НС</b>	DUR (4:45-5	:45 PM) I	DELAY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
		Left	4	62
	ND	Through	5	59
	NB	Right	9	24
		Total	18	42
		Left	601	75
	SB	Through	11	72
	30	Right	121	20
LIC 20 9 N Albany Dd		Total	733	66
US 20 & N Albany Rd		Left	81	163
	EB	Through	639	223
		Total	720	216
		Left	4	73
	WB	Through	729	15
	VV D	Right	776	17
		Total	1509	16
		Total	2980	77
		Left	452	291
	SB	Right	14	262
		Total	466	290
		Left	33	211
UC 20 % Chringhill Dr	EB	Through	1209	200
US 20 & Springhill Dr		Total	1242	201
		Through	1493	38
	WB	Right	727	31
		Total	2220	36
		Total	3928	118
		Left	86	5
	NB	Through	1708	8
		Total	1794	8
Lyon & 1st		Through	91	541
	WB	Right	508	670
		Total	599	651
		Total	2393	169
		Through	1544	7
	NB	Right	69	8
		Total	1613	7
Lyon & 2nd		Left	250	47
	EB	Through	544	40
		Total	794	42
		Total	2407	19
		Left	98	14

				Average
Intersection	Approach	Movement	Volume	Delay (s
	ND	Through	1502	1
	NB	Right	39	1
		Total	1639	14
		Left	67	1
Lyon & 3rd	EB	Through	89	1
		Total	156	1
		Through	80	2
	WB	Right	42	1
		Total	122	2
		Total	1917	1
		Left	39	
	NB	Through	1526	
	NB	Right	36	
		Total	1601	
		Left	40	ç
Lyon & 5th	EB	Through	44	8
		Total	84	9
		Through	22	2
	WB	Right	9	2
		Total	31	2
		Total	1716	1
		Left	628	10
	NB	U-Turn	6	ç
		Total	634	10
		Through	5	2
	SB	Right	886	2
		Total	891	2
Lyon & 9th		Left	1162	3
Lyon & Jun		Through	6	2
	EB	Right	2	
		U-Turn	50	1
		Total	1220	3
	WB	Through	3	5
		Total	3	5
		Total	2748	4
		Left	44	3
	NB	Right	10	1
		Total	54	3
		Left	996	2
		Through	451	1
Ellsworth & 9th	SB	Right	431	1

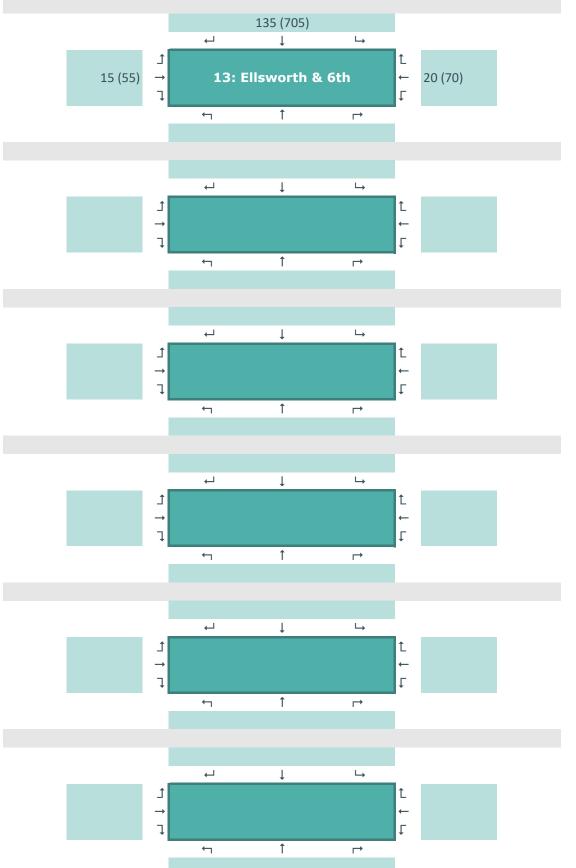
				Average
Intersection	Approach	Movement	Volume	Delay (s
		Total	1491	1
		Through	210	4
	EB	Right	6	2
		Total	216	4
		Total	1761	2
		Left	27	
	SB	Through	1268	
	56	Right	32	
		Total	1327	
		Through	57	۷
Ellsworth & 5th	EB	Right	54	-
		Total	111	3
		Left	22	
	WB	Through	39	1
		Total	61	1
		Total	1499	
		Left	52	
		Through	1236	
	SB	Right	32	
		Total	1320	
		Through	103	3
Ellsworth & 3rd	EB	Right	83	2
		Total	186	2
		Left	59	
	WB	Through	117	-
		Total	176	2
		Total	1682	
		Left	391	
	SB	Through	1192	
		Total	1583	
Ellsworth & 3rd		Through	319	31
	EB	Right	105	24
		Total	424	30
		Total	2007	6
		Through	1529	13
	SB	Right	149	14
		Total	1678	13
Ellsworth & 1st		Left	53	
	WB	Through	122	
		Total	175	3
		Total	1853	12

NO-BUILD PM PEAK HOUR (4:45-5:45 PM) DELAY										
Intersection	Approach	Movement	Volume	Average Delay (s						
		Through	1332							
	SB	Right	12							
		Total	1344							
	EB	Through	6	3						
Ellsworth & 6th		Right	23	2						
Elisworth & oth		Total	29	2						
		Left	4	1						
-	WB	Through	14	8						
		Total	18	9						
		Total	1391							



#### **TABLE: QUEUE COUNTERS (Avg/95th)** 250 (560) ⊣ Ţ $\Box$ 345 (425) 1 Ĺ 7: Lyon & 9th ← 5 (35) **→** J L ← 1 ⊢ 605 (685) 20 (70) 305 (875) 435 (875) ┙ $\Box$ Ţ 1 Ĺ 125 (290) $\rightarrow$ 8: Ellsworth & 9th ← ļ L 1 ← $\rightarrow$ 35 (85) ┙ ╘ Ţ 1 Ĺ 60 (275) 9: Ellsworth & 5th 20 (50) $\rightarrow$ ← ļ Γ 1 ← $\rightarrow$ 115 (880) ┙ Ţ $\Box$ 1 Ĺ 10: Ellsworth & 3rd 85 (185) 70 (155) $\rightarrow$ ← L ļ 1 ← $\rightarrow$ 125 (305) ⊣ $\square$ Ţ 1 Ĺ 570 (615) 11: Ellsworth & 2nd ← $\rightarrow$ L J 1 ← $\rightarrow$ 1525 (1695) ⊣ $\mapsto$ Ţ 1 Ĺ **→** 12: Ellsworth & 1st 70 (160) ← ļ L 1 ← $\rightarrow$

# TABLE: QUEUE COUNTERS (Avg/95th)



	No-Build Vissim Travel Time Results										
				Travel Time (Seconds)							
Direction	From/To	Scenario	4:00-4:15	4:15-4:30	4:30-4:45	4:45-5:00	5:00-5:15	5:15-5:30	5:30-5:45	5:45-6:00	Peak Hour (4:45-5:45 PM)
Northbound	Lyon Street north of OR 99E SB Off-	Existing	169	170	169	175	181	173	166	158	174
Northbound	Ramp/US 20 at N Albany Rd	No-Build	227	243	272	250	245	239	241	216	244
										Difference	40.3%
Southbound	US 20 at N Albany Rd/OR 99E NB	Existing	240	265	264	279	263	251	261	216	264
Southbound	On-Ramp	No-Build	318	408	489	538	599	602	547	557	571
										Difference	116.8%

	Average	Vehicle Hours	Latent		Vehicle Miles	
	Delay / veh	of Delay	Demand	Latent Delay	Travelled	Travel Time
	(sec)	(hrs)	(veh)	(veh-hrs)	(mi)	(hrs)
Avg	1622.6	976.9	1152.4	1151.5	10637.7	1368.8
StdDev	69.2	46.2	52.5	78.8	158.5	45.6
Min	1504.7	901.8	1044.0	1023.4	10403.7	1294.9
Мах	1725.3	1045.9	1237.0	1291.4	10885.1	1436.6

Avg delay/veh (min/veh)

9.75

















### **APPENDIX F: UNSERVED DEMAND RESULTS**

**NO-BUILD AND PROJECT BUNDLES** 

ALBANY US 20 CORRIDOR STUDY • VISSIM PROTOCOL CALIBRATION AND PROJECT BUNDLE RESULTS REPORT • FEBRUARY 2024



Unserved Demand by Input Location (at 6:00 PM)										
	No-l	No-Build		Bundle 1 Bu		dle 2	Bundle 3			
Input Location	Unserved	% Served	Unserved	% Served	Unserved	% Served	Unserved	% Served		
1: 1st Ave - WB	596	67%	0	100%	2	100%	2	100%		
7: Pacific Hwy WB off-ramp - WB	0	100%	0	100%	18	99%	0	100%		
13: 7th Ave - EB	0	100%	5	98%	7	98%	10	97%		
17: 2nd Ave - EB	172	86%	47	96%	46	96%	28	98%		
20: US20 w/o North Albany Rd - EB	198	89%	0	100%	0	100%	0	100%		
22: Springhill Dr - SB	185	85%	0	100%	6	100%	0	100%		
Total	1153	91.2%	52	99.6%	79	99.4%	40	99.7%		

## **APPENDIX G: PROJECT BUNDLE 1 RESULTS**

GEH, DELAY, QUEUING, AND SYSTEM MEASURES



DKS

	BUNDLI	E 1 GEH -	4:45 to 5:4!	5 PM	
Intersection					
Number	Intersection Name	Movement	Input Volume	VISSIM Output Volume	GEH
		NBL	5	4	0.5
		NBT	5	5	0.0
		NBR	10	9	0.3
		SBL	625	639	0.6
		SBT	10	11	0.3
		SBR	125	125	0.0
1	US 20 & N Albany Rd	EBL	110	103	0.7
		EBT	840	834	0.2
		EBR	0	1	1.4
		WBL	5	5	0.0
		WBT	805	824	0.7
		WBR	855	870	0.5
		Total	3395	3428	0.6
		SBL	600	570	1.2
		SBR	20	20	0.0
		EBL	45	45	0.0
2	US 20 & Springhill Dr	EBT	1430	1442	0.3
		WBT	1645	1683	0.9
		WBR	800	837	1.3
		Total	4540	4596	0.8
		NBL	85	89	0.4
		NBT	1700	1761	1.5
3	Lyon & 1st	WBT	130	133	0.3
_		WBR	745	764	0.7
		Total	2660	2747	1.7
		NBT	1500	1580	2.0
		NBR	65	70	0.6
4	Lyon & 2nd	EBL	285	268	1.0
-	_,	EBT	665	647	0.7
		Total	2515	2565	1.0
		NBL	95	100	0.5
		NBT	1460	1540	2.1
		NBR	40	40	0.0
		EBL	65	66	0.1
5	Lyon & 3rd	EBT	95	91	0.4
		WBT	85	80	0.6
		WBR	40	42	0.3
		Total	1880	1958	1.8
		NBL	40	41	0.2
		NBT	1485	1558	1.9
		NBR	35	36	0.2
		EBL	40	41	0.2
6	Lyon & 5th	EBT	45	49	0.6
		WBT	20	22	0.4
		WBR	10	9	0.3
		Total	1675	1756	2.0
		NBL	605	637	1.3
		NBU	5	5	0.0
		SBT	5	6	0.4
		SBR	895	910	0.5
		EBL	1285	1284	0.0

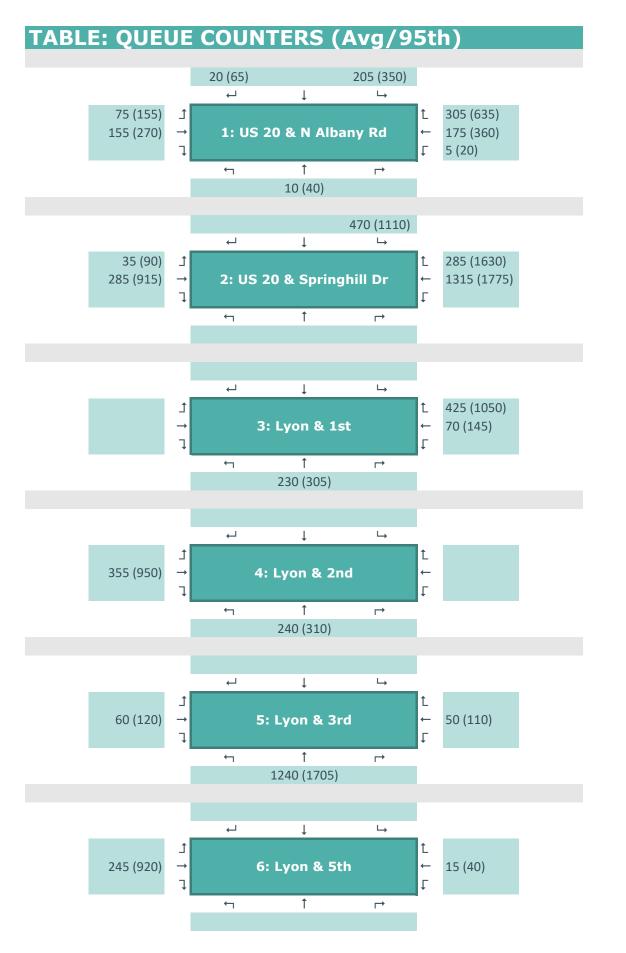
BUNDLE 1 GEH - 4:45 to 5:45 PM Intersection									
		EBR	5	3	1.0				
		EBU	55	51	0.5				
		WBL	0	0					
		WBT	5	3	1.0				
		Total	2865	2904	0.7				
		NBL	45	45	0.0				
		NBR	10	10	0.0				
	Ellsworth & 9th	SBL	1130	1119	0.3				
0		SBT	510	505	0.2				
8		SBR	55	54	0.1				
		EBT	210	211	0.1				
		EBR	5	6	0.4				
		Total	1965	1948	0.4				
		SBL	30	30	0.0				
9		SBT	1500	1488	0.3				
	Ellsworth & 5th	SBR	40	41	0.2				
		EBT	55	56	0.1				
		EBR	55	53	0.3				
		WBL	25	22	0.6				
		WBT	35	41	1.0				
		Total	1740	1730	0.2				
10		SBL	60	57	0.4				
		SBT	1480	1468	0.3				
		SBR	40	37	0.5				
		EBT	100	101	0.1				
	Ellsworth & 3rd	EBR	85	81	0.4				
		WBL	65	59	0.8				
		WBT	115	121	0.6				
		Total	1945	1926	0.4				
		SBL	490	486	0.2				
11		SBT	1440	1426	0.2				
	Ellsworth & 2nd	EBT	460	361	4.9				
		EBR	140	114	2.3				
		Total	2530	2386	2.9				
		SBT	1855	1833	0.5				
12	Ellsworth & 1st	SBR	175	176	0.1				
			75		0.1				
		WBL		79					
		WBT	140 2245	145 2233	0.4				
		Total							
	Ellsworth & 6th	SBL	5	0	3.2				
13		SBT	1560	1548	0.3				
		SBR	15	13	0.5				
		EBT	5	6	0.4				
		EBR	25	24	0.2				
		WBL	10	4	2.3				
		WBT	10	13	0.9				
		Total	1630	1609	0.5				

BUNDLE 1 PM	м реак но	OUR (4:45-5	5:45 PM) I	DELAY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
		Left	4	58
		Through	5	51
	NB	Right	9	15
		Total	18	35
		Left	639	33
	SB	Through	11	33
	56	Right	125	7
		Total	775	29
US 20 & N Albany Rd		Left	103	53
	EB	Through	834	14
	ED	Right	1	21
		Total	938	18
		Left	5	58
	WB	Through	824	18
	VV D	Right	870	20
		Total	1699	19
		Tota	l 3430	21
		Left	570	84
	SB	Right	20	74
		Total	590	84
	EB	Left	45	58
US 20 & Springhill Dr		Through	1442	19
		Total	1487	20
		Through	1683	35
	WB	Right	837	36
		Total	2520	35
		Tota	l 4597	36
		Left	89	5
	NB	Through	1761	8
		Total	1850	8
Lyon & 1st		Through	133	46
	WB	Right	764	93
		Total	897	86
		Tota	l 2747	33
		Through	1580	12
	NB	Right	70	14
		Total	1650	12
Lyon & 2nd		Left	268	33
	EB	Through	647	31
		Total	915	32
		Tota	l 2565	19

BUNDLE 1 P	М РЕАК НС	OUR (4:45-5:	45 PM) I	DELAY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
		Left	100	18
	NB	Through	1540	19
	ND	Right	40	18
		Total	1680	19
		Left	66	19
Lyon & 3rd	EB	Through	91	21
		Total	157	20
		Through	80	25
	WB	Right	42	13
		Total	122	21
		Total	1959	19
		Left	41	14
	NB	Through	1558	18
		Right	36	15
		Total	1635	18
	EB	Left	41	237
Lyon & 5th		Through	49	212
		Total	90	224
	WB	Through	22	20
		Right Total	9 <b>31</b>	26 <b>22</b>
		Total	1756	22
		Left	637	71
	NB	U-Turn	5	69
	IND.	Total	642	70
		Through	6	54
	SB	Right	910	46
		Total	916	46
		Left	1284	31
Lyon & 9th		Through	7	19
	EB	Right	3	5
		U-Turn	51	44
		Total	1345	31
	14/12	Through	3	58
	WB	Total	3	58
		Total	2906	45
		Left	45	42
	NB	Right	10	22
		Total	55	39
		Left	1119	24
	CP	Through	505	10

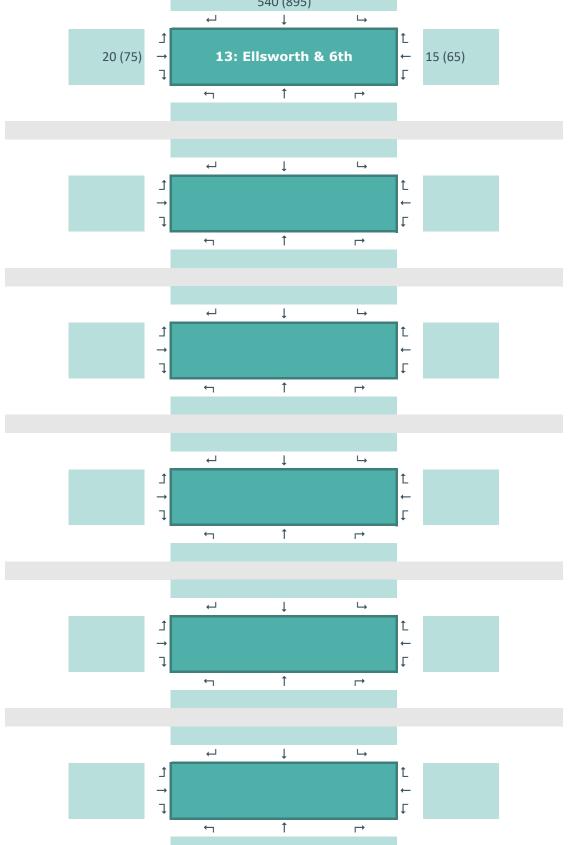
		OUR (4:45-5)		Average
Intersection	Approach	Movement	Volume	Delay (s)
Ellsworth & 9th	30	Right	54	(
		Total	1678	19
		Through	211	4(
	EB	Right	6	22
		Total	217	40
		Total	1950	22
		Left	30	2
	SB	Through	1488	1
	30	Right	41	1
		Total	1559	13
		Through	56	13
Ellsworth & 5th	EB	Right	53	12
		Total	109	133
		Left	22	1
	WB	Through	41	1
		Total	63	1!
		Total	1731	20
	<b>SB</b> F F 1	Left	57	
		Through	1468	
		Right	37	
		Total	1562	
		Through	101	5
Ellsworth & 3rd	EB	Right	81	5
		Total	182	5
		Left	59	1
	WB	Through	121	2
		Total	180	20
		Total		13
		Left	486	
	SB	Through	1426	
		Total	1912	!
Ellsworth & 2nd		Through	361	26
	EB	Right	114	19
		Total	475	249
		Total	1922	54
	CP	Through	1833	4
	SB	Right	176	4
		Total	2009	4!
Ellowerth 9 1 at				
Ellsworth & 1st	WB	Left Through	79 145	4

BUNDLE 1 PM PEAK HOUR (4:45-5:45 PM) DELAY							
Intersection	Approach	Movement	Volume	Average Delay (s			
		Total	2233	44			
		Through	1548	1			
	SB	Right	13	1			
		Total	1561	18			
		Through	6	5			
Ellsworth & 6th	EB	Right	24	6			
Elisworth & oth		Total	30	6			
		Left	4	7			
	WB	Through	13	5			
		Total	17	62			
		Total	1608	19			



#### **TABLE: QUEUE COUNTERS (Avg/95th)** 440 (910) ⊣ Ţ $\rightarrow$ 380 (420) 1 Ĺ 7: Lyon & 9th 5 (40) ← **→** J L ← 1 ⊢ 285 (685) 50 (200) 590 (875) 765 (885) ┙ ╘ Ţ 1 Ĺ 130 (250) $\rightarrow$ 8: Ellsworth & 9th ← ļ L 1 ← $\rightarrow$ 40 (85) ┙ ╘ Ţ 1 Ĺ 130 (495) 9: Ellsworth & 5th 25 (60) $\rightarrow$ ← ļ Γ 1 ← $\rightarrow$ 715 (880) ┙ Ţ $\Box$ 1 Ĺ 10: Ellsworth & 3rd 135 (400) $\rightarrow$ ← 75 (160) L ļ 1 ← $\rightarrow$ 125 (305) 90 (305) ⊣ Ţ $\hookrightarrow$ 1 Ĺ 570 (615) 11: Ellsworth & 2nd ← $\rightarrow$ L J 1 ← $\rightarrow$ 990 (1665) ⊣ $\mapsto$ Ţ 1 Ĺ **→** 12: Ellsworth & 1st ← 85 (135) ļ L 1 ← $\rightarrow$

# TABLE: QUEUE COUNTERS (Avg/95th) 540 (895)



Latent Demand

	Average	Vehicle Hours	Latent		Vehicle Miles	
	Delay / veh	of Delay	Demand	Latent Delay	Travelled	Travel Time
	(sec)	(hrs)	(veh)	(veh-hrs)	(mi)	(hrs)
Avg	1036.2	627.9	52.5	65.6	11933.2	1071.5
StdDev	160.1	108.0	24.7	42.3	184.2	107.2
Min	739.8	430.4	0.0	0.7	11643.1	875.6
Max	1284.7	795.9	90.0	131.0	12274.9	1234.5

Avg delay/vehicle (min/veh)

3.18

### 400-415 PM

1000 ft

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### 415-430 PM

1000 ft

Maxar

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mme

#### 430-445 PM

1000 ft

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### 445-500 PM

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1000 ft

mmg

1000 ft

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### 515-530 PM

1000 ft

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1000 ft

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## 545-600 PM

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#### **APPENDIX H: PROJECT BUNDLE 2 RESULTS**

GEH, DELAY, QUEUING, AND SYSTEM MEASURES



DKS

	BUNDLE 2 GEH - 4:45 to 5:45 PM							
Intersection								
Number	Intersection Name	Movement	Input Volume	VISSIM Output Volume	GEH			
		NBL	5	6	0.4			
		NBT	5	5	0.0			
		NBR	10	9	0.3			
		SBL	625	618	0.3			
		SBT	10	10	0.0			
		SBR	125	127	0.2			
1	US 20 & N Albany Rd	EBL	110	104	0.6			
_		EBT	840	833	0.2			
		EBR	0	1	1.4			
		WBL	5	4	0.5			
		WBT	805	798	0.2			
		WBR	855	850	0.2			
		Total	3395	3363	0.6			
		SBL	600	557	1.8			
		SBR	20	17	0.7			
		EBL	45	46	0.1			
2	US 20 & Springhill Dr	EBT	1430	1413	0.5			
		WBT	1645	1638	0.2			
		WBR	800	817	0.6			
		Total	4540	4486	0.8			
		NBL	85	85	0.0			
		NBT	1700	1707	0.2			
3	Lyon & 1st	WBT	130	136	0.5			
_		WBR	745	757	0.4			
		Total	2660	2684	0.5			
		NBT	1500	1524	0.6			
		NBR	65	72	0.8			
4	Lyon & 2nd	EBL	285	268	1.0			
	_,	EBT	665	639	1.0			
		Total	2515	2501	0.3			
		NBL	95	99	0.4			
		NBT	1460	1487	0.7			
		NBR	40	40	0.0			
		EBL	65	68	0.4			
5	Lyon & 3rd	EBT	95	91	0.4			
		WBT	85	79	0.7			
		WBR	40	43	0.5			
		Total	1880	1906	0.6			
		NBL	40	39	0.2			
		NBT	1485	1516	0.8			
		NBR	35	37	0.3			
		EBL	40	37	0.5			
6	Lyon & 5th	EBT	45	45	0.0			
		WBT	20	22	0.4			
		WBR	10	9	0.3			
		Total	1675	1705	0.7			
		NBL	605	639	1.4			
		NBU	5	5	0.0			
		SBT	5	5	0.0			
		SBR	895	886	0.3			
		EBL	1285	1262	0.6			
1	Lyon & 9th	EBT	5	7	0.8			

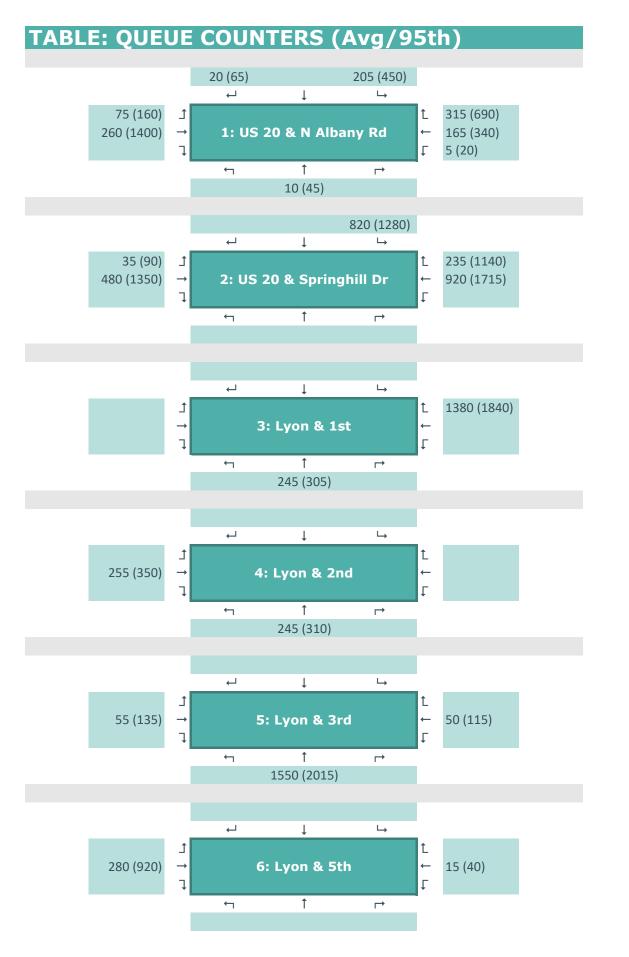
	BUNDL	E 2 G <u>EH</u> -	4:45 to 5:4	5 PM	
Intersection					
Number	Intersection Name	Movement	Input Volume	VISSIM Output Volume	GEH
		EBR	5	2	1.6
		EBU	55	51	0.5
		WBL	0	0	
		WBT	5	3	1.0
		Total	2865	2859	0.1
		NBL	45	44	0.1
		NBR	10	11	0.3
		SBL	1130	1098	1.0
0		SBT	510	495	0.7
8	Ellsworth & 9th	SBR	55	52	0.4
		EBT	210	210	0.0
		EBR	5	6	0.4
		Total	1965	1916	1.1
		SBL	30	30	0.0
		SBT	1500	1452	1.2
		SBR	40	41	0.2
		EBT	55	56	0.1
9	Ellsworth & 5th	EBR	55	52	0.4
		WBL	25	22	0.6
		WBT	35	41	1.0
		Total	1740	1691	1.2
		SBL	60	56	0.5
		SBT	1480	1436	1.2
		SBR	40	38	0.3
		EBT	100	104	0.4
10	Ellsworth & 3rd	EBR	85	81	0.4
		WBL	65	59	0.8
		WBE	115	119	0.4
		Total	1945	1892	1.2
		SBL	490	481	0.4
		SBT	1440	1391	1.3
11	Ellsworth & 2nd	EBT	460	366	4.6
ΤT		EBR	140	143	0.3
		Total	2530	2380	3.0
		SBT	1855	1795	1.4
10		SBR	175	173	0.2
12	Ellsworth & 1st	WBL	75	78	0.3
		WBT	140	141	0.1
		Total	2245	2186	1.3
		SBL	5	0	3.2
		SBT	1560	1514	1.2
		SBR	15	13	0.5
13	Ellsworth & 6th	EBT	5	6	0.4
		EBR	25	25	0.0
		WBL	10	5	1.8
		WBT	10	14	1.2
		Total	1630	1574	1.4

BUNDLE 2 PM	и реак но	)UR (4:45-	5:45 PM)	DELAY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
		Left	6	65
		Through	5	57
	NB	Right	9	15
		Total	20	41
		Left	618	35
	SB	Through	10	34
	30	Right	127	7
		Total	755	30
US 20 & N Albany Rd		Left	104	55
	EB	Through	833	25
	LD	Right	1	18
		Total	938	28
		Left	4	61
	WB	Through	798	17
	WV D	Right	850	20
		Total	1652	19
		Tota	al 3365	24
	SB	Left	557	160
		Right	17	147
		Total	574	160
		Left	46	73
US 20 & Springhill Dr	EB	Through	1413	42
		Total	1459	43
		Through	1638	27
	WB	Right	817	27
		Total	2455	27
		Tota		49
		Left	85	6
	NB	Through	1707	9
		Total	1792	9
Lyon & 1st		Through	136	312
	WB	Right	757	352
		Total	893	346
		Tota		121
	ND	Through	1524	3
	NB	Right	72	2
Luce 9 Ded		Total	<b>1596</b>	3
Lyon & 2nd	ED	Left	268	32
	EB	Through	639	31
		Total	907	31
		Tota	al 2503	13

BUNDLE 2 P	М РЕАК НС	OUR (4:45-5:	45 PM) I	DELAY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
		Left	99	19
	ND	Through	1487	22
	NB	Right	40	23
		Total	1626	21
		Left	68	21
Lyon & 3rd	EB	Through	91	21
		Total	159	21
		Through	79	25
	WB	Right	43	12
		Total	122	20
		Total	1907	21
		Left	39	20
	NB	Through	1516	25
		Right	37	23
		Total	1592	25
	EB	Left	37	300
Lyon & 5th		Through	45	258
		Total	82	277
	WB	Through	22	20
		Right	9	32
		Total Total	31	23
		Left	<b>1705</b> 639	125
	NB	U-Turn	5	125
	ND	Total	<b>644</b>	125
		Through	5	73
	SB	Right	886	92
	50	Total	891	92
		Left	1262	33
Lyon & 9th		Through	7	18
	EB	Right	2	74
		U-Turn	51	139
		Total	1322	37
		Through	3	67
	WB	Total	3	67
		Total	2860	74
		Left	44	43
	NB	Right	11	24
		Total	55	39
		Left	1098	25
	SB	Through	495	11

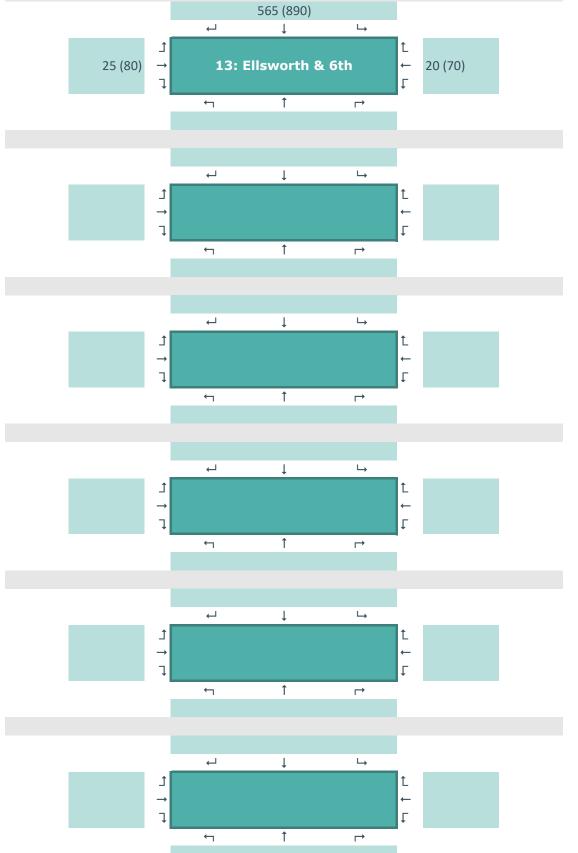
				Average
Intersection	Approach	Movement	Volume	Delay (s
Ellsworth & 9th	30	Right	52	
		Total	1645	20
		Through	210	3
	EB	Right	6	2
		Total	216	39
		Total	1916	23
		Left	30	3
	SB	Through	1452	1
	36	Right	41	1
		Total	1523	1
		Through	56	18
Ellsworth & 5th	EB	Right	52	18
		Total	108	18
		Left	22	1
	WB	Through	41	1
		Total	63	1
		Total	1694	2
		Left	56	
	5B	Through	1436	1
		Right	38	
		Total	1530	
		Through	104	6
Ellsworth & 3rd	EB	Right	81	6
		Total	185	6
		Left	59	1
	WB	Through	119	2
		Total	178	2
		Total	1893	10
	CD	Left	481	
	SB	Through Total	1391	
Ellsworth & 2nd			1872	25
Elisworth & Zhu	EB	Through	366	25
	ED	Right	143	16
		Total Total	509 2381	223
		Through	1795	6
	SB	Right	1793	6
	30	Total	<b>1968</b>	6
Ellsworth & 1st		Left	78	3
	WB	Through	141	2
	110	Total	219	3

BUNDLE 2 PM PEAK HOUR (4:45-5:45 PM) DELAY						
Intersection	Approach	Movement	Volume	Average Delay (s)		
		Total	2187	60		
		Through	1514	2		
	SB	Right	13	2		
		Total	1527	2		
		Through	6	4		
Ellsworth & 6th	EB	Right	25	6		
		Total	31	6		
		Left	5	7		
	WB	Through	14	5		
		Total	19	6		
		Total	1577	2		



#### **TABLE: QUEUE COUNTERS (Avg/95th)** 700 (910) ⊣ Ţ $\Box$ 365 (445) 1 Ĺ 7: Lyon & 9th ← 5 (25) **→** J L ⊢ ← 1 425 (690) 100 (205) 515 (875) 725 (885) ┙ ╘ Ţ 1 Ĺ 120 (250) $\rightarrow$ 8: Ellsworth & 9th ← ļ L 1 ← $\rightarrow$ 40 (90) ┙ ╘ Ţ 1 Ĺ 185 (610) 9: Ellsworth & 5th $\rightarrow$ ← 25 (65) ļ Γ 1 ← $\rightarrow$ 140 (310) ┙ $\Box$ Ţ 1 Ĺ 10: Ellsworth & 3rd 150 (390) 70 (160) $\rightarrow$ ← L ļ 1 ← $\rightarrow$ 140 (305) 95 (295) ⊣ Ţ $\hookrightarrow$ 1 Ĺ 520 (625) 11: Ellsworth & 2nd ← $\rightarrow$ L J 1 ← $\rightarrow$ 1135 (1690) ⊣ $\mapsto$ Ţ 1 Ĺ **→** 12: Ellsworth & 1st ← 80 (135) ļ L 1 ← $\rightarrow$

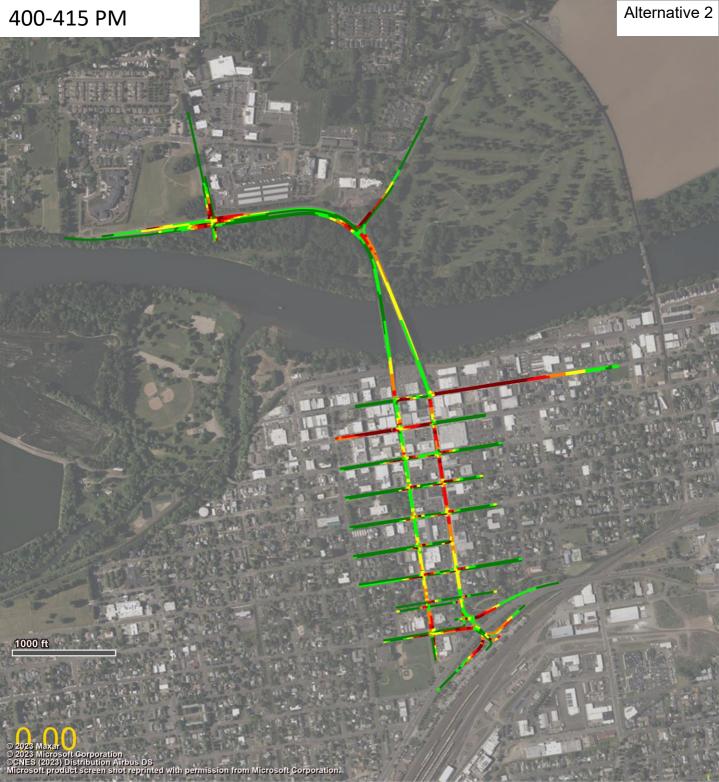
## TABLE: QUEUE COUNTERS (Avg/95th)

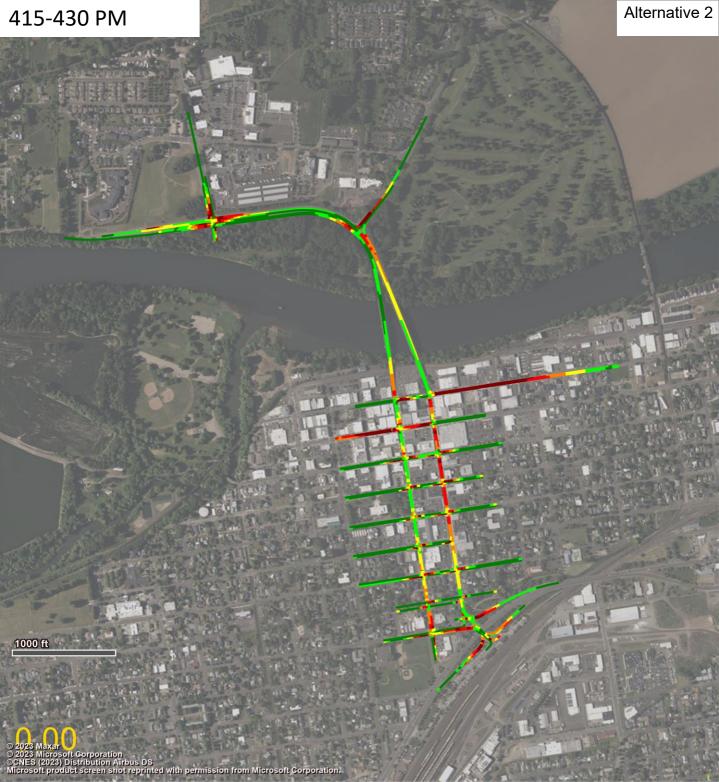


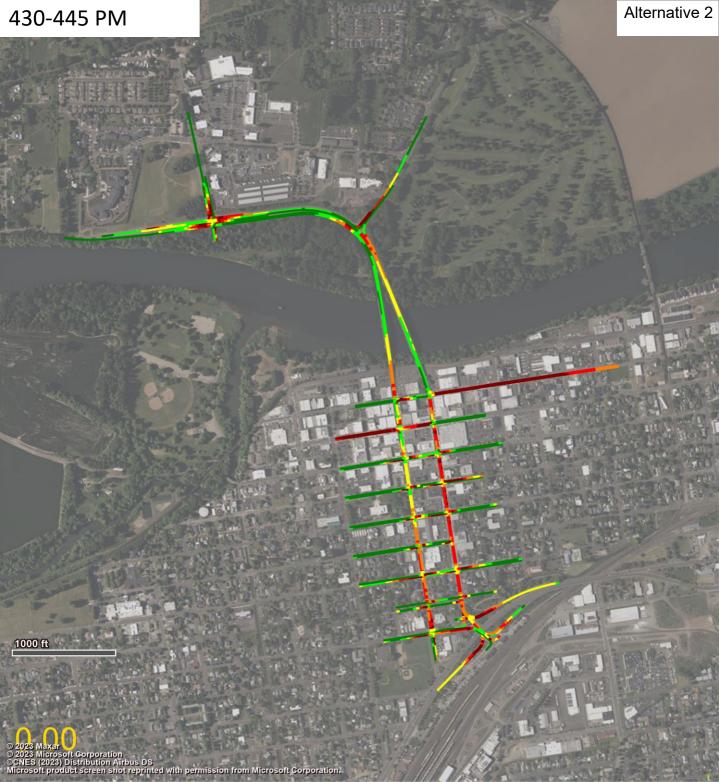
	Average	Vehicle Hours	Latent		Vehicle Miles	
	Delay / veh	of Delay	Demand	Latent Delay	Travelled	Travel Time
	(sec)	(hrs)	(veh)	(veh-hrs)	(mi)	(hrs)
Avg	1357.9	860.1	88.5	121.3	11760.1	1297.1
StdDev	156.8	117.4	45.4	73.7	190.8	113.9
Min	1137.5	697.2	0.0	6.2	11472.6	1139.1
Max	1627.1	1065.9	138.0	227.1	12075.0	1496.6

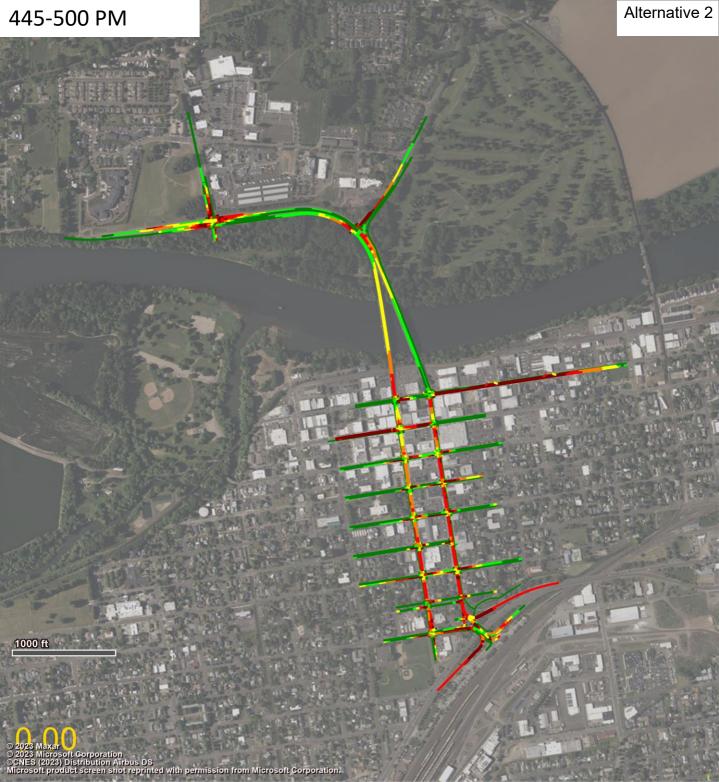
Avg delay/veh (min/veh)

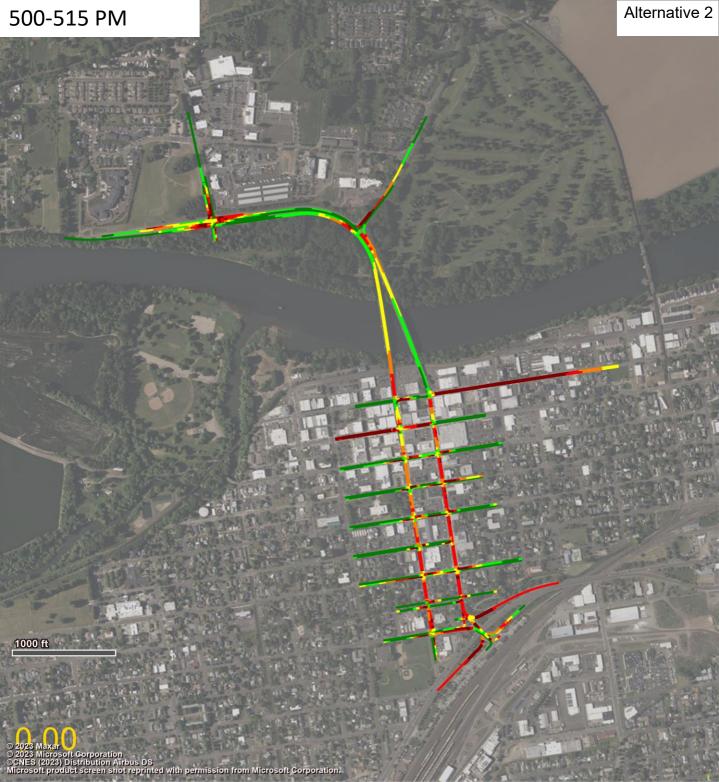
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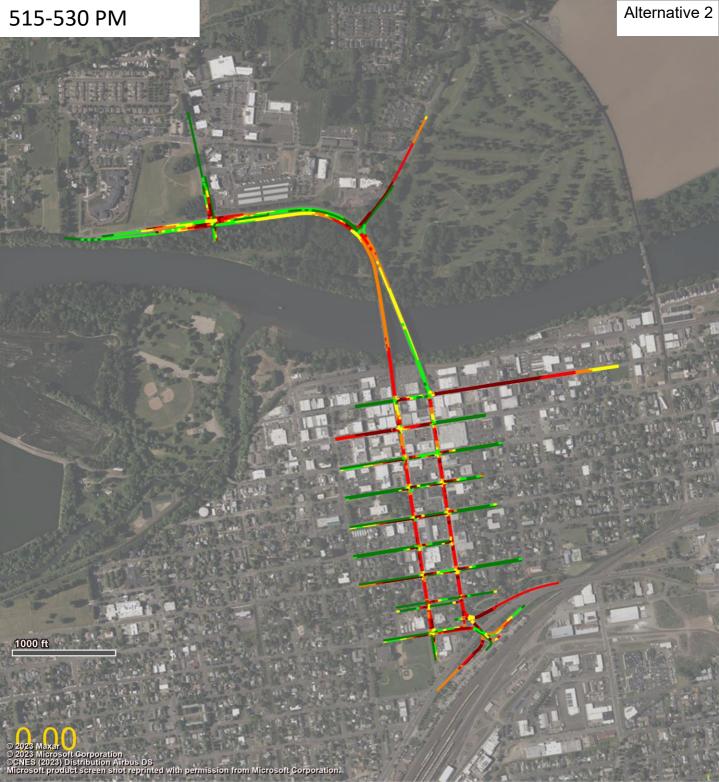


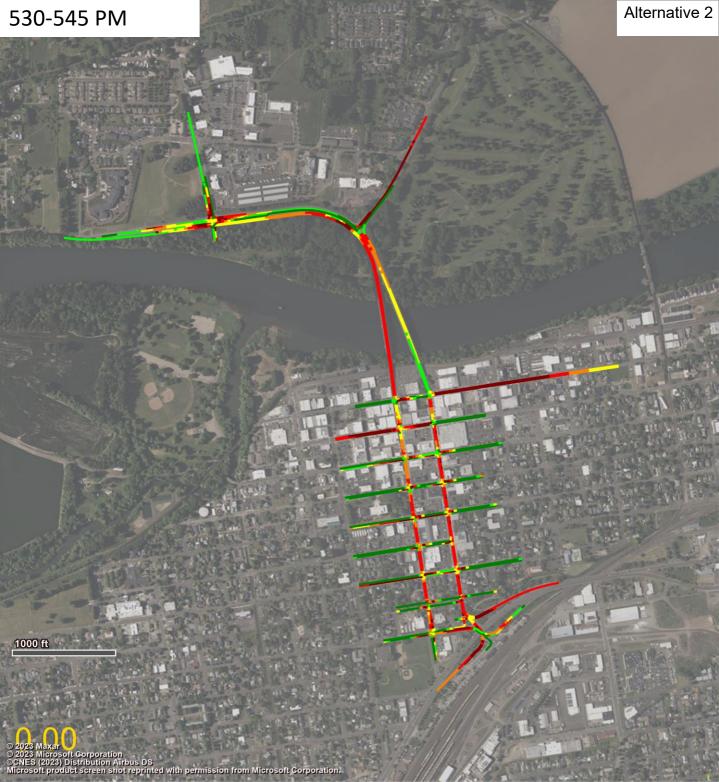


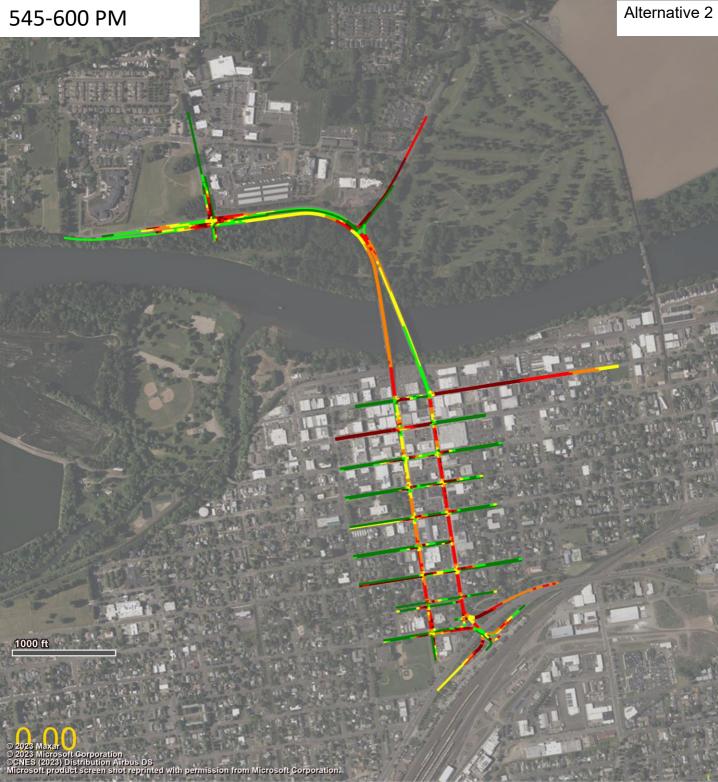












#### **APPENDIX I: PROJECT BUNDLE 3 RESULTS**

GEH, DELAY, QUEUING, AND SYSTEM MEASURES



	BUNDLE 3 GEH - 4:45 to 5:45 PM							
Intersection								
Number	Intersection Name	Movement	Input Volume	VISSIM Output Volume	GEH			
		NBL	5	5	0.0			
		NBT	5	5	0.0			
		NBR	10	9	0.3			
		SBL	625	619	0.2			
		SBT	10	10	0.0			
		SBR	125	126	0.1			
1	US 20 & N Albany Rd	EBL	110	105	0.5			
_		EBT	840	840	0.0			
		EBR	0	0				
		WBL	5	4	0.5			
		WBT	805	822	0.6			
		WBR	855	858	0.1			
		Total	3395	3401	0.1			
		SBL	600	589	0.5			
		SBR	20	18	0.5			
		EBL	45	46	0.1			
2	US 20 & Springhill Dr	EBT	1430	1418	0.3			
		WBT	1645	1663	0.4			
		WBR	800	818	0.6			
		Total	4540	4552	0.2			
		NBL	85	86	0.1			
		NBT	1700	1729	0.7			
3	Lyon & 1st	WBT	130	135	0.4			
		WBR	745	753	0.3			
		Total	2660	2704	0.8			
		NBT	1500	1540	1.0			
		NBR	65	75	1.2			
4	Lyon & 2nd	EBL	285	272	0.8			
	_,	EBT	665	648	0.7			
		Total	2515	2534	0.4			
		NBL	95	99	0.4			
		NBT	1460	1500	1.0			
		NBR	40	38	0.3			
		EBL	65	68	0.4			
5	Lyon & 3rd	EBT	95	91	0.4			
		WBT	85	80	0.6			
		WBR	40	42	0.3			
		Total	1880	1917	0.8			
		NBL	40	40	0.0			
		NBT	1485	1514	0.7			
		NBR	35	35	0.0			
		EBL	40	40	0.0			
6	Lyon & 5th	EBT	45	46	0.1			
		WBT	20	22	0.4			
		WBR	10	9	0.3			
		Total	1675	1707	0.8			
		NBL	605	622	0.7			
		NBU	5	5	0.0			
		SBT	5	5	0.0			
		SBR	895	894	0.0			
		EBL	1285	1271	0.4			

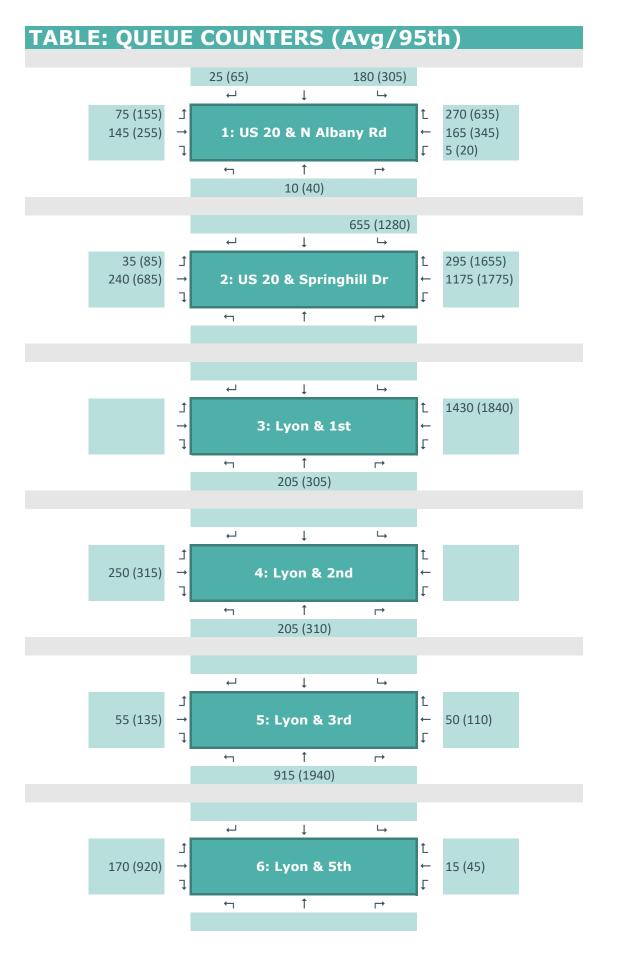
	BUNDL	E 3 GEH -	4:45 to 5:4	5 PM	
Intersection					
Number	Intersection Name	Movement	Input Volume	VISSIM Output Volume	GEH
		EBR	5	3	1.0
		EBU	55	52	0.4
		WBL	0	0	
		WBT	5	3	1.0
		Total	2865	2861	0.1
		NBL	45	43	0.3
		NBR	10	10	0.0
		SBL	1130	1107	0.7
2		SBT	510	503	0.3
8	Ellsworth & 9th	SBR	55	52	0.4
		EBT	210	212	0.1
		EBR	5	5	0.0
		Total	1965	1933	0.7
		SBL	30	30	0.0
		SBT	1500	1467	0.9
		SBR	40	40	0.0
_		EBT	55	54	0.1
9	Ellsworth & 5th	EBR	55	52	0.4
		WBL	25	22	0.6
		WBT	35	41	1.0
		Total	1740	1708	0.8
		SBL	60	57	0.4
		SBT	1480	1453	0.7
		SBR	40	41	0.2
		EBT	100	102	0.2
10	Ellsworth & 3rd	EBR	85	81	0.4
		WBL	65	60	0.6
		WBT	115	118	0.3
		Total	1945	1909	0.8
		SBL	490	482	0.4
		SBT	1440	1408	0.8
11	Ellsworth & 2nd	EBT	460	401	2.8
		EBR	140	126	1.2
		Total	2530	2416	2.3
		SBT	1855	1814	1.0
		SBR	175	178	0.2
12	Ellsworth & 1st	WBL	75	77	0.2
IZ		WBL	140	143	0.2
		Total	2245	2212	0.7
		SBL	5	0	3.2
		SBT	1560	1526	0.9
		SBR	15	14	0.9
		EBT	5	6	0.3
13	Ellsworth & 6th	EBR	25	25	0.4
		WBL	10	5	1.8
			10	13	
		WBT Total	1630	13	0.9

BUNDLE 3 PM	<mark>И РЕАК</mark> НС	OUR (4:45-5)	:45 PM) I	DELAY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
		Left	5	54
	NB	Through	5	57
	ND	Right	9	13
		Total	19	36
		Left	619	32
	SB	Through	10	36
	50	Right	126	7
US 20 & N Albany Rd		Total	755	28
		Left	105	50
	EB	Through	840	13
		Total	945	17
		Left	4	57
	WB	Through	822	18
		Right	858	19
		Total	1684	18
		Total	3403	20
		Left	589	113
	SB	Right	18	110
		Total	607	113
		Left	46	55
US 20 & Springhill Dr	EB	Through	1418	13
		Total	1464	15
	MD	Through	1663	34
	WB	Right	818	36
		Total Total	2481	35
		Left	<b>4552</b> 86	<b>39</b> 5
	NB	Through	1729	7
	ND	Total	1815	7
Lyon & 1st		Through	135	328
	WB	Right	753	370
	WD	Total	888	363
		Total	2703	124
		Through	1540	3
	NB	Right	75	2
		Total	1615	3
Lyon & 2nd		Left	272	31
	EB	Through	648	30
		Total	920	30
		Total	2535	13
		Left	99	15

BUNDLE 3 P	М РЕАК НО	OUR (4:45-5:	45 PM) I	DELAY
				Average
Intersection	Approach	Movement	Volume	Delay (s)
	ND	Through	1500	16
	NB	Right	38	15
		Total	1637	16
		Left	68	19
Lyon & 3rd	EB	Through	91	20
		Total	159	20
		Through	80	24
	WB	Right	42	11
		Total	122	20
		Total	1918	17
		Left	40	11
	NB	Through	1514	13
	ND	Right	35	12
		Total	1589	12
		Left	40	142
Lyon & 5th	EB	Through	46	123
		Total	86	132
		Through	22	24
	WB	Right	9	34
		Total	31	27
		Total	1706	19
		Left	622	53
	NB	U-Turn	5	65
		Total	627	53
		Through	5	29
	SB	Right	894	36
		Total	899	36
Lyon & 9th		Left	1271	31
Lyon & 9th		Through	7	14
	EB	Right	3	2
		U-Turn	52	41
		Total	1333	31
	WB	Through	3	57
	VV D	Total	3	57
		Total	2862	38
		Left	43	41
	NB	Right	10	21
		Total	53	38
		Left	1107	23
	SB	Through	503	11
Ellsworth & 9th	38	Right	52	9

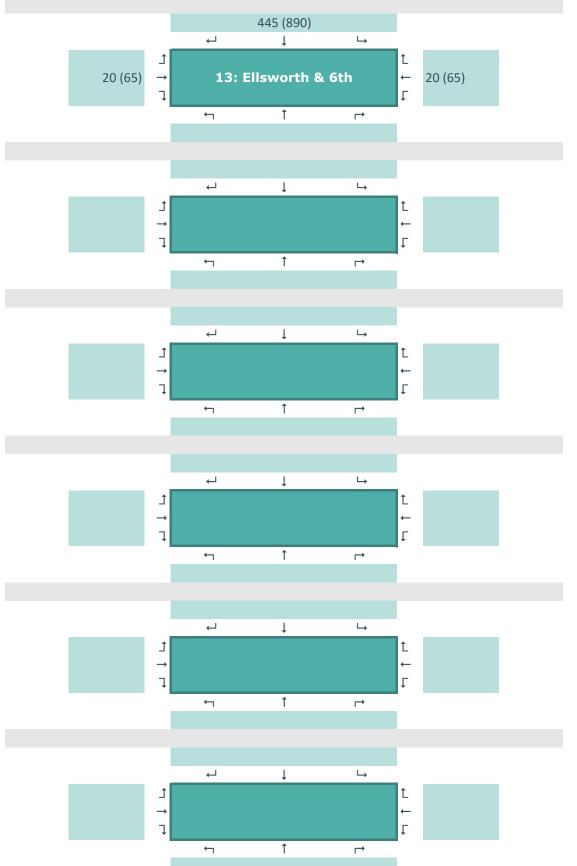
				Averag
Intersection	Approach	Movement	Volume	Delay (
		Total	1662	1
		Through	212	
	EB	Right	5	
		Total	217	3
		Total	1932	2
		Left	30	
	SB	Through	1467	
	36	Right	40	
		Total	1537	1
		Through	54	1
Ellsworth & 5th	EB	Right	52	1
		Total	106	1:
		Left	22	
	WB	Through	41	
		Total	63	:
		Total	1706	:
		Left	57	
	CD	Through	1453	
	SB	Right	41	
		Total	1551	
		Through	102	
Ellsworth & 3rd	EB	Right	81	
		Total	183	
		Left	60	
	WB	Through	118	
		Total	178	2
		Total	1912	1
		Left	482	
	SB	Through	1408	
		Total	1890	
Ellsworth & 2nd		Through	401	2
	EB	Right	126	1
		Total	527	18
		Total	2417	4
		Through	1814	
	SB	Right	178	
		Total	1992	3
Ellsworth & 1st		Left	77	
	WB	Through	143	
		Total	220	3
		Total	2212	3

BUNDLE 3 PM	и реак но	UR (4:45-5:	:45 PM) [	DELAY
Intersection	Approach	Movement	Volume	Average Delay (s)
		Through	1526	16
	SB	Right	14	17
		Total	1540	16
		Through	6	41
Ellsworth & 6th	EB	Right	25	53
		Total	31	51
		Left	5	70
	WB	Through	13	71
		Total	18	71
		Total	1589	17



#### **TABLE: QUEUE COUNTERS (Avg/95th)** 365 (905) ⊣ Ţ $\Box$ 355 (445) 1 Ĺ 7: Lyon & 9th ← 5 (35) **→** J L ← 1 ⊢ 230 (685) 45 (200) 520 (885) 670 (890) ┙ ╘ Ţ 1 Ĺ 125 (270) $\rightarrow$ 8: Ellsworth & 9th ← ļ L 1 ← $\rightarrow$ 35 (85) ┙ ╘ Ţ 1 Ĺ 125 (520) 9: Ellsworth & 5th 25 (60) $\rightarrow$ ← ļ Γ 1 ← $\rightarrow$ 115 (310) ┙ $\Box$ Ţ 1 Ĺ 10: Ellsworth & 3rd 110 (290) 70 (175) $\rightarrow$ ← L ļ 1 ← $\rightarrow$ 115 (305) 90 (295) ⊣ Ţ $\hookrightarrow$ 1 Ĺ 465 (615) 11: Ellsworth & 2nd ← $\rightarrow$ L J 1 ← $\rightarrow$ 790 (1665) ⊣ $\mapsto$ Ţ 1 Ĺ **→** 12: Ellsworth & 1st ← 80 (135) ļ L 1 ← $\rightarrow$

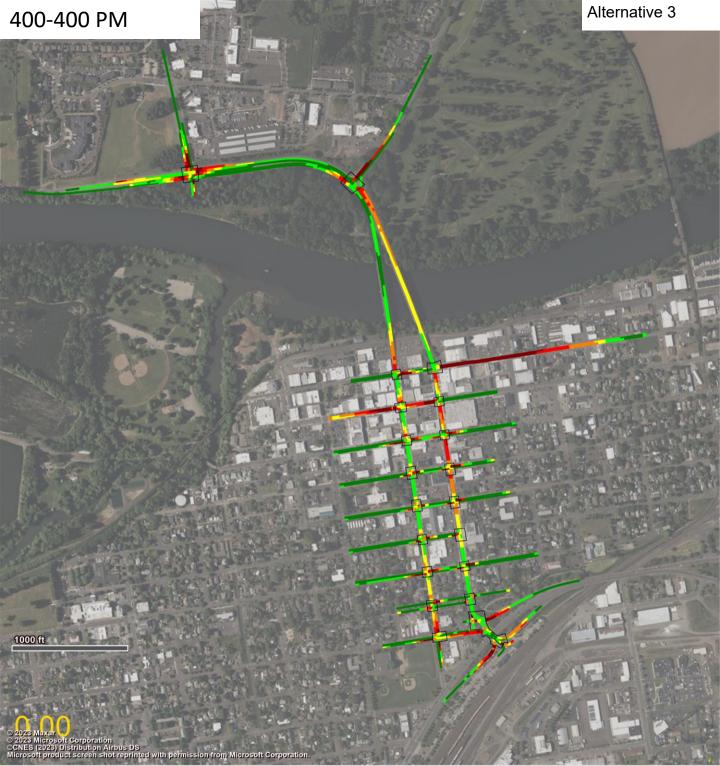
# TABLE: QUEUE COUNTERS (Avg/95th)

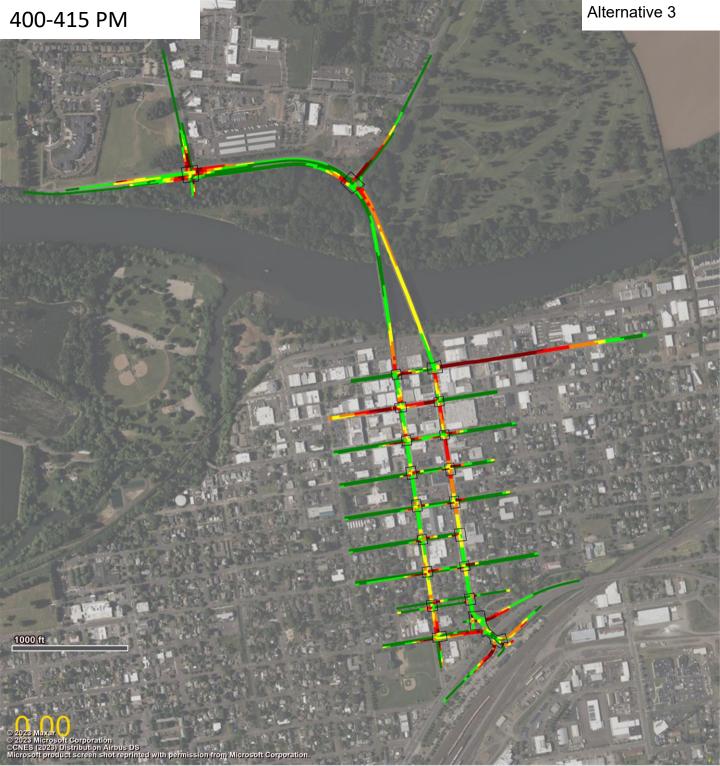


	Average	Vehicle Hours	Latent	Vehicle Miles					
	Delay / veh	of Delay	Demand	Latent Delay	Travelled	Travel Time			
	(sec)	(hrs)	(veh)	(veh-hrs)	(mi)	(hrs)			
Avg	1138.3	698.8	31.8	44.6	11875.8	1140.6			
StdDev	195.8	136.6	32.8	41.6	162.1	135.2			
Min	788.5	461.2	0.0	0.7	11633.6	905.6			
Max	1414.8	898.4	91.0	118.6	12157.5	1338.2			

Avg delay/vehicle (min/veh)

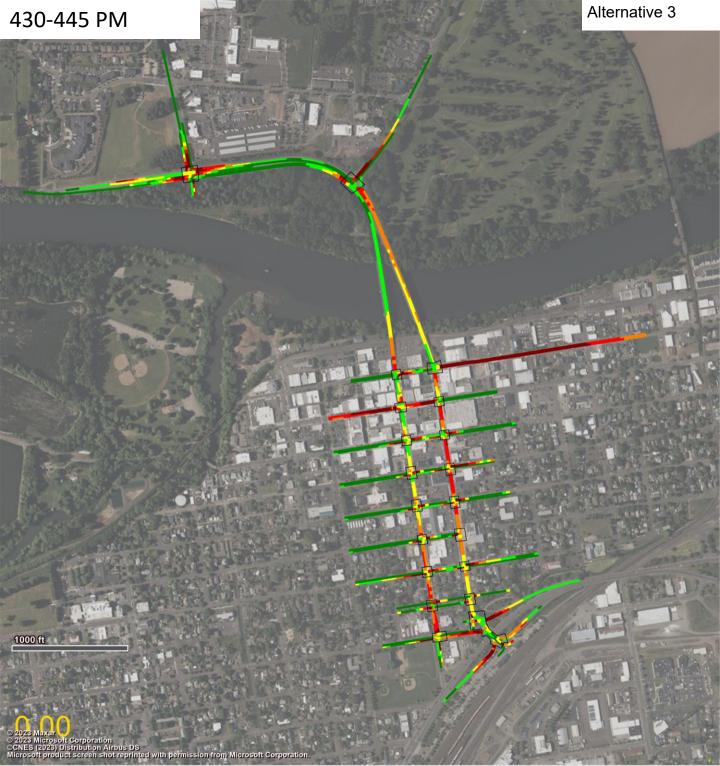
3.40



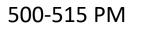


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# **APPENDIX J: PROJECT BUNDLES TRAVEL TIME RESULTS**

**PROJECT BUNDLES 1, 2, AND 3** 



			Projec	t Bundles V	issim Trave	el Time Res	ults				
			Travel Time (Seconds)								
Direction	From/To	Scenario	4:00-4:15	4:15-4:30	4:30-4:45	4:45-5:00	5:00-5:15	5:15-5:30	5:30-5:45	5:45-6:00	Peak Hour (4:45-5:45 PM)
		No-Build	227	243	272	250	245	239	241	216	244
Northbound	Lyon Street north of OR 99E SB Off-	Bundle 1	250	300	346	332	311	311	266	227	305
Northbound	Ramp/US 20 at N Albany Rd	Bundle 2	268	308	354	340	336	337	329	326	335
		Bundle 3	242	269	315	303	270	276	266	233	279
		No-Build	318	408	489	538	599	602	547	557	571
Southbound		Bundle 1	238	273	290	311	351	422	341	316	356
Southbound	US 20 at N Albany Rd/OR 99E NB	Bundle 2	243	286	328	352	420	486	385	364	411
	On-Ramp	Bundle 3	235	277	302	297	334	372	324	346	331

# **APPENDIX B – PROPOSED ALTERNATIVES SYNCHRO** RESULTS

DKS ALBANY US 20 CORRIDOR STUDY • LEVEL 2 EVALUATION MEMORANDUM APPENDICES • APRIL 2024

	٦	-	$\mathbf{F}$	•	-	•	•	Ť	1	1	Ļ	~
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	1	<b>∱1</b> ≱		ľ	- <b>†</b> †	1		\$		1	ŧ	1
Traffic Volume (vph)	110	660	5	10	865	470	5	0	10	988	5	130
Future Volume (vph)	110	660	5	10	865	470	5	0	10	988	5	130
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Lane Width	12	12	12	12	12	16	12	12	12	12	12	16
Total Lost time (s)	4.0	4.0		4.0	4.0	4.0		4.0		4.0	4.0	4.0
Lane Util. Factor	1.00	0.95		1.00	0.95	1.00		1.00		0.95	0.95	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	0.99		1.00		1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00		1.00		1.00	1.00	1.00
Frt	1.00	1.00		1.00	1.00	0.85		0.91		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00		0.98		0.95	0.95	1.00
Satd. Flow (prot)	1646	3225		1662	3260	1653		1563		1533	1531	1616
Flt Permitted	0.95	1.00		0.95	1.00	1.00		0.98		0.95	0.95	1.00
Satd. Flow (perm)	1646	3225		1662	3260	1653		1563		1533	1531	1616
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	120	717	5	11	940	511	5	0	11	1074	5	141
RTOR Reduction (vph)	0	1	0	0	0	121	0	16	0	0	0	78
Lane Group Flow (vph)	120	721	0	11	940	390	0	0	0	591	488	63
Confl. Bikes (#/hr)						1						1
Heavy Vehicles (%)	1%	3%	0%	0%	2%	1%	0%	0%	0%	3%	17%	3%
Turn Type	Prot	NA		Prot	NA	pm+ov	Split	NA		Split	NA	Perm
Protected Phases	5	2		1	6	4	8	8		4	4	
Permitted Phases	•	_			•	6	•	•			•	4
Actuated Green, G (s)	13.0	57.3		1.7	46.0	100.4		1.7		54.4	54.4	54.4
Effective Green, g (s)	13.5	58.5		2.2	47.2	102.4		2.2		55.4	55.4	55.4
Actuated g/C Ratio	0.10	0.44		0.02	0.35	0.76		0.02		0.41	0.41	0.41
Clearance Time (s)	4.5	5.2		4.5	5.2	5.0		4.5		5.0	5.0	5.0
Vehicle Extension (s)	2.5	4.0		2.5	4.0	2.5		2.5		2.5	2.5	2.5
Lane Grp Cap (vph)	165	1404		27	1145	1260		25		632	631	666
v/s Ratio Prot	c0.07	0.22		0.01	c0.29	0.13		c0.00		c0.39	0.32	000
v/s Ratio Perm	00.01	0.22		0.01	00.20	0.10		00.00		00.00	0.02	0.04
v/c Ratio	0.73	0.51		0.41	0.82	0.31		0.01		0.94	0.77	0.09
Uniform Delay, d1	58.6	27.6		65.4	39.7	5.0		65.0		37.7	34.0	24.1
Progression Factor	1.00	1.00		1.00	1.00	1.00		1.00		1.00	1.00	1.00
Incremental Delay, d2	13.9	0.4		7.1	5.1	0.1		0.1		21.1	5.6	0.0
Delay (s)	72.5	28.0		72.5	44.8	5.1		65.1		58.9	39.7	24.2
Level of Service	72.5 E	20.0 C		72.5 E	D	А		E		50.5 E	D	24.2 C
Approach Delay (s)		34.3			31.1	Λ		65.1		-	47.2	Ŭ
Approach LOS		C			C			E			D	
Intersection Summary												
HCM 2000 Control Delay			37.6	Н	CM 2000	) Level of	Service		D			
HCM 2000 Volume to Capa	acity ratio		0.85									
Actuated Cycle Length (s)			134.3	S	um of los	st time (s)			16.0			
Intersection Capacity Utiliza	ation		79.1%			of Service	)		D			
Analysis Period (min)			15									
c Critical Lane Group												

	≯	+	+	×.	1	1		
Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations	٢	<b>†</b> †	<b>†</b> †	1	ኘዣ	02.1		
Traffic Volume (vph)	35	1623	1285	575	562	60		
Future Volume (vph)	35	1623	1285	575	562	60		
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750		
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0			
Lane Util. Factor	1.00	0.95	0.95	1.00	0.97			
Frpb, ped/bikes	1.00	1.00	1.00	0.98	1.00			
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00			
Frt	1.00	1.00	1.00	0.85	0.99			
Flt Protected	0.95	1.00	1.00	1.00	0.96			
Satd. Flow (prot)	1583	3260	3260	1439	3170			
Flt Permitted	0.95	1.00	1.00	1.00	0.96			
Satd. Flow (perm)	1583	3260	3260	1439	3170			
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92		
Adj. Flow (vph)	38	1764	1397	625	611	65		
RTOR Reduction (vph)	0	0	0	025	7	0		
Lane Group Flow (vph)	38	1764	1397	625	669	0		
Confl. Bikes (#/hr)	50	1704	1007	7	005	1		
Heavy Vehicles (%)	5%	2%	2%	1%	0%	8%		
Turn Type	Prot	NA	NA	Free	Prot	070		
Protected Phases	1	6	2	TIEE	8			
Permitted Phases	1	6	2	Free	0			
Actuated Green, G (s)	3.1	65.2	58.1	101.5	26.8			
Effective Green, g (s)	3.1	66.2	59.1	101.5	27.3			
Actuated g/C Ratio	0.03	0.65	0.58	1.00	0.27			
Clearance Time (s)	4.0	5.0	5.0	1.00	4.5			
Vehicle Extension (s)	2.5	4.7	6.0		2.5			
	48	2126	1898	1439	852			
Lane Grp Cap (vph) v/s Ratio Prot	40 0.02	c0.54	0.43	1409	c0.21			
v/s Ratio Prot	0.02	0.54	0.43	0.43	60.Z I			
v/c Ratio	0.79	0.83	0.74	0.43	0.78			
Uniform Delay, d1	48.9	13.4	15.5	0.43	34.4			
Progression Factor	48.9	1.00	1.00	1.00	1.00			
Incremental Delay, d2	57.1	3.1	2.1	1.00	4.6			
Delay (s)	105.9	16.5	17.6	1.0	39.0			
Level of Service	105.9 F	10.5 B	17.0 B	1.0 A	39.0 D			
Approach Delay (s)	Г	18.4	ы 12.5	A	39.0			
Approach LOS		10.4 B	12.5 B		39.0 D			
		D	D		U			
Intersection Summary			10.0		014 6 6 6 6			
HCM 2000 Control Delay			18.8	Н	CM 2000	Level of Service	В	
HCM 2000 Volume to Capac	city ratio		0.85	•	<b>.</b>		10.0	
Actuated Cycle Length (s)			101.5		um of lost		12.0	
Intersection Capacity Utilizat	lion		74.8%	IC	CU Level o	of Service	D	
Analysis Period (min)			15					
<ul> <li>Critical Lane Group</li> </ul>								

#### HCM Signalized Intersection Capacity Analysis 3: Ellsworth Street & 1st Avenue

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					-4†						<b>∱</b> }	
Traffic Volume (vph)	0	0	0	35	115	0	0	0	0	0	2010	185
Future Volume (vph)	0	0	0	35	115	0	0	0	0	0	2010	185
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)					4.0						4.0	
Lane Util. Factor					0.95						0.95	
Frpb, ped/bikes					1.00						1.00	
Flpb, ped/bikes					0.99						1.00	
Frt					1.00						0.99	
Flt Protected					0.99						1.00	
Satd. Flow (prot)					3230						3216	
Flt Permitted					0.99						1.00	
Satd. Flow (perm)					3230						3216	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	0	0	0	38	125	0	0	0	0	0	2185	201
RTOR Reduction (vph)	0	0	0	0	10	0	0	0	0	0	9	0
Lane Group Flow (vph)	0	0	0	0	153	0	0	0	0	0	2377	0
Confl. Peds. (#/hr)	9		18	18		9	10		9	9		10
Confl. Bikes (#/hr)												2
Heavy Vehicles (%)	0%	0%	0%	2%	1%	0%	0%	0%	0%	0%	2%	1%
Turn Type				Perm	NA						NA	
Protected Phases					4						2	
Permitted Phases				4	-						_	
Actuated Green, G (s)				•	21.0						51.0	
Effective Green, g (s)					21.0						51.0	
Actuated g/C Ratio					0.26						0.64	
Clearance Time (s)					4.0						4.0	
Lane Grp Cap (vph)					847						2050	
v/s Ratio Prot					041						c0.74	
v/s Ratio Perm					0.05						00.11	
v/c Ratio					0.18						1.16	
Uniform Delay, d1					22.8						14.5	
Progression Factor					0.61						1.00	
Incremental Delay, d2					0.4						77.7	
Delay (s)					14.3						92.2	
Level of Service					B						F	
Approach Delay (s)		0.0			14.3			0.0			92.2	
Approach LOS		A			B			A			F	
Intersection Summary												
HCM 2000 Control Delay			87.3	Н	CM 2000	Level of S	Service		F			
HCM 2000 Volume to Capacit	tv ratio		0.87									
Actuated Cycle Length (s)	.,		80.0	S	um of lost	time (s)			8.0			
Intersection Capacity Utilization	on		90.1%			of Service			E			
Analysis Period (min)			15						_			
c Critical Lane Group												

#### HCM Signalized Intersection Capacity Analysis 4: Lyon Street & 1st Avenue

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					↑	77		-4 <b>†</b>				
Traffic Volume (vph)	0	0	0	0	85	580	65	1280	0	0	0	0
Future Volume (vph)	0	0	0	0	85	580	65	1280	0	0	0	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)					4.0	4.0		5.5				
Lane Util. Factor					1.00	0.88		0.95				
Frpb, ped/bikes					1.00	0.96		1.00				
Flpb, ped/bikes					1.00	1.00		1.00				
Frt					1.00	0.85		1.00				
Flt Protected					1.00	1.00		1.00				
Satd. Flow (prot)					1733	2491		3251				
Flt Permitted					1.00	1.00		1.00				
Satd. Flow (perm)					1733	2491		3251				
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	0	0	0	0	92	630	71	1391	0	0	0	0
RTOR Reduction (vph)	0	0	0	0	0	0	0	36	0	0	0	0
Lane Group Flow (vph)	0	0	0	0	92	630	0	1426	0	0	0	0
Confl. Peds. (#/hr)	30		2	2		30	4		2	2		4
Confl. Bikes (#/hr)						1			4			
Heavy Vehicles (%)	0%	0%	0%	0%	1%	1%	2%	2%	0%	0%	0%	0%
Turn Type					NA	custom	Perm	NA				
Protected Phases					4	3		6				
Permitted Phases						4	6					
Actuated Green, G (s)					32.6	32.6		37.9				
Effective Green, g (s)					32.6	32.6		37.9				
Actuated g/C Ratio					0.41	0.41		0.47				
Clearance Time (s)					4.0	4.0		5.5				
Vehicle Extension (s)					2.5	2.5		4.0				
Lane Grp Cap (vph)					706	1015		1540				
v/s Ratio Prot					0.05	c0.12		1010				
v/s Ratio Perm					0.00	0.13		0.44				
v/c Ratio					0.13	0.62		0.93				
Uniform Delay, d1					14.8	18.8		19.7				
Progression Factor					1.00	1.00		0.69				
Incremental Delay, d2					0.4	2.9		8.5				
Delay (s)					15.2	21.7		22.1				
Level of Service					B	C		C				
Approach Delay (s)		0.0			20.8	Ŭ		22.1			0.0	
Approach LOS		A			C			С			A	
Intersection Summary												
HCM 2000 Control Delay			21.7	Н	CM 200	) Level of	Service		С			
HCM 2000 Volume to Capacity	/ ratio		0.83						-			
Actuated Cycle Length (s)			80.0	S	um of los	st time (s)			13.5			
Intersection Capacity Utilization	n		73.1%			of Service	)		D			
Analysis Period (min)			15						_			
c Critical Lane Group												

# HCM Signalized Intersection Capacity Analysis 5: Ellsworth Street & 2nd Avenue

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		<b>∱1</b> ≱								1	<u></u>	
Traffic Volume (vph)	0	375	105	0	0	0	0	0	0	510	1535	0
Future Volume (vph)	0	375	105	0	0	0	0	0	0	510	1535	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)		4.0								1.0	4.0	
Lane Util. Factor		0.95								1.00	0.95	
Frpb, ped/bikes		1.00								1.00	1.00	
Flpb, ped/bikes		1.00								1.00	1.00	
Frt		0.97								1.00	1.00	
Flt Protected		1.00								0.95	1.00	
Satd. Flow (prot)		3173								1662	3260	
Flt Permitted		1.00								0.95	1.00	
Satd. Flow (perm)		3173								1662	3260	
	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	0	408	114	0	0	0	0	0	0	554	1668	0
RTOR Reduction (vph)	0	29	0	0	0	0	0	0	0	159	0	0
Lane Group Flow (vph)	0	493	0	0	0	0	0	0	0	395	1668	0
Confl. Peds. (#/hr)	1	100	2	2	Ŭ	1	1	Ű	1	1	1000	1
Confl. Bikes (#/hr)	•		1	_		•	•			•		1
Heavy Vehicles (%)	0%	1%	1%	0%	0%	0%	0%	0%	0%	0%	2%	0%
Turn Type	0,0	NA	170	0,0	0,0	0,0	0,0	0,0	0,0	Prot	NA	0,0
Protected Phases		8								5	2	
Permitted Phases		U								Ū	2	
Actuated Green, G (s)		11.7								29.7	60.3	
Effective Green, g (s)		11.7								30.7	60.3	
Actuated g/C Ratio		0.15								0.38	0.75	
Clearance Time (s)		4.0								2.0	4.0	
Vehicle Extension (s)		2.5								2.5	4.0	
Lane Grp Cap (vph)		464								637	2457	
v/s Ratio Prot		c0.16								0.24	c0.51	
v/s Ratio Perm		00.10								0.24	00.01	
v/c Ratio		1.06								0.62	0.68	
Uniform Delay, d1		34.1								19.9	5.0	
Progression Factor		1.00								1.43	0.11	
Incremental Delay, d2		59.3								0.1	0.11	
Delay (s)		93.5								28.7	0.7	
Level of Service		55.5 F								20.7 C	0.7 A	
Approach Delay (s)		93.5			0.0			0.0		U	7.7	
Approach LOS		95.5 F			0.0 A			0.0 A			7.7 A	
		Г			A			A			~	
Intersection Summary												
HCM 2000 Control Delay			24.0	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacity r	ratio		0.74									
Actuated Cycle Length (s)			80.0		um of los				8.0			
Intersection Capacity Utilization			90.1%	IC	CU Level	of Service			E			
Analysis Period (min)			15									
c Critical Lane Group												

#### HCM Signalized Intersection Capacity Analysis 6: Lyon Street & 2nd Avenue

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations								<b>≜</b> ⊅				
Traffic Volume (vph)	255	630	0	0	0	0	0	1090	30	0	0	0
Future Volume (vph)	255	630	0	0	0	0	0	1090	30	0	0	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)		4.0						4.0				
Lane Util. Factor		0.95						0.95				
Frpb, ped/bikes		1.00						1.00				
Flpb, ped/bikes		1.00						1.00				
Frt		1.00						1.00				
Flt Protected		0.99						1.00				
Satd. Flow (prot)		3244						3247				
Flt Permitted		0.99						1.00				
Satd. Flow (perm)		3244						3247				
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	277	685	0	0	0	0	0	1185	33	0	0	0
RTOR Reduction (vph)	0	55	0	0	0	0	0	3	0	0	0	0
Lane Group Flow (vph)	0	907	0	0	0	0	0	1215	0	0	0	0
Confl. Peds. (#/hr)	1		1	1		1	1		1	1		1
Confl. Bikes (#/hr)			2	-		-						1
Heavy Vehicles (%)	1%	1%	0%	0%	0%	0%	0%	2%	0%	0%	0%	0%
Turn Type	Perm	NA				.,.		NA			.,.	
Protected Phases		8						6				
Permitted Phases	8	-										
Actuated Green, G (s)	Ŭ	21.0						51.0				
Effective Green, g (s)		21.0						51.0				
Actuated g/C Ratio		0.26						0.64				
Clearance Time (s)		4.0						4.0				
Lane Grp Cap (vph)		851						2069				
v/s Ratio Prot		001						c0.37				
v/s Ratio Perm		0.28						00.01				
v/c Ratio		1.07						0.59				
Uniform Delay, d1		29.5						8.4				
Progression Factor		0.69						0.20				
Incremental Delay, d2		47.4						1.0				
Delay (s)		67.9						2.7				
Level of Service		07.5 E						Α				
Approach Delay (s)		67.9			0.0			2.7			0.0	
Approach LOS		07.5 E			A			Α			A	
		L			Π			Λ			Л	
Intersection Summary			04 5		014 0000	1						
HCM 2000 Control Delay			31.5	Н		Level of S	Service		С			
HCM 2000 Volume to Capacit	y ratio		0.73	~		£			0.0			
Actuated Cycle Length (s)			80.0		um of los				8.0			
Intersection Capacity Utilizatio	n		70.7%	IC	U Level	of Service			С			
Analysis Period (min)			15									

	-	$\mathbf{\hat{v}}$	٦	3		
Movement	EBT	EBR	NBL	NEL		
Lane Configurations	<b>≜</b> †⊅		٦	ኘካ		
Traffic Volume (vph)	820	5	5	420		
Future Volume (vph)	820	5	5	420		
Ideal Flow (vphpl)	1750	1750	1750	1750		
Total Lost time (s)	6.5		6.5	6.5		
Lane Util. Factor	0.95		1.00	0.97		
Frt	1.00		1.00	1.00		
Flt Protected	1.00		1.00	0.95		
Satd. Flow (prot)	3322		1733	3193		
Flt Permitted	1.00		1.00	0.95		
Satd. Flow (perm)	3322		1733	3193		
Peak-hour factor, PHF	0.92	0.92	0.92	0.92		
Adj. Flow (vph)	891	5	5	457		
RTOR Reduction (vph)	0	0	0	0		
Lane Group Flow (vph)	896	0	5	457		
Heavy Vehicles (%)	0%	1%	1%	1%		
Turn Type	NA		Prot	Prot		
Protected Phases	2		3	4		
Permitted Phases						
Actuated Green, G (s)	35.3		9.9	19.1		
Effective Green, g (s)	35.3		9.9	19.1		
Actuated g/C Ratio	0.42		0.12	0.23		
Clearance Time (s)	6.5		6.5	6.5		
Vehicle Extension (s)	6.0		2.5	2.5		
Lane Grp Cap (vph)	1399		204	727		
v/s Ratio Prot	c0.27		c0.00	c0.14		
v/s Ratio Perm						
v/c Ratio	0.64		0.02	0.63		
Uniform Delay, d1	19.2		32.7	29.2		
Progression Factor	1.00		1.00	1.00		
Incremental Delay, d2	1.7		0.0	1.5		
Delay (s)	20.9		32.7	30.6		
Level of Service	С		С	С		
Approach Delay (s)	20.9		32.7	30.6		
Approach LOS	С		С	С		
Intersection Summary						
HCM 2000 Control Delay			24.2	H	CM 2000 Level of Service	С
HCM 2000 Volume to Capa	acity ratio		0.55			
Actuated Cycle Length (s)			83.8	S	um of lost time (s)	21.0
Intersection Capacity Utiliz	ation		57.4%	IC	U Level of Service	В
Analysis Period (min)			15			
c Critical Lane Group						

### HCM Signalized Intersection Capacity Analysis 17: Lyon Street & 99E WB Offramp

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBR	SEL	SER	
Lane Configurations					et 🗧	1	<u>ሕ</u> ግ				
Traffic Volume (vph)	0	0	0	0	5	850	425	0	0	0	
Future Volume (vph)	0	0	0	0	5	850	425	0	0	0	
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	
Total Lost time (s)					4.0	4.0	6.5				
Lane Util. Factor					0.95	0.95	0.97				
Frt					0.85	0.85	1.00				
Flt Protected					1.00	1.00	1.00				
Satd. Flow (prot)					1402	1399	3361				
Flt Permitted					1.00	1.00	1.00				
Satd. Flow (perm)					1402	1399	3361				
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	0	0	0	0	5	924	462	0	0	0	
RTOR Reduction (vph)	0	0	0	0	228	228	0	0	0	0	
Lane Group Flow (vph)	0	0	0	0	239	234	462	0	0	0	
Heavy Vehicles (%)	0%	0%	0%	0%	1%	1%	1%	0%	2%	2%	
Turn Type					NA	Prot	Prot				
Protected Phases					6	6	385				
Permitted Phases											
Actuated Green, G (s)					28.4	28.4	47.4				
Effective Green, g (s)					28.4	28.4	44.4				
Actuated g/C Ratio					0.34	0.34	0.53				
Clearance Time (s)					4.0	4.0					
Vehicle Extension (s)					4.0	4.0					
Lane Grp Cap (vph)					475	474	1780				
v/s Ratio Prot					c0.17	0.17	c0.14				
v/s Ratio Perm											
v/c Ratio					0.50	0.49	0.26				
Uniform Delay, d1					22.1	22.0	10.7				
Progression Factor					1.00	1.00	0.00				
Incremental Delay, d2					1.1	1.1	0.1				
Delay (s)					23.2	23.1	0.1				
Level of Service					С	С	Α				
Approach Delay (s)		0.0			23.2		0.1		0.0		
Approach LOS		А			С		А		А		
Intersection Summary											
HCM 2000 Control Delay			15.5	H	CM 2000	Level of	Service		В		
HCM 2000 Volume to Capacity	y ratio		0.41								
Actuated Cycle Length (s)			83.8	S	um of lost	time (s)			21.0		
Intersection Capacity Utilizatio	n		41.4%		U Level o		)		А		
Analysis Period (min)			15								
c Critical Lane Group											

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	٦	¥î≽		ሻ	<b>†</b> †	1		\$		٦	र्भ	1
Traffic Volume (vph)	110	840	0	5	803	855	5	5	10	643	10	127
Future Volume (vph)	110	840	0	5	803	855	5	5	10	643	10	127
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Lane Width	12	12	12	12	12	16	12	12	12	12	12	16
Total Lost time (s)	4.0	4.0		4.0	4.0	4.0		4.0		4.0	4.0	4.0
Lane Util. Factor	1.00	0.95		1.00	0.95	1.00		1.00		0.95	0.95	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	0.99		1.00		1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00		1.00		1.00	1.00	1.00
Frt	1.00	1.00		1.00	1.00	0.85		0.93		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00		0.99		0.95	1.00	1.00
Satd. Flow (prot)	1646	3228		1662	3260	1655		1612		1519	1421	1616
Flt Permitted	0.95	1.00		0.95	1.00	1.00		0.99		0.95	1.00	1.00
Satd. Flow (perm)	1646	3228		1662	3260	1655		1612		1519	1421	1616
Peak-hour factor, PHF	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97
Adj. Flow (vph)	113	866	0	5	828	881	5	5	10	663	10	131
RTOR Reduction (vph)	0	0	0	0	0	111	0	10	0	0	0	72
Lane Group Flow (vph)	113	866	0	5	828	770	0	10	0	663	10	59
Confl. Bikes (#/hr)						1						1
Heavy Vehicles (%)	1%	3%	0%	0%	2%	1%	0%	0%	0%	4%	17%	3%
Turn Type	Prot	NA		Prot	NA	pm+ov	Split	NA		Split	NA	Perm
Protected Phases	5	2		1	6	4	8	8		4	4	
Permitted Phases	-				-	6	-	-				4
Actuated Green, G (s)	12.4	53.7		0.9	42.2	103.5		2.7		61.3	61.3	61.3
Effective Green, g (s)	12.9	54.9		1.4	43.4	105.5		3.2		62.3	62.3	62.3
Actuated g/C Ratio	0.09	0.40		0.01	0.31	0.77		0.02		0.45	0.45	0.45
Clearance Time (s)	4.5	5.2		4.5	5.2	5.0		4.5		5.0	5.0	5.0
Vehicle Extension (s)	2.5	4.0		2.5	4.0	2.5		2.5		2.5	2.5	2.5
Lane Grp Cap (vph)	154	1286		16	1026	1267		37		686	642	730
v/s Ratio Prot	c0.07	0.27		0.00	c0.25	0.27		c0.01		c0.44	0.01	100
v/s Ratio Perm	00.01	0.21		0.00	00.20	0.19		00.01		00.11	0.01	0.04
v/c Ratio	0.73	0.67		0.31	0.81	0.61		0.28		0.97	0.02	0.08
Uniform Delay, d1	60.8	34.1		67.7	43.4	7.1		66.2		36.7	20.8	21.5
Progression Factor	1.00	1.00		1.00	1.00	1.00		1.00		1.00	1.00	1.00
Incremental Delay, d2	15.6	1.5		8.0	5.0	0.7		2.9		26.0	0.0	0.0
Delay (s)	76.4	35.6		75.7	48.3	7.8		69.1		62.7	20.8	21.5
Level of Service	E	D		E	D	A		E		E	C	21.0 C
Approach Delay (s)		40.3		_	27.6	7.		69.1		_	55.5	Ŭ
Approach LOS		D			C			E			E	
Intersection Summary												
HCM 2000 Control Delay			37.7	Н	CM 2000	) Level of	Service		D			
HCM 2000 Volume to Capa	acity ratio		0.87									
Actuated Cycle Length (s)			137.8			st time (s)			16.0			
Intersection Capacity Utiliza	ation		78.3%	IC	CU Level	of Service	;		D			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations	<u> </u>	<u></u>	<u>^</u>	1	<u>۲</u> ۲	ODIX		
Traffic Volume (vph)	45	1448	1645	800	582	18		
Future Volume (vph)	45	1448	1645	800	582	18		
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750		
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0			
Lane Util. Factor	1.00	0.95	0.95	1.00	0.97			
Frpb, ped/bikes	1.00	1.00	1.00	0.98	1.00			
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00			
Frt	1.00	1.00	1.00	0.85	1.00			
Flt Protected	0.95	1.00	1.00	1.00	0.95			
Satd. Flow (prot)	1583	3228	3260	1439	3213			
Flt Permitted	0.95	1.00	1.00	1.00	0.95			
Satd. Flow (perm)	1583	3228	3260	1439	3213			
Peak-hour factor, PHF	0.97	0.97	0.97	0.97	0.97	0.97		
Adj. Flow (vph)	46	1493	1696	825	600	19		
RTOR Reduction (vph)	0	0	0	0	2	0		
Lane Group Flow (vph)	46	1493	1696	825	617	0		
Confl. Bikes (#/hr)				7		1		
Heavy Vehicles (%)	5%	3%	2%	1%	0%	8%		
Turn Type	Prot	NA	NA	Free	Prot			
Protected Phases	1	6	2		8			
Permitted Phases		6		Free				
Actuated Green, G (s)	4.4	76.7	68.3	111.6	25.4			
Effective Green, g (s)	4.4	77.7	69.3	111.6	25.9			
Actuated g/C Ratio	0.04	0.70	0.62	1.00	0.23			
Clearance Time (s)	4.0	5.0	5.0		4.5			
Vehicle Extension (s)	2.5	4.7	6.0		2.5			
Lane Grp Cap (vph)	62	2247	2024	1439	745			
v/s Ratio Prot	0.03	0.46	c0.52		c0.19			
v/s Ratio Perm				c0.57				
v/c Ratio	0.74	0.66	0.84	0.57	0.83			
Uniform Delay, d1	53.0	9.6	16.7	0.0	40.7			
Progression Factor	1.00	1.00	1.00	1.00	1.00			
Incremental Delay, d2	35.9	0.9	3.7	1.7	7.4			
Delay (s)	89.0	10.5	20.5	1.7	48.2			
Level of Service	F	В	С	А	D			
Approach Delay (s)		12.9	14.3		48.2			
Approach LOS		В	В		D			
Intersection Summary								
HCM 2000 Control Delay			18.3	Н	CM 2000	Level of Service	;	
HCM 2000 Volume to Capaci	ty ratio		0.85					
Actuated Cycle Length (s)			111.6	S	um of lost	time (s)		
Intersection Capacity Utilization	on		74.7%		U Level o			
Analysis Period (min)			15					
a Critical Lana Crown								

c Critical Lane Group

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#### HCM Signalized Intersection Capacity Analysis 3: Ellsworth Street & 1st Avenue

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations											<b>≜</b> ⊅	
Traffic Volume (vph)	0	0	0	75	140	0	0	0	0	0	1855	175
Future Volume (vph)	0	0	0	75	140	0	0	0	0	0	1855	175
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)					4.0						4.0	
Lane Util. Factor					0.95						0.95	
Frpb, ped/bikes					1.00						1.00	
Flpb, ped/bikes					0.99						1.00	
Frt					1.00						0.99	
Flt Protected					0.98						1.00	
Satd. Flow (prot)					3196						3215	
Flt Permitted					0.98						1.00	
Satd. Flow (perm)					3196						3215	
Peak-hour factor, PHF	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97
Adj. Flow (vph)	0	0	0	77	144	0	0	0	0	0	1912	180
RTOR Reduction (vph)	0	0	0	0	19	0	0	0	0	0	9	0
Lane Group Flow (vph)	0	0	0	0	202	0	0	0	0	0	2083	0
Confl. Peds. (#/hr)	9		18	18		9	10		9	9		10
Confl. Bikes (#/hr)												2
Heavy Vehicles (%)	0%	0%	0%	2%	1%	0%	0%	0%	0%	0%	2%	1%
Turn Type				Perm	NA						NA	
Protected Phases					4						2	
Permitted Phases				4								
Actuated Green, G (s)					17.0						55.0	
Effective Green, g (s)					17.0						55.0	
Actuated g/C Ratio					0.21						0.69	
Clearance Time (s)					4.0						4.0	
Lane Grp Cap (vph)					679						2210	
v/s Ratio Prot					010						c0.65	
v/s Ratio Perm					0.06						00.00	
v/c Ratio					0.30						0.94	
Uniform Delay, d1					26.5						11.1	
Progression Factor					1.14						1.00	
Incremental Delay, d2					0.9						9.7	
Delay (s)					31.0						20.8	
Level of Service					C						C	
Approach Delay (s)		0.0			31.0			0.0			20.8	
Approach LOS		A			C			A			C	
Intersection Summary												
HCM 2000 Control Delay			21.8	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capacity	ratio		0.79									
Actuated Cycle Length (s)			80.0	S	um of los	t time (s)			8.0			
Intersection Capacity Utilization			82.6%			of Service			E			
Analysis Period (min)			15									
c Critical Lane Group												

#### HCM Signalized Intersection Capacity Analysis 4: Lyon Street & 1st Avenue

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					•	77						
Traffic Volume (vph)	0	0	0	0	130	745	85	1700	0	0	0	0
Future Volume (vph)	0	0	0	0	130	745	85	1700	0	0	0	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)					4.0	4.0		7.0				
Lane Util. Factor					1.00	0.88		0.95				
Frpb, ped/bikes					1.00	1.00		1.00				
Flpb, ped/bikes					1.00	1.00		1.00				
Frt					1.00	0.85		1.00				
Flt Protected					1.00	1.00		1.00				
Satd. Flow (prot)					1559	2592		3252				
Flt Permitted					1.00	1.00		1.00				
Satd. Flow (perm)					1559	2592		3252				
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	0	0	0	0	137	784	89	1789	0	0	0	0
RTOR Reduction (vph)	0	0	0	0	0	0	0	37	0	0	0	0
Lane Group Flow (vph)	0	0	0	0	137	784	0	1841	0	0	0	0
Confl. Peds. (#/hr)	30		2	2		30	4		2	2		4
Confl. Bikes (#/hr)			_	_		1	-		4			-
Heavy Vehicles (%)	0%	0%	0%	0%	1%	1%	2%	2%	0%	0%	0%	0%
Parking (#/hr)	• , •	• ,•	•,•	•,•	0	. , •	_/*	_/*	• / •	• / •	• ,•	• / •
Turn Type					NA	custom	Perm	NA				
Protected Phases					4	3	1 Onn	6				
Permitted Phases						U	6	U				
Actuated Green, G (s)					32.2	24.0	Ŭ	36.8				
Effective Green, g (s)					32.2	24.0		36.8				
Actuated g/C Ratio					0.40	0.30		0.46				
Clearance Time (s)					4.0	4.0		7.0				
Vehicle Extension (s)					2.5	2.5		4.0				
Lane Grp Cap (vph)					627	777		1495				
v/s Ratio Prot					c0.09	c0.30		1495				
v/s Ratio Perm					0.09	0.50		0.57				
v/c Ratio					0.22	1.01		1.23				
Uniform Delay, d1					15.7	28.0		21.6				
Progression Factor					1.00	1.00		0.61				
Incremental Delay, d2					0.8	34.5		106.9				
Delay (s)					16.5	62.5		120.0				
Level of Service					10.5 B	02.5 E		120.0 F				
Approach Delay (s)		0.0			55.7	E		120.0			0.0	
Approach LOS		0.0 A			55.7 E			120.0 F			0.0 A	
		A			E			Г			A	
Intersection Summary												
HCM 2000 Control Delay			98.9	Н	CM 2000	) Level of	Service		F			
HCM 2000 Volume to Capacity	/ ratio		1.09									
Actuated Cycle Length (s)			80.0			st time (s)			15.0			
Intersection Capacity Utilization	n		93.9%	IC	U Level	of Service	)		F			
Analysis Period (min)			15									
c Critical Lane Group												

c Critical Lane Group

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#### HCM Signalized Intersection Capacity Analysis 5: Ellsworth Street & 2nd Avenue

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		Åî≽								ľ	<u></u>	
Traffic Volume (vph)	0	460	140	0	0	0	0	0	0	490	1440	0
Future Volume (vph)	0	460	140	0	0	0	0	0	0	490	1440	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)		4.0								4.0	4.0	
Lane Util. Factor		0.95								1.00	0.95	
Frpb, ped/bikes		1.00								1.00	1.00	
Flpb, ped/bikes		1.00								1.00	1.00	
Frt		0.96								1.00	1.00	
Flt Protected		1.00								0.95	1.00	
Satd. Flow (prot)		3165								1662	3260	
Flt Permitted		1.00								0.95	1.00	
Satd. Flow (perm)		3165								1662	3260	
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	0	479	146	0	0	0	0	0	0	510	1500	0
RTOR Reduction (vph)	0	31	0	0	0	0	0	0	0	0	0	0
Lane Group Flow (vph)	0	594	0	0	0	0	0	0	0	510	1500	0
Confl. Peds. (#/hr)	1		2	2		1	1		1	1		1
Confl. Bikes (#/hr)			1									1
Heavy Vehicles (%)	0%	1%	1%	0%	0%	0%	0%	0%	0%	0%	2%	0%
Turn Type		NA								Prot	NA	
Protected Phases		8								5	2	
Permitted Phases										-		
Actuated Green, G (s)		22.0								58.0	50.0	
Effective Green, g (s)		22.0								58.0	50.0	
Actuated g/C Ratio		0.28								0.72	0.62	
Clearance Time (s)		4.0								4.0	4.0	
Vehicle Extension (s)		2.5								2.5	4.0	
Lane Grp Cap (vph)		870								1204	2037	
v/s Ratio Prot		c0.19								0.31	c0.46	
v/s Ratio Perm												
v/c Ratio		0.68								0.42	0.74	
Uniform Delay, d1		25.9								4.4	10.4	
Progression Factor		1.00								0.68	0.40	
Incremental Delay, d2		4.3								0.4	1.0	
Delay (s)		30.2								3.4	5.1	
Level of Service		C								A	A	
Approach Delay (s)		30.2			0.0			0.0			4.7	
Approach LOS		С			A			A			A	
Intersection Summary												
HCM 2000 Control Delay			10.7	Н	CM 2000	Level of \$	Service		В			
HCM 2000 Volume to Capacity	ratio		0.74									
Actuated Cycle Length (s)			80.0	S	um of losi	t time (s)			10.0			
Intersection Capacity Utilization	1		82.6%	IC	CU Level	of Service	•		E			
Analysis Period (min)			15									
c Critical Lane Group												

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#### HCM Signalized Intersection Capacity Analysis 6: Lyon Street & 2nd Avenue

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4†						<b>∱</b> ₽				
Traffic Volume (vph)	285	665	0	0	0	0	0	1500	65	0	0	0
Future Volume (vph)	285	665	0	0	0	0	0	1500	65	0	0	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)		7.0						4.0				
Lane Util. Factor		0.95						0.95				
Frpb, ped/bikes		1.00						1.00				
Flpb, ped/bikes		1.00						1.00				
Frt		1.00						0.99				
Flt Protected		0.99						1.00				
Satd. Flow (prot)		3242						3240				
Flt Permitted		0.99						1.00				
Satd. Flow (perm)		3242						3240				
Peak-hour factor, PHF	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Adj. Flow (vph)	297	693	0	0	0	0	0	1562	68	0	0	0
RTOR Reduction (vph)	0	19	0	0	0	0	0	4	0	0	0	0
Lane Group Flow (vph)	0	971	0	0	0	0	0	1627	0	0	0	0
Confl. Peds. (#/hr)	1		1	1		1	1		1	1		1
Confl. Bikes (#/hr)			2									1
Heavy Vehicles (%)	1%	1%	0%	0%	0%	0%	0%	2%	0%	0%	0%	0%
Turn Type	Perm	NA						NA				
Protected Phases		8						6				
Permitted Phases	8											
Actuated Green, G (s)		23.0						46.0				
Effective Green, g (s)		23.0						46.0				_
Actuated g/C Ratio		0.29						0.58				
Clearance Time (s)		7.0						4.0				
Lane Grp Cap (vph)		932						1863				
v/s Ratio Prot								c0.50				
v/s Ratio Perm		0.30										
v/c Ratio		1.04						0.87				_
Uniform Delay, d1		28.5						14.5				
Progression Factor		1.09						0.39				_
Incremental Delay, d2		38.6						3.7				
Delay (s)		69.8						9.4				
Level of Service		E			0.0			A			0.0	
Approach Delay (s)		69.8			0.0			9.4			0.0	
Approach LOS		E			А			А			А	
Intersection Summary												
HCM 2000 Control Delay			32.2	Н	CM 2000	Level of S	Service		С			
HCM 2000 Volume to Capaci	ty ratio		0.93									
Actuated Cycle Length (s)			80.0		um of los				11.0			
Intersection Capacity Utilization	on		88.7%	IC	U Level	of Service			E			
Analysis Period (min)			15									

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Movement	EBT	EBR	NBL	NEL			
Lane Configurations	<b>≜</b> †⊅		5	ሻሻ			
Traffic Volume (vph)	0	1285	0	605			
Future Volume (vph)	0	1285	0	605			
Ideal Flow (vphpl)	1750	1750	1750	1750			
Total Lost time (s)	6.5			6.5			
Lane Util. Factor	0.95			0.97			
Frt	0.85			1.00			
Flt Protected	1.00			0.95			
Satd. Flow (prot)	2798			3072			
Flt Permitted	1.00			0.95			
Satd. Flow (perm)	2798			3072			
Peak-hour factor, PHF	0.92	0.92	0.92	0.92			
Adj. Flow (vph)	0	1397	0	658			
RTOR Reduction (vph)	0	0	0	0			
Lane Group Flow (vph)	1397	0	0	658			
Heavy Vehicles (%)	0%	1%	1%	5%			
Turn Type	NA		Prot	Prot			
Protected Phases	2		3	4			
Permitted Phases							
Actuated Green, G (s)	62.9			26.5			
Effective Green, g (s)	62.9			26.5			
Actuated g/C Ratio	0.50			0.21			
Clearance Time (s)	6.5			6.5			
Vehicle Extension (s)	6.0			2.5			
Lane Grp Cap (vph)	1396			646			
v/s Ratio Prot	c0.50			c0.21			
v/s Ratio Perm							
v/c Ratio	1.87dr			1.02			
Uniform Delay, d1	31.6			49.8			
Progression Factor	1.00			1.00			
Incremental Delay, d2	24.3			40.2			
Delay (s)	55.8			89.9			
Level of Service	E			F			
Approach Delay (s)	55.8		0.0	89.9			
Approach LOS	E		А	F			
Intersection Summary							
HCM 2000 Control Delay			66.7	ł	HCM 2000 Level of Service	E	
HCM 2000 Volume to Capa	acity ratio		0.86				
Actuated Cycle Length (s)			126.0		Sum of lost time (s)	21.0	
Intersection Capacity Utiliza	ation		74.9%	I	CU Level of Service	D	
Analysis Period (min)			15				
dr Defacto Right Lane. R	Recode with	1 though	lane as a	right la	ne.		

### HCM Signalized Intersection Capacity Analysis 17: Lyon Street & 99E WB Offramp

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL2	NBL	NBR	SEL	SER	
Lane Configurations					et 🗧	1		24				
Traffic Volume (vph)	0	0	0	0	5	895	5	600	0	0	0	
Future Volume (vph)	0	0	0	0	5	895	5	600	0	0	0	
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	
Total Lost time (s)					4.0	4.0		6.5				
Lane Util. Factor					0.95	0.95		1.00				
Frt					0.85	0.85		1.00				
Flt Protected					1.00	1.00		1.00				
Satd. Flow (prot)					1402	1399		1733				
Flt Permitted					1.00	1.00		1.00				
Satd. Flow (perm)					1402	1399		1733				
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	
Adj. Flow (vph)	0	0	0	0	5	973	5	652	0	0	0	
RTOR Reduction (vph)	0	0	0	0	89	89	0	36	0	0	0	
Lane Group Flow (vph)	0	0	0	0	403	397	0	621	0	0	0	
Heavy Vehicles (%)	0%	0%	0%	0%	1%	1%	0%	1%	0%	2%	2%	
Turn Type					NA	Prot	Perm	Prot				
Protected Phases					6	6		385				
Permitted Phases							385					
Actuated Green, G (s)					59.4	59.4		58.6				
Effective Green, g (s)					59.4	59.4		55.6				
Actuated g/C Ratio					0.47	0.47		0.44				
Clearance Time (s)					4.0	4.0						
Vehicle Extension (s)					4.0	4.0						
Lane Grp Cap (vph)					660	659		764				
v/s Ratio Prot					c0.29	0.28						
v/s Ratio Perm								0.36				
v/c Ratio					0.61	0.60		0.81				
Uniform Delay, d1					24.7	24.6		30.7				
Progression Factor					1.00	1.00		1.38				
Incremental Delay, d2					1.9	1.8		0.6				
Delay (s)					26.6	26.4		42.9				
Level of Service					С	С		D				
Approach Delay (s)		0.0			26.5			42.9		0.0		
Approach LOS		А			С			D		A		
Intersection Summary												
HCM 2000 Control Delay			33.1	H	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capacit	y ratio		0.77									
Actuated Cycle Length (s)			126.0		um of lost				21.0			
Intersection Capacity Utilizatio	n		65.5%	IC	U Level o	of Service	;		С			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	۲	<b>∱</b> ⊅		٦	<b>^</b>	1		\$		٦	र्स	1
Traffic Volume (vph)	110	840	0	5	805	855	5	5	10	625	10	125
Future Volume (vph)	110	840	0	5	805	855	5	5	10	625	10	125
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Lane Width	12	12	12	12	12	16	12	12	12	12	12	16
Total Lost time (s)	4.0	4.0		4.0	4.0	4.0		4.0		4.0	4.0	4.0
Lane Util. Factor	1.00	0.95		1.00	0.95	1.00		1.00		0.95	0.95	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	0.99		1.00		1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00		1.00		1.00	1.00	1.00
Frt	1.00	1.00		1.00	1.00	0.85		0.93		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00		0.99		0.95	1.00	1.00
Satd. Flow (prot)	1646	3228		1662	3260	1655		1612		1564	1421	1616
Flt Permitted	0.95	1.00		0.95	1.00	1.00		0.99		0.95	1.00	1.00
Satd. Flow (perm)	1646	3228		1662	3260	1655		1612		1564	1421	1616
Peak-hour factor, PHF	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97
Adj. Flow (vph)	113	866	0	5	830	881	5	5	10	644	10	129
RTOR Reduction (vph)	0	0	0	0	0	114	0	10	0	0	0	72
Lane Group Flow (vph)	113	866	0	5	830	767	0	10	0	644	10	57
Confl. Bikes (#/hr)						1						1
Heavy Vehicles (%)	1%	3%	0%	0%	2%	1%	0%	0%	0%	1%	17%	3%
Turn Type	Prot	NA		Prot	NA	pm+ov	Split	NA		Split	NA	Perm
Protected Phases	5	2		1	6	4	8	8		4	4	
Permitted Phases	-				-	6	-	-				4
Actuated Green, G (s)	12.3	52.9		0.9	41.5	98.9		2.6		57.4	57.4	57.4
Effective Green, g (s)	12.8	54.1		1.4	42.7	100.9		3.1		58.4	58.4	58.4
Actuated g/C Ratio	0.10	0.41		0.01	0.32	0.76		0.02		0.44	0.44	0.44
Clearance Time (s)	4.5	5.2		4.5	5.2	5.0		4.5		5.0	5.0	5.0
Vehicle Extension (s)	2.5	4.0		2.5	4.0	2.5		2.5		2.5	2.5	2.5
Lane Grp Cap (vph)	158	1313		17	1046	1255		37		686	623	709
v/s Ratio Prot	c0.07	0.27		0.00	c0.25	0.27		c0.01		c0.41	0.01	
v/s Ratio Perm		•				0.20				••••		0.04
v/c Ratio	0.72	0.66		0.29	0.79	0.61		0.28		0.94	0.02	0.08
Uniform Delay, d1	58.3	32.0		65.3	41.1	7.2		63.8		35.6	21.1	21.7
Progression Factor	1.00	1.00		1.00	1.00	1.00		1.00		1.00	1.00	1.00
Incremental Delay, d2	13.4	1.3		6.9	4.5	0.8		2.9		20.5	0.0	0.0
Delay (s)	71.7	33.3		72.2	45.6	8.0		66.8		56.1	21.1	21.7
Level of Service	E	С		E	D	A		E		E	С	С
Approach Delay (s)		37.8			26.4			66.8			50.0	
Approach LOS		D			С			E			D	
Intersection Summary												
HCM 2000 Control Delay			35.1	Н	CM 2000	) Level of	Service		D			
HCM 2000 Volume to Capa	acity ratio		0.84		2000				U			
Actuated Cycle Length (s)			133.0	S		st time (s)			16.0			
Intersection Capacity Utiliza	ation		78.3%			of Service			10.0 D			
Analysis Period (min)			15						U			
c Critical Lane Group												
o ontiour Eurio Oroup												

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Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations	٢	<b>†</b> †	††	1	ኘዣ	02.1		
Traffic Volume (vph)	35	1605	1285	575	590	60		
Future Volume (vph)	35	1605	1285	575	590	60		
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750		
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0			
Lane Util. Factor	1.00	0.95	0.95	1.00	0.97			
Frpb, ped/bikes	1.00	1.00	1.00	0.98	1.00			
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00			
Frt	1.00	1.00	1.00	0.85	0.99			
Flt Protected	0.95	1.00	1.00	1.00	0.96			
Satd. Flow (prot)	1583	3260	3260	1439	3090			
Flt Permitted	0.95	1.00	1.00	1.00	0.96			
Satd. Flow (perm)	1583	3260	3260	1439	3090			
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92		
Adj. Flow (vph)	38	1745	1397	625	641	65		
RTOR Reduction (vph)	0	0	0	020	7	0		
Lane Group Flow (vph)	38	1745	1397	625	699	0		
Confl. Bikes (#/hr)	00	11-10	1001	7	000	1		
Heavy Vehicles (%)	5%	2%	2%	1%	3%	8%		
Turn Type	Prot	NA	NA	Free	Prot	0,0		
Protected Phases	1	6	2	1100	8			
Permitted Phases	1	6	2	Free	U			
Actuated Green, G (s)	3.1	65.7	58.6	103.4	28.2			
Effective Green, g (s)	3.1	66.7	59.6	103.4	28.7			
Actuated g/C Ratio	0.03	0.65	0.58	1.00	0.28			
Clearance Time (s)	4.0	5.0	5.0	1.00	4.5			
Vehicle Extension (s)	2.5	4.7	6.0		2.5			
Lane Grp Cap (vph)	47	2102	1879	1439	857			
v/s Ratio Prot	0.02	c0.54	0.43	1-100	c0.23			
v/s Ratio Perm	0.02	00.04	0.40	0.43	00.20			
v/c Ratio	0.81	0.83	0.74	0.43	0.82			
Uniform Delay, d1	49.9	14.0	16.2	0.43	34.9			
Progression Factor	1.00	1.00	1.00	1.00	1.00			
Incremental Delay, d2	62.0	3.2	2.2	1.00	5.9			
Delay (s)	111.9	17.3	18.4	1.0	40.8			
Level of Service	F	В	10.4 B	1.0 A	40.0 D			
Approach Delay (s)	1	19.3	13.0	Λ	40.8			
Approach LOS		19.5 B	13.0 B		40.0 D			
		U	U		U			
Intersection Summary			40.0		014 0000		P	
HCM 2000 Control Delay			19.8	Н	CM 2000	Level of Service	В	
HCM 2000 Volume to Capac	city ratio		0.86	~			40.0	
Actuated Cycle Length (s)	e		103.4		um of lost		12.0	
Intersection Capacity Utilizat	tion		75.2%	IC	CU Level o	of Service	D	
Analysis Period (min)			15					
Critical Lane (Froup								

c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					el el	1		-4 <b>†</b>				
Traffic Volume (vph)	0	0	0	0	85	580	65	1280	0	0	0	0
Future Volume (vph)	0	0	0	0	85	580	65	1280	0	0	0	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)					4.0	4.0		5.5				
Lane Util. Factor					0.95	0.95		0.95				
Frpb, ped/bikes					0.96	0.98		1.00				
Flpb, ped/bikes					1.00	1.00		1.00				
Frt					0.88	0.85		1.00				
Flt Protected					1.00	1.00		1.00				
Satd. Flow (prot)					1403	1365		3251				
Flt Permitted					1.00	1.00		1.00				
Satd. Flow (perm)					1403	1365		3251				
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	0	0	0.02	0	92	630	71	1391	0.02	0.02	0.02	0.02
RTOR Reduction (vph)	0	Ŭ Ŭ	0	0	0	0	0	35	0 0	0	0 0	0
Lane Group Flow (vph)	0	0	0	0	407	315	0	1427	0	0	0	0
Confl. Peds. (#/hr)	30	U	2	2	-01	30	4	1721	2	2	U	4
Confl. Bikes (#/hr)	50		2	2		1	7		4	2		7
Heavy Vehicles (%)	0%	0%	0%	0%	1%	1%	2%	2%	0%	0%	0%	0%
Turn Type	070	070	0 /0	0 /0	NA	custom	Perm	NA	070	070	070	0 /0
Protected Phases					4	3	Feilii	6				
Permitted Phases					4	4	6	0				
Actuated Green, G (s)					31.6	31.6	0	38.9				
Effective Green, g (s)					31.6	31.6		38.9				
• • •					0.40	0.40		0.49				
Actuated g/C Ratio Clearance Time (s)					4.0	4.0		5.5				
Vehicle Extension (s)					2.5	4.0		4.0				
Lane Grp Cap (vph)					554	539		1580				_
v/s Ratio Prot					c0.29	0.11		0.44				
v/s Ratio Perm					0 72	0.12		0.44				_
v/c Ratio					0.73	0.58		0.90				
Uniform Delay, d1					20.6	19.0		18.8				_
Progression Factor					1.00	1.00		0.70				
Incremental Delay, d2					8.4	4.6		6.7				_
Delay (s)					29.0	23.6		19.8				
Level of Service		0.0			C	С		B			0.0	_
Approach Delay (s) Approach LOS		0.0 A			26.7 C			19.8 B			0.0	
		A			U			D			A	
Intersection Summary												
HCM 2000 Control Delay			22.1	Н	CM 200	) Level of	Service		С			
HCM 2000 Volume to Capacit	y ratio		0.88									
Actuated Cycle Length (s)			80.0			st time (s)			13.5			
Intersection Capacity Utilization	n		77.1%	IC	CU Level	of Service	;		D			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	٦	<b>∱</b> ⊅		۲.	<b>^</b>	1		\$		٦	र्स	1
Traffic Volume (vph)	110	840	0	5	805	855	5	5	10	625	10	125
Future Volume (vph)	110	840	0	5	805	855	5	5	10	625	10	125
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Lane Width	12	12	12	12	12	16	12	12	12	12	12	16
Total Lost time (s)	4.0	4.0		4.0	4.0	4.0		4.0		4.0	4.0	4.0
Lane Util. Factor	1.00	0.95		1.00	0.95	1.00		1.00		0.95	0.95	1.00
Frpb, ped/bikes	1.00	1.00		1.00	1.00	0.99		1.00		1.00	1.00	0.99
Flpb, ped/bikes	1.00	1.00		1.00	1.00	1.00		1.00		1.00	1.00	1.00
Frt	1.00	1.00		1.00	1.00	0.85		0.93		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00		0.99		0.95	1.00	1.00
Satd. Flow (prot)	1646	3228		1662	3260	1653		1612		1564	1421	1616
Flt Permitted	0.95	1.00		0.95	1.00	1.00		0.99		0.95	1.00	1.00
Satd. Flow (perm)	1646	3228		1662	3260	1653		1612		1564	1421	1616
Peak-hour factor, PHF	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97
Adj. Flow (vph)	113	866	0	5	830	881	5	5	10	644	10	129
RTOR Reduction (vph)	0	0	0	0	0	159	0	10	0	0	0	79
Lane Group Flow (vph)	113	866	0	5	830	722	0	10	0	644	10	50
Confl. Bikes (#/hr)			-			1	-	-	-	-	-	1
Heavy Vehicles (%)	1%	3%	0%	0%	2%	1%	0%	0%	0%	1%	17%	3%
Turn Type	Prot	NA		Prot	NA	pm+ov	Split	NA		Split	NA	Perm
Protected Phases	5	2		1	6	4	8	8		4	4	i onn
Permitted Phases	Ū	-		•	Ŭ	6	Ū	Ŭ		•	•	4
Actuated Green, G (s)	6.1	33.6		0.9	28.4	61.6		1.8		33.2	33.2	33.2
Effective Green, g (s)	6.6	34.8		1.4	29.6	63.6		2.3		34.2	34.2	34.2
Actuated g/C Ratio	0.07	0.39		0.02	0.33	0.72		0.03		0.39	0.39	0.39
Clearance Time (s)	4.5	5.2		4.5	5.2	5.0		4.5		5.0	5.0	5.0
Vehicle Extension (s)	2.5	4.0		2.5	4.0	2.5		2.5		2.5	2.5	2.5
Lane Grp Cap (vph)	122	1266		26	1087	1185		41		603	547	623
v/s Ratio Prot	c0.07	0.27		0.00	c0.25	0.23		c0.01		c0.41	0.01	020
v/s Ratio Perm	00.07	0.21		0.00	00.20	0.20		00.01		00.41	0.01	0.03
v/c Ratio	0.93	0.68		0.19	0.76	0.61		0.25		1.07	0.02	0.08
Uniform Delay, d1	40.8	22.4		43.1	26.4	6.3		42.4		27.2	16.9	17.3
Progression Factor	1.00	1.00		1.00	1.00	1.00		1.00		1.00	1.00	1.00
Incremental Delay, d2	58.5	1.7		2.6	3.4	0.8		2.3		56.1	0.0	0.0
Delay (s)	99.3	24.1		45.7	29.9	7.1		44.7		83.4	16.9	17.3
Level of Service	55.0 F	C		-10.7 D	20.0 C	A		D		F	В	B
Approach Delay (s)		32.7		U	18.2	Λ		44.7			71.7	U
Approach LOS		C			B			D			E	
		Ŭ									-	
Intersection Summary												
HCM 2000 Control Delay			34.4	Н	CM 2000	) Level of	Service		С			
HCM 2000 Volume to Capa	city ratio		0.90									
Actuated Cycle Length (s)			88.7			st time (s)			16.0			
Intersection Capacity Utiliza	ition		78.3%	IC	CU Level	of Service	)		D			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations	<u> </u>	<b>^</b>	1	1	٦¥	OBIX		
Traffic Volume (vph)	45	1430	1645	800	600	20		
Future Volume (vph)	45	1430	1645	800	600	20		
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750		
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	1100		
Lane Util. Factor	1.00	0.95	0.95	1.00	0.97			
Frpb, ped/bikes	1.00	1.00	1.00	0.98	1.00			
Flpb, ped/bikes	1.00	1.00	1.00	1.00	1.00			
Frt	1.00	1.00	1.00	0.85	1.00			
Flt Protected	0.95	1.00	1.00	1.00	0.95			
Satd. Flow (prot)	1583	3228	3260	1439	3121			
Flt Permitted	0.95	1.00	1.00	1.00	0.95			
Satd. Flow (perm)	1583	3228	3260	1439	3121			
Peak-hour factor, PHF	0.97	0.97	0.97	0.97	0.97	0.97		
Adj. Flow (vph)	46	1474	1696	825	619	21		
RTOR Reduction (vph)	0	0	0	0	2	0		
Lane Group Flow (vph)	46	1474	1696	825	638	0		
Confl. Bikes (#/hr)				7		1		
Heavy Vehicles (%)	5%	3%	2%	1%	3%	8%		
Turn Type	Prot	NA	NA	Free	Prot			
Protected Phases	1	6	2		8			
Permitted Phases		6		Free				
Actuated Green, G (s)	3.8	71.5	63.7	108.0	27.0			
Effective Green, g (s)	3.8	72.5	64.7	108.0	27.5			
Actuated g/C Ratio	0.04	0.67	0.60	1.00	0.25			
Clearance Time (s)	4.0	5.0	5.0		4.5			
Vehicle Extension (s)	2.5	4.7	6.0		2.5			
Lane Grp Cap (vph)	55	2166	1952	1439	794			
v/s Ratio Prot	0.03	0.46	c0.52		c0.20			
v/s Ratio Perm				c0.57				
v/c Ratio	0.84	0.68	0.87	0.57	0.80			
Uniform Delay, d1	51.8	10.7	18.1	0.0	37.7			
Progression Factor	1.00	1.00	1.00	1.00	1.00			
Incremental Delay, d2	63.9	1.1	5.0	1.7	5.7			
Delay (s)	115.7	11.8	23.1	1.7	43.5			
Level of Service	F	В	С	А	D			
Approach Delay (s)		15.0	16.1		43.5			
Approach LOS		В	В		D			
Intersection Summary								
HCM 2000 Control Delay			19.5	Н	CM 2000	Level of Service		В
HCM 2000 Volume to Capa	city ratio		0.86					
Actuated Cycle Length (s)			108.0	S	um of lost	time (s)	1	12.0
Intersection Capacity Utiliza	tion		75.3%		U Level c			D
Analysis Period (min)			15					
a Critical Lana Crayer								

c Critical Lane Group

Project Bundle 2 US 20 Albany Study 12:00 am 06/13/2023 Future Conditions 30HV (2043) PM Peak Hour ADB

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					eî 👘	1						
Traffic Volume (vph)	0	0	0	0	130	745	85	1700	0	0	0	0
Future Volume (vph)	0	0	0	0	130	745	85	1700	0	0	0	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)					4.0	4.0		5.5				
Lane Util. Factor					0.95	0.95		0.95				
Frpb, ped/bikes					0.97	1.00		1.00				
Flpb, ped/bikes					1.00	1.00		1.00				
Frt					0.89	0.85		1.00				
Flt Protected					1.00	1.00		1.00				
Satd. Flow (prot)					1272	1399		3252				
Flt Permitted					1.00	1.00		1.00				
Satd. Flow (perm)					1272	1399		3252				
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	0	0	0	0	137	784	89	1789	0	0	0	0
RTOR Reduction (vph)	0	0	0	0	0	0	0	36	0	0	0	0
Lane Group Flow (vph)	0	0	0	0	529	392	0	1842	0	0	0	0
Confl. Peds. (#/hr)	30	Ŭ	2	2	020	30	4	1012	2	2	Ŭ	4
Confl. Bikes (#/hr)			-	_		1	•		4	-		•
Heavy Vehicles (%)	0%	0%	0%	0%	1%	1%	2%	2%	0%	0%	0%	0%
Parking (#/hr)	0,0	070	070	0,0	0	170	270	270	0,0	0,0	0,0	0,0
Turn Type					NA	custom	Perm	NA				
Protected Phases					4	3	I CIIII	6				
Permitted Phases						5	6	0				
Actuated Green, G (s)					32.6	16.0	U	37.9				
Effective Green, g (s)					32.6	16.0		37.9				
Actuated g/C Ratio					0.41	0.20		0.47				
Clearance Time (s)					4.0	4.0		5.5				
Vehicle Extension (s)					2.5	2.0		4.0				
Lane Grp Cap (vph)					518	279		1540				
v/s Ratio Prot					c0.42	c0.28		0.57				
v/s Ratio Perm					4 00	4 44		0.57				
v/c Ratio					1.02	1.41		1.20				
Uniform Delay, d1					23.7	32.0		21.1				
Progression Factor					1.00	1.00		0.57				
Incremental Delay, d2					45.0	202.4		91.3				
Delay (s)					68.7	234.4		103.3				
Level of Service		0.0			E	F		F			0.0	
Approach Delay (s)		0.0			139.2			103.3			0.0	
Approach LOS		А			F			F			А	
Intersection Summary												
HCM 2000 Control Delay			115.1	Н	CM 2000	) Level of	Service		F			
HCM 2000 Volume to Capaci	ty ratio		1.23									
Actuated Cycle Length (s)			80.0			st time (s)			13.5			
Intersection Capacity Utilization	on		97.7%	IC	CU Level	of Service	)		F			
Analysis Period (min)			15									
c Critical Lane Group												

c Critical Lane Group

Project Bundle 2 US 20 Albany Study 12:00 am 06/13/2023 Future Conditions 30HV (2043) PM Peak Hour ADB

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					el el	1		-4 <b>†</b>				
Traffic Volume (vph)	0	0	0	0	85	580	65	1280	0	0	0	0
Future Volume (vph)	0	0	0	0	85	580	65	1280	0	0	0	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)					4.0	4.0		5.5				
Lane Util. Factor					0.95	0.95		0.95				
Frpb, ped/bikes					0.98	0.99		1.00				
Flpb, ped/bikes					1.00	1.00		1.00				
Frt					0.88	0.85		1.00				
Flt Protected					1.00	1.00		1.00				
Satd. Flow (prot)					1428	1391		3251				
Flt Permitted					1.00	1.00		1.00				
Satd. Flow (perm)					1428	1391		3251				
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	0	0	0	0	92	630	71	1391	0	0	0	0
RTOR Reduction (vph)	0	0	0	0	0	0	0	36	0	0	0	0
Lane Group Flow (vph)	0	0	0	0	407	315	0	1426	0	0	0	0
Confl. Peds. (#/hr)	10	·	2	2		10	4		2	2	Ū	4
Confl. Bikes (#/hr)			_	_		1			4	_		
Heavy Vehicles (%)	0%	0%	0%	0%	1%	1%	2%	2%	0%	0%	0%	0%
Turn Type	• /•	• ,•	0,0	•,•	NA	custom	Perm	NA	• / •	• / •	• / •	
Protected Phases					4	3	T UIIII	6				
Permitted Phases					•	4	6	Ū				
Actuated Green, G (s)					33.2	33.2	Ŭ	37.3				
Effective Green, g (s)					33.2	33.2		37.3				
Actuated g/C Ratio					0.42	0.42		0.47				
Clearance Time (s)					4.0	4.0		5.5				
Vehicle Extension (s)					2.5	2.5		4.0				
Lane Grp Cap (vph)					592	577		1515				
v/s Ratio Prot					c0.28	0.17		1010				
v/s Ratio Perm					00.20	0.06		0.44				
v/c Ratio					0.69	0.55		0.94				
Uniform Delay, d1					19.2	17.7		20.3				
Progression Factor					1.00	1.00		0.70				
Incremental Delay, d2					6.4	3.7		10.0				
Delay (s)					25.6	21.4		24.1				
Level of Service					23.0 C	21.4 C		24.1 C				
Approach Delay (s)		0.0			23.7	U		24.1			0.0	
Approach LOS		A			23.7 C			24.1 C			0.0 A	
Intersection Summary												
HCM 2000 Control Delay			24.0	Н	CM 200	) Level of	Service		С			
HCM 2000 Volume to Capacity	ratio		0.87						-			
Actuated Cycle Length (s)			80.0	S	um of los	st time (s)			13.5			
Intersection Capacity Utilization	า		75.4%			of Service			D			
Analysis Period (min)			15						_			
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					4Î	1		-4 <b>†</b>				
Traffic Volume (vph)	0	0	0	0	130	745	85	1700	0	0	0	0
Future Volume (vph)	0	0	0	0	130	745	85	1700	0	0	0	0
Ideal Flow (vphpl)	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750	1750
Total Lost time (s)					4.0	4.0		5.5				
Lane Util. Factor					0.95	0.95		0.95				
Frpb, ped/bikes					0.98	1.00		1.00				
Flpb, ped/bikes					1.00	1.00		1.00				
Frt					0.89	0.85		1.00				
Flt Protected					1.00	1.00		1.00				
Satd. Flow (prot)					1294	1399		3252				
Flt Permitted					1.00	1.00		1.00				
Satd. Flow (perm)					1294	1399		3252				
Peak-hour factor, PHF	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
Adj. Flow (vph)	0	0	0	0	137	784	89	1789	0	0	0	0
RTOR Reduction (vph)	Ũ	Ũ	0	0	0	0	0	35	0	0	0 0	0
Lane Group Flow (vph)	0	0	0	0	529	392	0	1843	0	0	0	0
Confl. Peds. (#/hr)	10	Ŭ	2	2	020	10	4	1010	2	2	Ū	4
Confl. Bikes (#/hr)	10		2	-		1	•		4	-		•
Heavy Vehicles (%)	0%	0%	0%	0%	1%	1%	2%	2%	0%	0%	0%	0%
Parking (#/hr)	070	070	070	070	0	170	270	270	0 /0	070	070	070
Turn Type					NA	custom	Perm	NA				
Protected Phases					4	3	r enn	6				
Permitted Phases					4	5	6	0				
Actuated Green, G (s)					32.2	24.0	0	38.3				
Effective Green, g (s)					32.2	24.0		38.3				
Actuated g/C Ratio					0.40	0.30		0.48				
Clearance Time (s)					4.0	4.0		5.5				
Vehicle Extension (s)					4.0 2.5	4.0 2.0		4.0				
Lane Grp Cap (vph)					520	419		1556				
v/s Ratio Prot					c0.41	0.28		0.57				_
v/s Ratio Perm					4 00	0.04		0.57				
v/c Ratio					1.02	0.94		1.18				_
Uniform Delay, d1					23.9	27.2		20.9				
Progression Factor					1.00	1.00		0.55				_
Incremental Delay, d2					43.9	30.4		85.9				
Delay (s)					67.8	57.7		97.3				_
Level of Service					E	E		F				
Approach Delay (s)		0.0			63.5			97.3			0.0	
Approach LOS		А			E			F			А	
Intersection Summary												
HCM 2000 Control Delay			86.2	Н	CM 2000	) Level of	Service		F			
HCM 2000 Volume to Capacity	ratio		1.17									
Actuated Cycle Length (s)			80.0			st time (s)			13.5			
Intersection Capacity Utilization			96.0%	IC	CU Level	of Service	)		F			
Analysis Period (min)			15									
c Critical Lane Group												

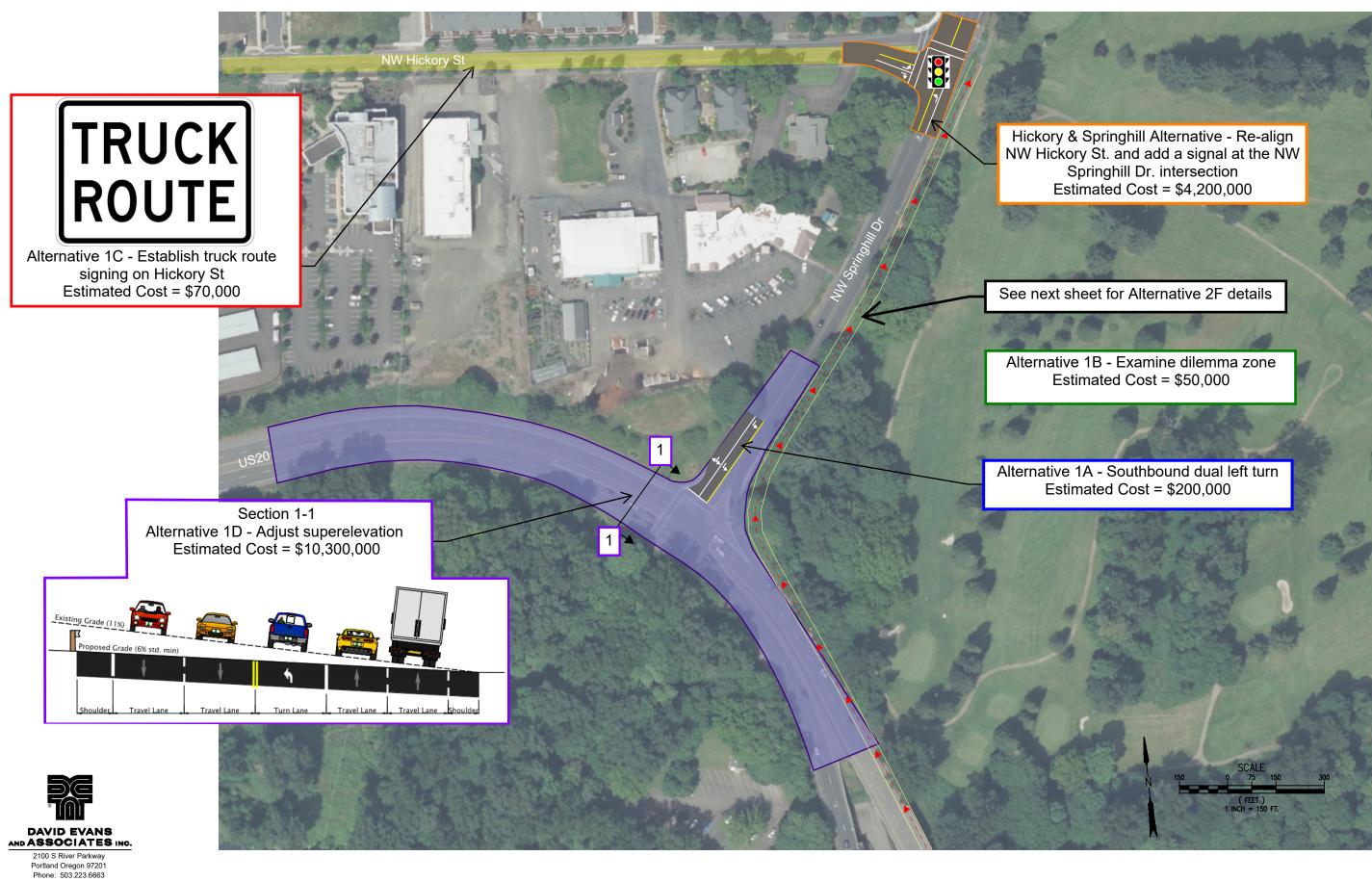
c Critical Lane Group

Project Bundle 3 US 20 Albany Study 12:00 am 06/13/2023 Future Conditions 30HV (2043) PM Peak Hour ADB

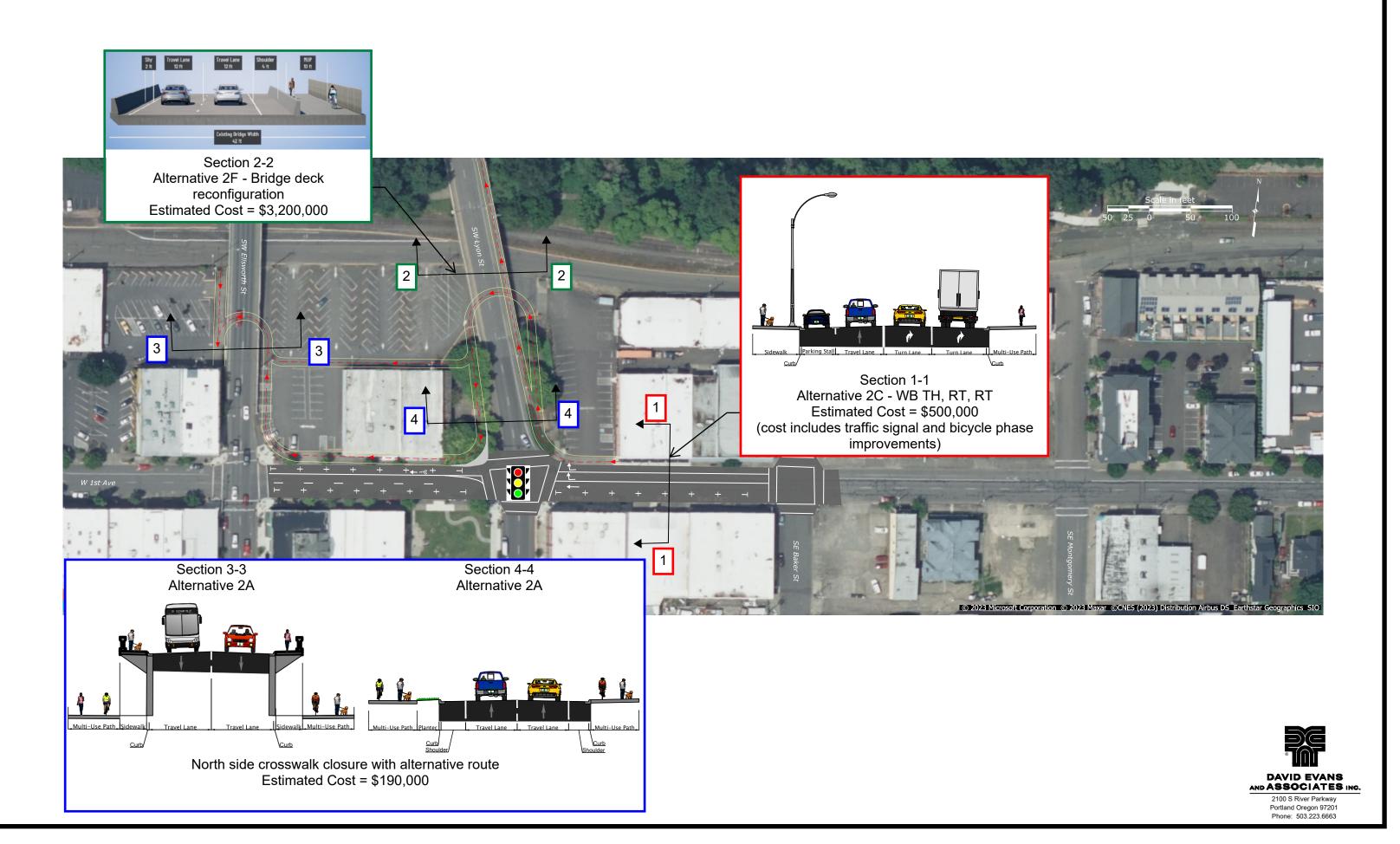
### **APPENDIX C – ALTERNATIVES SCHEMATICS**



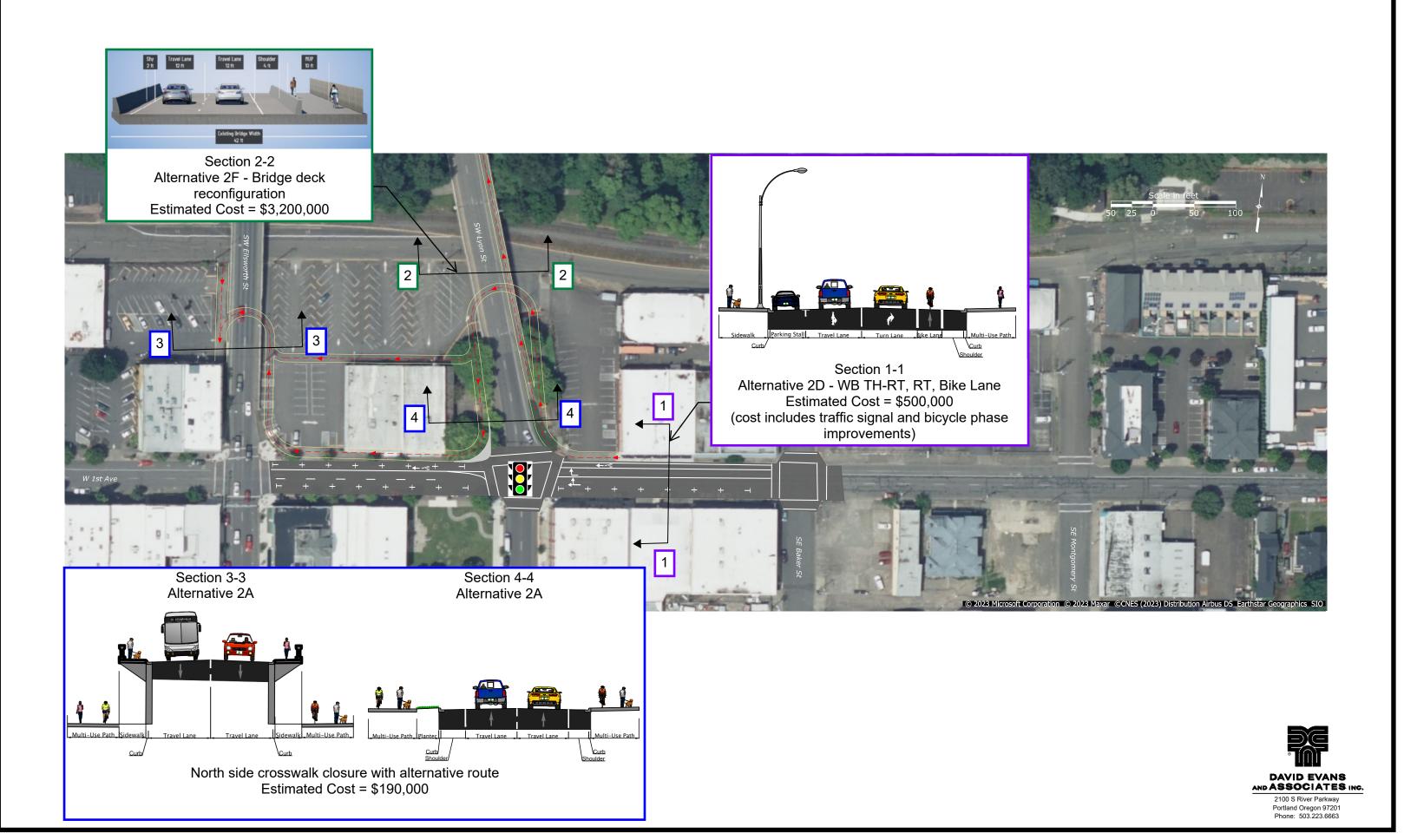
# SPRINGHILL DRIVE / US 20 ALTERNATIVES



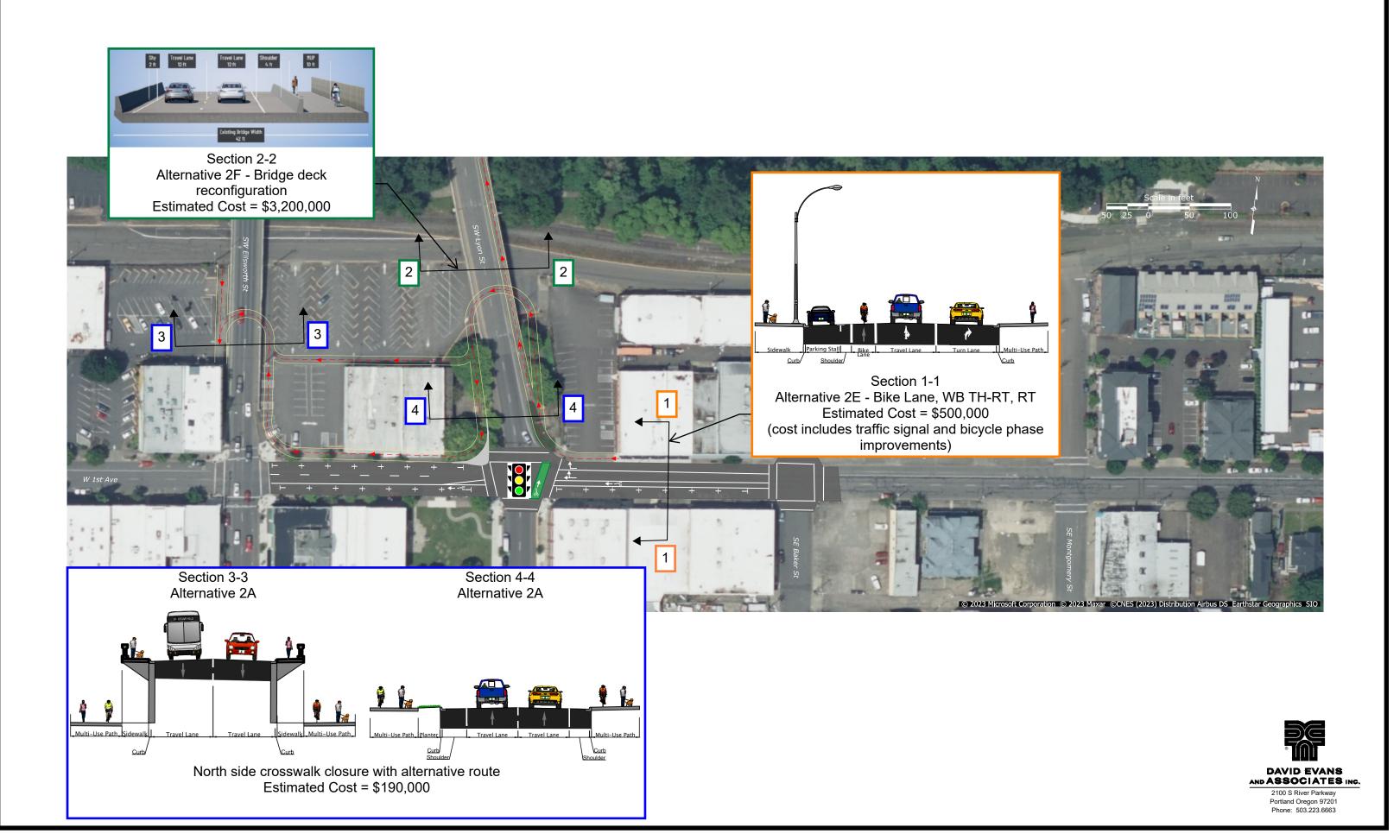
### 1ST / LYON ST ALTERNATIVES



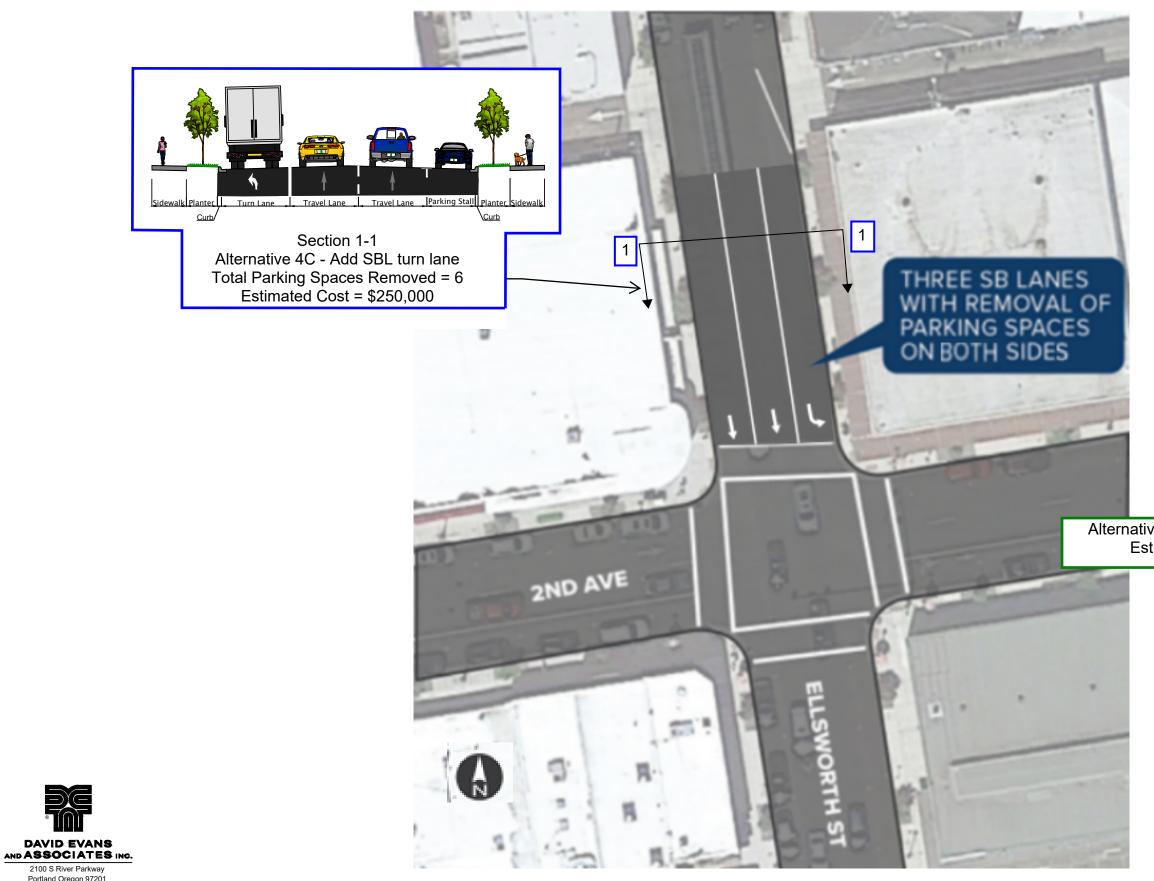
## 1ST / LYON ST ALTERNATIVES



### 1ST / LYON ST ALTERNATIVES



## 1ST & 2ND / ELLSWORTH ST ALTERNATIVES



2100 S River Parkway Portland Oregon 97201 Phone: 503.223.6663

Alternative 4B - Upgrade signal timing Estimated Cost = \$20,000

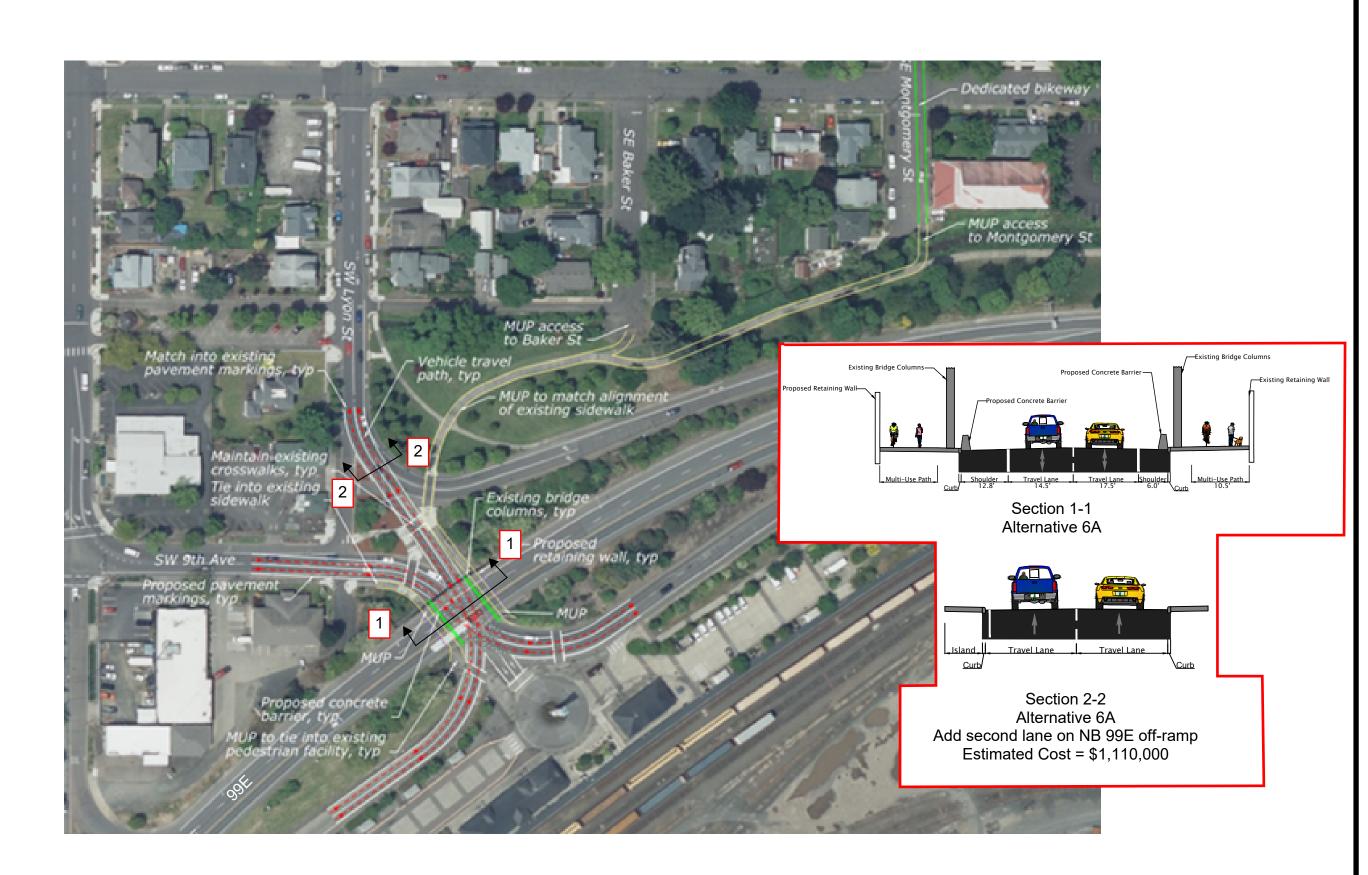
# DOWNTOWN UNSIGNALIZED INTERSECTIONS ALTERNATIVES





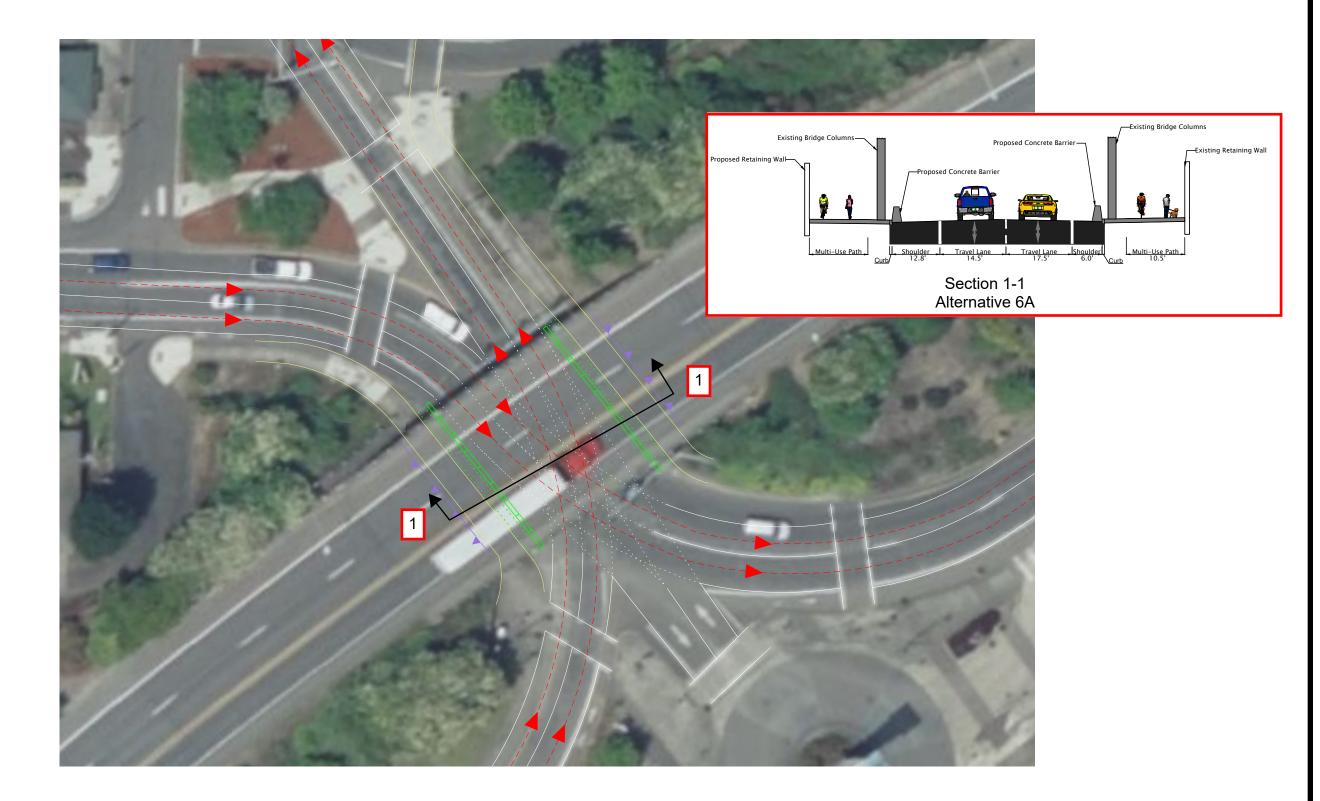


### 9TH / LYON ST / OR 99E ALTERNATIVES



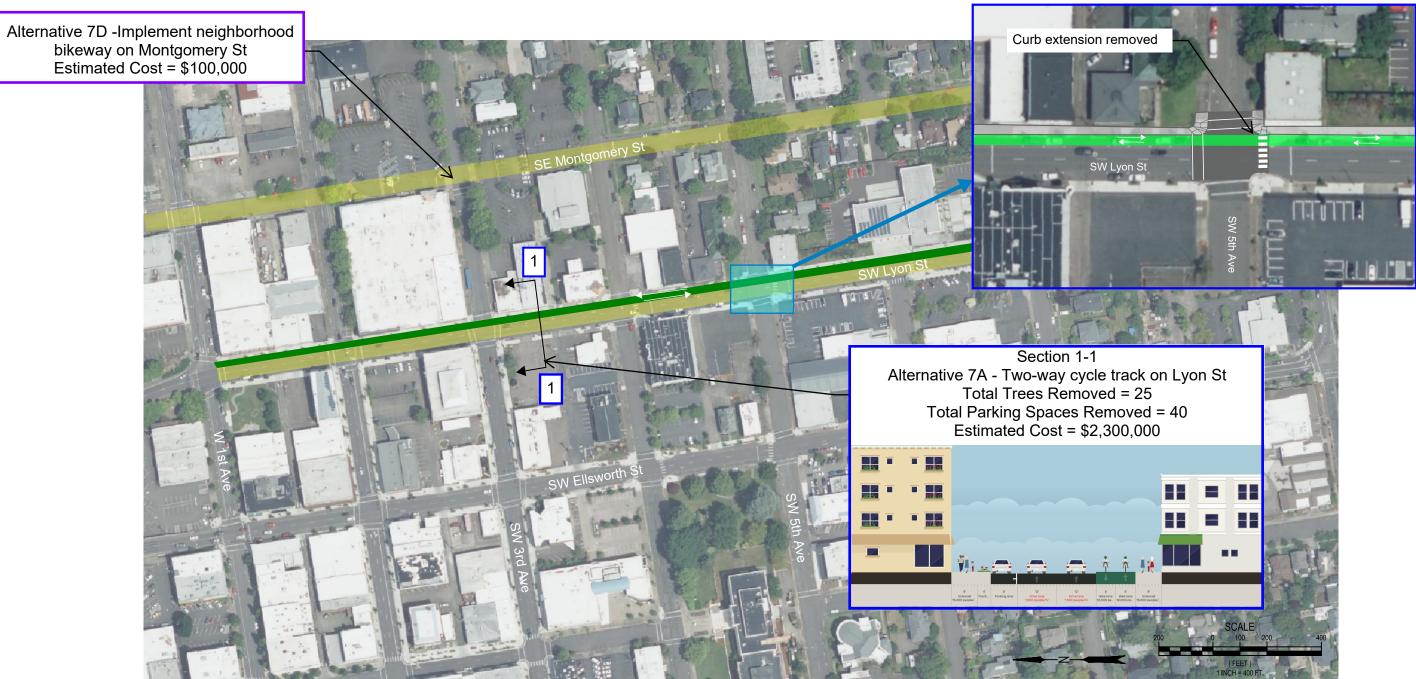


### 9TH / LYON ST / OR 99E ALTERNATIVES



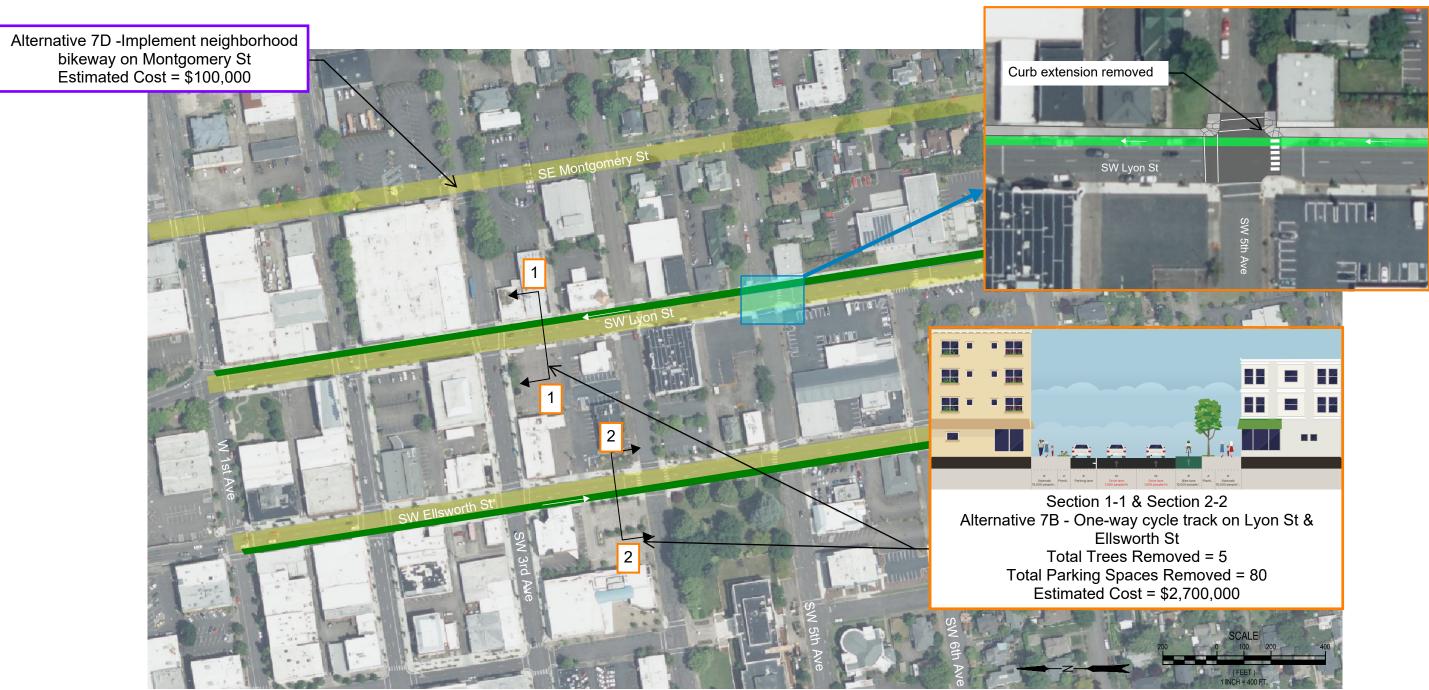


# LYON / ELLSWORTH **BIKE FACILITIES ALTERNATIVES**



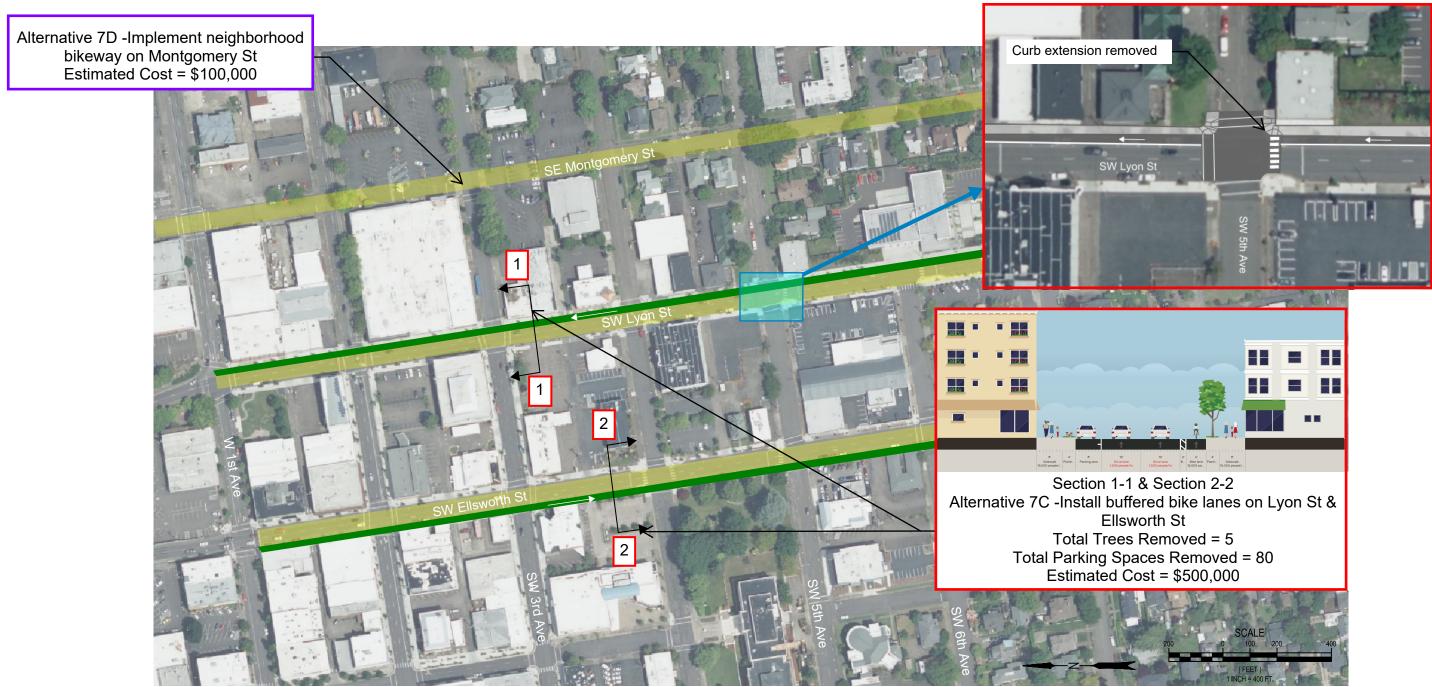


# LYON / ELLSWORTH **BIKE FACILITIES ALTERNATIVES**





# LYON / ELLSWORTH **BIKE FACILITIES ALTERNATIVES**





### **APPENDIX D – ADDITIONAL ALTERNATIVES ADDENDUM**



### ADDITIONAL ALTERNATIVES ADDENDUM

DATE:	April 30, 2024	
то:	Rob Emmons, PE   City of Albany Ron Irish, PE   City of Albany	
FROM:	Aaron Berger, PE   DKS Associates Scott Mansur, PE, PTOE, RSP <sub>1</sub>   DKS Associates	
SUBJECT:	US 20 Albany Study – Additional Alternatives Addendum	DKS P#23072-000

#### ADDITIONAL TRAFFIC NEEDS

After completing the US 20 corridor system evaluation with the Vissim model for Project Bundles 1, 2, and 3, some additional needs with viable solutions were highlighted that were not exposed in the No-Build Vissim model or within the HCM analysis. These needs are summarized as follows:

- Signal Progression at 9<sup>th</sup> Avenue The additional southbound traffic demand released from the 1<sup>st</sup> and 2<sup>nd</sup> Avenue/Ellsworth Street bottleneck by the proposed improvements creates more southbound queuing on Ellsworth Street due to poor progression at the Ellsworth Street/9<sup>th</sup> Avenue and Lyon Street/OR 99E/9<sup>th</sup> Avenue signals. The widening of the OR 99E northbound off-ramp to a dual lane approach provides additional signal timing flexibility to these two signals, which currently operate as free-running under peak hour conditions
- Queuing on 2<sup>nd</sup> Avenue between Ellsworth Street and Lyon Street these queues become a new bottleneck in the system with the improvements to the 1<sup>st</sup> Avenue/Lyon Street intersection and the 2<sup>nd</sup> Avenue/Ellsworth Street intersection. The eastbound left turn at 2<sup>nd</sup> Avenue and Lyon Street is held up by northbound Lyon Street queues and propagates into the eastbound through traffic on 2<sup>nd</sup> Avenue.

#### ADDITIONAL ALTERNATIVES EVALUATION

Based on the additional identified traffic needs, the following alternatives were developed and evaluated:

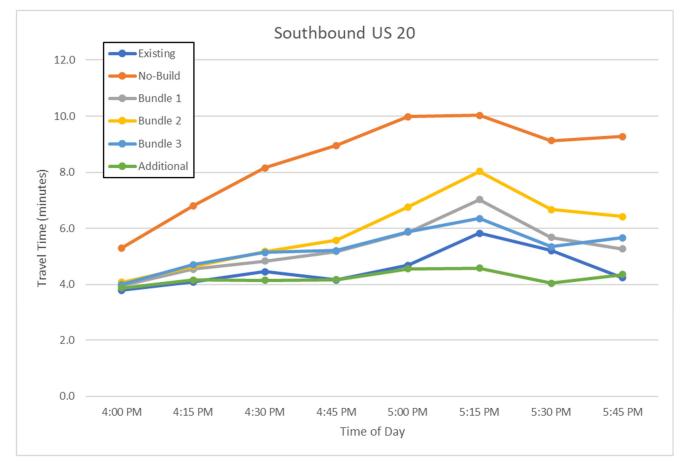
- Alternative 8: Signal Coordination at 9<sup>th</sup> Avenue/Ellsworth Street and 9<sup>th</sup> Avenue/Lyon Street/OR 99E – This alternative involved coordinating these two intersections during at least the PM peak period using a 120 second cycle length and a 10 second offset, progressing the southbound/eastbound movement. The estimated cost of this alternative is <u>\$50,000</u>.
- Alternative 9: New Exclusive Eastbound Left Turn Lane at 2<sup>nd</sup> Avenue/Lyon Street

   This alternative involves removing parking for half a block on both sides of 2<sup>nd</sup> Avenue between Ellsworth Street and Lyon Street, re-striping the approach to include an exclusive

eastbound left turn lane, and re-timing the signal to include both an eastbound left turn phase and a corresponding protected pedestrian phase. The estimated cost of this alternative is **\$250,000**.

Both these alternatives were evaluated using the Vissim model for Project Bundle 3, and the model results were compared against Project Bundle 3 to determine the potential project benefits.

From a corridor perspective, the signal coordination of the two 9<sup>th</sup> Avenue signals decreased queuing on southbound Ellsworth Street and improved average southbound travel times on US 20 by 1.1 minutes (20%) during the PM peak period. The southbound travel time profiles are shown in Figure 1.



#### FIGURE 1: SOUTHBOUND US 20 TRAVEL TIME

The exclusive eastbound left turn lane at 2<sup>nd</sup> Avenue/Lyon Street improved the unserved demand on 2<sup>nd</sup> Avenue from 2% to 0%. Net, the two proposed improvements reduced the system delay by 13% over Project Bundle 3 conditions, from 3.4 to 2.9 minutes of delay per vehicle. The improvements also result in a net unserved demand of only one vehicle by 6 PM, compared to 41 vehicles under No-Build conditions. The full queue plots by 15-minute PM peak period time interval are included as Appendix A to this document. These results indicate that both **Alternative 8** and **Alternative 9** provide substantial operational benefits to the US 20 corridor and the local system, reducing travel delays and queuing.

#### RECOMMENDATIONS

Based on the findings from this evaluation, **Alternative 8** and **Alternative 9** are recommended for inclusion in the US 20 corridor plan and for adoption into the upcoming Albany TSP project list. **Alternative 8** (9<sup>th</sup> Avenue signal coordination) is recommended to be implemented as a two-phase project:

- **Phase 1** would be a Short-Term project and would involve a review and update of the entire US 20 corridor timing on Lyon Street and Ellsworth Street, including consideration of different cycle lengths. This alternative is recommended for simultaneous implementation with the other short-term alternatives along the couplet portion of the corridor that affect signal timing and/or lane configurations.
- Phase 2 would be a Long-Term project and would be implemented with Alternative 6A (OR 99E northbound off-ramp second lane), coordinating the two signals on 9<sup>th</sup> Avenue to better progress southbound to eastbound traffic.

**Alternative 9** (eastbound left turn lane and phasing at 2<sup>nd</sup> Avenue/Lyon Street) is recommended for Short-Term implementation, ideally as a simultaneous project with Alternative 4C (southbound left turn at 2<sup>nd</sup> Avenue/Ellsworth St).

#### APPENDICES

#### **APPENDIX A – ADDITIONAL ALTERNATIVES 2043 CONDITIONS QUEUE PLOTS**

### **APPENDIX A: ADDITIONAL ALTERNATIVES**

**2043 PM CONDITIONS QUEUE PLOTS** 

